

Re-Issued for Permit

### Drainage Assessment

North Stonington Civil Design

Silicon Ranch Corporation

North Stonington, Connecticut

June 25, 2021

(Revision 3)



Version	Date	Description/Summary of Changes
Revision 0	9-30-20	Issued for Permit
Revision 1	2-19-21	Amended 2.3.1 Wetland Description
Revision 2	5-24-21	
Revision 3	6-25-21	

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#### Attachments

- Appendix A Soil Resources Report
- Appendix B USGS & FEMA Firm Maps
- Appendix C NOAA Precipitation Data
- Appendix D Stormwater Drainage Area Map, Peak Flow Calculations, and Pond Design
- Appendix E Curve Number
- Appendix F Time of Concentration
- Appendix G Map of Wetlands
- Appendix H Erosion and Sediment Control Calculations
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#### 1. Narrative

#### 1.1. Project Description

Silicon Ranch Corporation intends to develop a photovoltaic solar site consisting of solar panels, racking, inverters, switchgear, and associated infrastructure necessary for a solar farm. The project site is located on portions of 5 contiguous parcels totaling just over 156 acres. The site location is under 2 miles west of the Connecticut and Rhode Island state line and north of I-95. This report summarizes the proposed facilities and impacts to the stormwater runoff.

#### 1.2. Existing Conditions

Of the five parcels utilized for this project, the two parcels on the north are vacant and wooded and the three parcels to the south are hilly and surrounded by fields previously used for farming, wooded areas, and residential properties. For this project, the existing area was divided into four drainage study areas based on areas of developable land for optimal solar panel orientation and placement. Analysis points were chosen for each of these areas to analyze drainage such that existing flow patterns are maintained and offsite flows do not enter the study areas.

The site consists of type A, B, C, and D soils, but primarily consists of soil type "B". The primary existing land cover is wooded area. The existing site is sparsely covered in trees with forest litter covering the soil; therefore, a fair hydrologic condition was used to compute the curve number. For both existing and proposed conditions, the 2-year (24 hour), 10-year (24 hour), 25-year (24 hour), 50-year (24 hour), and 100-year (24 hour) storms were analyzed and summarized in **Tables 1-5.** 

#### 1.3. Proposed Conditions

Under post-developed conditions, the overland drainage pattern will mimic the existing conditions. Within the 4 study areas, a total of 6 stormwater basins were designed for the 6 primary existing drainage areas. Ditch conveyance is proposed to divert runoff into the proposed stormwater BMPs. The ground cover within the limits of disturbance will change from wooded areas to grassed open space in good hydrologic condition, reducing the curve number and impacting the peak flows. The existing site requires minimal grading. Refer to the drainage area map in **Appendix D**.

#### 2. Stormwater Calculations

#### 2.1. Stormwater Peak Flow Calculations

Sub-basins were developed and analyzed based on the existing and proposed land covers and the hydrologic soil groups for the site found in the Soil Survey. Gravel roadways, transformer pads, and solar arrays were accounted for as impervious in the Weighted Curve Numbers (CN) calculation which was based on the TR-55 method. Although the site will be minimally graded, the CN calculations account for soil compaction activities during the construction of the solar array by increasing the hydrologic soil group present on-site by one-half of the next higher group type. The Time of Concentrations were generated by using the velocity factors from the NRCS Part 630 of the National Engineering Handbook, Chapter 15 and limited to 100 feet for sheet flow. The changes in time of concentration for post-developed runoff are due to a lower Manning's N number due to the change in land cover. The Soil Resource Report for the site can be found in **Appendix A.** The results of the CN and Time of Concentration can be found in **Appendix D and E** respectively. This data,



along with the drainage area, was input into HydroCAD to generate hydrographs. The output of the HydroCAD model can be found in **Appendix C**.

The total rainfall depth was entered into the model and ran utilizing the NRCS Type III rainfall distribution with a 0.05-hour time interval. The HydroCAD results and full storm water peak flow calculations can be found in **Appendix D** of this report. **Tables 1-5** below summarize the peak flows for existing and proposed conditions in different design storms.

Table 1: Pre- and Post-developed peak flows for the 2-yr, 24-hr storm

Name	Area	Pre-Inflow	Post- Inflow	Pre-Inflow vs.	Post-Outflow	Pre-Inflow vs. Post-
Ivallie	(ac)	Q2 (cfs)	Q2 (cfs)	Post-Inflow Q2	Q2 (cfs)	Outflow Q2
1A	4.19	0.71	5.18	4.47	0.83	0.12
1B	4.57	0.99	6.05	5.06	0.77	-0.22
1C	11.85	2.36	16.97	14.61	2.22	-0.14
2	3.66	2.18	5.35	3.17	0.34	-1.84
4	9.02	3.02	10.24	7.22	0.34	-2.68
5	15.22	6.91	26.00	19.09	3.15	-3.76

Table 2: Pre- and Post-developed peak flows for the 10-yr, 24-hr storm

	_	l	l			
Name	Area	Pre-Inflow	Post-Inflow	Pre-Inflow vs.	Post-Outflow	Pre-Inflow vs. Post-
Ivaille	(ac)	Q10 (cfs)	Q10 (cfs)	Post-Inflow Q10	Q10 (cfs)	Outflow Q10
1A	4.19	2.45	10.38	7.93	1.54	-0.91
1B	4.57	3.45	11.32	7.87	1.38	-2.07
1C	11.85	8.18	30.71	22.53	9.93	1.75
2	3.66	4.97	9.89	4.92	5.24	0.27
4	9.02	9.06	21.38	12.32	1.49	-7.57
5	15.22	16.19	34.49	18.3	12.19	-4.00

**Table 3**: Pre- and Post-developed peak flows for the 25-yr, 24-hr storm

Name	Area	Pre-Inflow	Post-Inflow	Pre-Inflow vs.	Post-Outflow	Pre-Inflow vs. Post-
Name	(ac)	Q25 (cfs)	Q25 (cfs)	Post-Inflow Q25	Q25 (cfs)	Outflow Q25
1A	4.19	3.80	13.81	10.01	1.82	-1.98
1B	4.57	5.35	14.69	9.34	1.65	-3.70
1C	11.85	12.71	39.43	26.72	12.29	-0.42
2	3.66	6.90	12.76	5.86	6.35	-0.55
4	9.02	13.54	29.01	15.47	4.75	-8.79
5	15.22	22.66	43.82	21.16	19.41	-3.25

Name	Area	Pre-Inflow	Post-Inflow	Pre-Inflow vs.	Post-Outflow	Pre-Inflow vs. Post-
Name	(ac)	Q50 (cfs)	Q50 (cfs)	Post-Inflow Q50	Q50 (cfs)	Outflow Q50
1A	4.19	4.91	16.42	11.51	2.10	-2.81
1B	4.57	6.89	17.24	10.35	1.81	-5.08
1C	11.85	16.38	45.97	29.59	13.75	-2.63
2	3.66	8.39	14.93	6.54	6.89	-1.50
4	9.02	17.12	34.74	17.62	10.21	-6.91
5	15.22	27.73	50.80	23.07	24.45	-3.28

Table 5: Pre- and Post-developed peak flows for the 100-yr, 24-hr storm

Name	Area (ac)	Pre-Inflow Q100 (cfs)	Post-Inflow Q100 (cfs)	Pre-Inflow vs. Post-Inflow Q100	Post-Outflow Q100 (cfs)	Pre-Inflow vs. Post- Outflow Q100
1A	4.19	6.15	19.22	13.07	4.84	-1.31
1B	4.57	8.62	19.96	11.34	2.53	-6.09
1C	11.85	20.49	52.94	32.45	18.72	-1.77
2	3.66	10.02	17.23	7.21	9.90	-0.12
4	9.02	21.11	40.93	19.82	16.86	-4.25
5	15.22	33.24	76.83	43.59	29.36	-3.88

#### 2.2. Pond, Culvert, and Ditch Calculations

In every drainage area, the post-development peak discharge was greater than the predevelopment peak discharge. To mitigate this increase, ponds are designed to retain water and ensure the post-development flows remain at or below the pre-development flows. These ponds were designed to attenuate the 100-year storm discharge. The pond outlet control consists of an outfall structure with an orifice, culvert, weir and an emergency spillway for 100-year storm discharge. Riprap armoring will be provided at pipe outlets and spillways. Riprap aprons are positioned on slopes less than or equal to fifteen percent. Pond calculations can be found in **Appendix D** of this report.

In addition to the attenuating the peak flows, ponds were designed with consideration for water quality requirements. The orifice invert is set at the water surface elevation for the water quality volume to ensure it's fully retained and treated. Water quality calculations can be found in **Appendix I** of this report.

Access to the site will be from four different driveways, two of which will require culverts for wetland and stream crossings. Three new culverts were designed using AutoCAD Hydraflow Hydrographs Extension. These culverts were designed in accordance with CT DEEP Stream Crossing Guidelines and USACE Openness Ratio Calculations. For additional information on the culvert design calculations see **Appendix I**.

Each drainage area will require permanent ditches to capture and convey flows to the ponds. The ditches were designed using AutoCAD Hydraflow Express using a 100-yr (24 hour) storm event and



CT DEEP conveyance criteria. The flows were calculated as a percentage of the overall subbasin flows per the proposed HydroCAD modeling results. These ditches consist of both trapezoidal and triangular channels. For additional information on ditch design calculations see **Appendix I**.

#### 2.3. Wetlands, FEMA Floodplains, and Coastal Boundaries

#### 2.3.1.Wetlands

Wetlands have been delineated for the site and a map of the wetlands can be found in **Appendix G**. Design has been considered in a way to reduce impacts as much as possible.

#### 2.3.2.FEMA Floodplains

FEMA Floodplains are not located on the site. FEMA Maps of the site can be found in **Appendix B**.

#### 2.3.3. Coastal Boundaries

Coastal Boundaries are not located near the site and were not a necessary consideration for this project. See FEMA Maps located in **Appendix B**.

#### 3. Erosion and Sediment Control

#### 3.1. Erosion and Sediment Control Plans

4. An Erosion and Sediment (E&S) Control Plan has been developed to mitigate the short-term impacts of the site improvements during construction and includes the following information: descriptive specifications concerning land grading, topsoiling, temporary vegetative cover, permanent vegetative cover, vegetative cover selection and mulching, sediment basins, filter rolls, and erosion checks. Details can be found in the E&S plans and have been provided for all erosion controls as necessary. In all cases, the E&S Control Plan shall be implemented in accordance with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control.

#### 4.1. Temporary Stabilization

Temporary stabilization for the site includes silt fence, filter rolls, ditch checks, sediment basins, riprap outlet protection, and construction entrances to reduce vehicular tracking of sediment. Sediment basins are designed to retain the 10-year, 24-hour storm with a retention time of 10 hours. Sediment basins will be constructed in each drainage area that will be converted to a stormwater pond at the end of the project to keep the post-development flows at or below the predevelopment flows. All E&S control measures are designed in accordance with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control. See **Appendix H** for the Erosion and Sediment Control calculations for the sediment basins and traps. These stabilization practices shall be installed and reinforced on the site per the E&S plans before any construction occurs and in accordance with the progressing phases of the project.

#### 4.2. Permanent Stabilization

Permanent stabilization practice on the site will include permanent seeding. Stabilization and permanent seed will be in accordance with the project specifications and plans.



# Appendix A

Soil Resource Report



Natural Resources Conservation Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

## **Custom Soil Resource** Report for State of Connecticut



### **Preface**

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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### **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

### Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons

Soil Map Unit Lines

Soil Map Unit Points

#### **Special Point Features**

Blowout  $\odot$ 

Borrow Pit

Clay Spot

**Closed Depression** 

Gravel Pit

**Gravelly Spot** Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

Spoil Area



Stony Spot



Very Stony Spot



Wet Spot Other



Special Line Features

#### **Water Features**

Streams and Canals

#### Transportation

Rails ---

Interstate Highways

**US Routes** 

Major Roads

 $\sim$ 

Local Roads

#### Background

Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12.000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: State of Connecticut Survey Area Data: Version 20, Jun 9, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Mar 20, 2019—Mar 27, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

### **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
3	Ridgebury, Leicester, and Whitman soils, 0 to 8 percent slopes, extremely stony	3.0	1.9%
13	Walpole sandy loam, 0 to 3 percent slopes	2.6	1.6%
29A	Agawam fine sandy loam, 0 to 3 percent slopes	1.2	0.7%
34B	Merrimac fine sandy loam, 3 to 8 percent slopes	5.7	3.5%
38C	Hinckley loamy sand, 3 to 15 percent slopes	2.2	1.3%
38E	Hinckley loamy sand, 15 to 45 percent slopes	0.1	0.1%
46B	Woodbridge fine sandy loam, 0 to 8 percent slopes, very stony	4.3	2.6%
51B	Sutton fine sandy loam, 0 to 8 percent slopes, very stony	6.1	3.7%
60B	Canton and Charlton fine sandy loams, 3 to 8 percent slopes	5.3	3.2%
60C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes	2.0	1.2%
61B	Canton and Charlton fine sandy loams, 0 to 8 percent slopes, very stony	45.5	27.7%
61C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes, very stony	15.8	9.7%
73C	Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky	9.2	5.6%
84B	Paxton and Montauk fine sandy loams, 3 to 8 percent slopes	2.0	1.2%
85B	Paxton and Montauk fine sandy loams, 3 to 8 percent slopes, very stony	14.2	8.7%
86C	Paxton and Montauk fine sandy loams, 3 to 15 percent slopes, extremely stony	2.4	1.5%
86D	Paxton and Montauk fine sandy loams, 15 to 35 percent slopes, extremely stony	0.1	0.0%
306	Udorthents-Urban land complex	40.9	24.9%
703A	Haven silt loam, 0 to 3 percent slopes	1.3	0.8%
Totals for Area of Interest		164.1	100.0%

### **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas

shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

#### State of Connecticut

## 3—Ridgebury, Leicester, and Whitman soils, 0 to 8 percent slopes, extremely stony

#### **Map Unit Setting**

National map unit symbol: 2t2qt

Elevation: 0 to 1,480 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Ridgebury, extremely stony, and similar soils: 40 percent Leicester, extremely stony, and similar soils: 35 percent Whitman, extremely stony, and similar soils: 17 percent

Minor components: 8 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Ridgebury, Extremely Stony**

#### Setting

Landform: Drumlins, depressions, drainageways, hills, ground moraines

Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope, head slope

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

#### **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 6 inches: fine sandy loam Bw - 6 to 10 inches: sandy loam

Bg - 10 to 19 inches: gravelly sandy loam Cd - 19 to 66 inches: gravelly sandy loam

#### Properties and qualities

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 15 to 35 inches to densic material

Drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: D

Ecological site: F144AY009CT - Wet Till Depressions

Hydric soil rating: Yes

#### **Description of Leicester, Extremely Stony**

#### Setting

Landform: Ground moraines, depressions, drainageways, hills Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear Across-slope shape: Concave

Parent material: Coarse-loamy melt-out till derived from gneiss, granite, and/or

schist

#### **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 7 inches: fine sandy loam

Bg - 7 to 18 inches: fine sandy loam

BC - 18 to 24 inches: fine sandy loam

C1 - 24 to 39 inches: gravelly fine sandy loam C2 - 39 to 65 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: High (about 9.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B/D

Ecological site: F144AY009CT - Wet Till Depressions

Hydric soil rating: Yes

#### **Description of Whitman, Extremely Stony**

#### Setting

Landform: Depressions, drainageways, hills, ground moraines, drumlins

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

#### Typical profile

Oi - 0 to 1 inches: peat

A - 1 to 10 inches: fine sandy loam

Bg - 10 to 17 inches: gravelly fine sandy loam Cdg - 17 to 61 inches: fine sandy loam

#### **Properties and qualities**

Slope: 0 to 3 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 7 to 38 inches to densic material

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: Frequent

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: D

Ecological site: F144AY009CT - Wet Till Depressions

Hydric soil rating: Yes

#### **Minor Components**

#### Woodbridge, extremely stony

Percent of map unit: 6 percent

Landform: Ground moraines, drumlins, hills

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Swansea

Percent of map unit: 2 percent Landform: Swamps, bogs Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### 13—Walpole sandy loam, 0 to 3 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2svkl Elevation: 0 to 1,020 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 250 days

Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

Walpole and similar soils: 80 percent Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Walpole**

#### Setting

Landform: Outwash terraces, outwash plains, depressions, deltas, depressions

Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Tread, dip, talf

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Sandy glaciofluvial deposits derived from igneous, metamorphic

and sedimentary rock

#### **Typical profile**

Oe - 0 to 1 inches: mucky peat A - 1 to 7 inches: sandy loam Bg - 7 to 21 inches: sandy loam

BC - 21 to 25 inches: gravelly sandy loam C - 25 to 65 inches: very gravelly sand

#### Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 4 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Moderate (about 6.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: B/D

Ecological site: F144AY028MA - Wet Outwash

Hydric soil rating: Yes

#### **Minor Components**

#### Sudbury

Percent of map unit: 10 percent

Landform: Deltas, outwash plains, terraces Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Linear

Hydric soil rating: No

#### Scarboro

Percent of map unit: 10 percent

Landform: Outwash terraces, deltas, outwash plains Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### 29A—Agawam fine sandy loam, 0 to 3 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2tyqw

Elevation: 0 to 1,040 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 250 days

Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Agawam and similar soils: 85 percent *Minor components:* 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Agawam**

#### Setting

Landform: Outwash plains, kame terraces, kames, moraines, outwash terraces Landform position (two-dimensional): Backslope, shoulder, footslope, summit Landform position (three-dimensional): Side slope, crest, tread, riser, rise, dip

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Coarse-loamy eolian deposits over sandy and gravelly glaciofluvial deposits derived from gneiss, granite, schist, and/or phyllite

#### **Typical profile**

Ap - 0 to 11 inches: fine sandy loam Bw1 - 11 to 16 inches: fine sandy loam Bw2 - 16 to 26 inches: fine sandy loam 2C1 - 26 to 39 inches: loamy fine sand 2C2 - 39 to 55 inches: loamy fine sand 2C3 - 55 to 65 inches: loamy sand

#### **Properties and qualities**

Slope: 0 to 3 percent

Depth to restrictive feature: 15 to 35 inches to strongly contrasting textural

stratification

Drainage class: Well drained Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: B

Ecological site: F145XY008MA - Dry Outwash

Hydric soil rating: No

#### **Minor Components**

#### Ninigret

Percent of map unit: 5 percent

Landform: Terraces Down-slope shape: Linear Across-slope shape: Concave

Hydric soil rating: No

#### Windsor

Percent of map unit: 4 percent

Landform: Outwash plains, outwash terraces, deltas, dunes

Landform position (three-dimensional): Tread, riser

Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Hydric soil rating: No

#### Walpole

Percent of map unit: 3 percent

Landform: Outwash plains, depressions, outwash terraces, depressions, deltas

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip, talf

Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

#### Hinckley

Percent of map unit: 3 percent

Landform: Outwash plains, eskers, kames, deltas

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Nose slope, side slope, crest, head slope,

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

#### 34B—Merrimac fine sandy loam, 3 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 2tyqs

Elevation: 0 to 1,290 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

#### Map Unit Composition

Merrimac and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Merrimac**

#### Setting

Landform: Kames, eskers, moraines, outwash terraces, outwash plains
Landform position (two-dimensional): Backslope, footslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest, riser, tread

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy glaciofluvial deposits derived from granite, schist, and gneiss over sandy and gravelly glaciofluvial deposits derived from granite,

schist, and gneiss

#### Typical profile

Ap - 0 to 10 inches: fine sandy loam Bw1 - 10 to 22 inches: fine sandy loam

Bw2 - 22 to 26 inches: stratified gravel to gravelly loamy sand 2C - 26 to 65 inches: stratified gravel to very gravelly sand

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 2 percent Maximum salinity: Nonsaline (0.0 to 1.4 mmhos/cm)

Sodium adsorption ratio, maximum: 1.0

Available water capacity: Low (about 4.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: A

Ecological site: F145XY008MA - Dry Outwash

Hydric soil rating: No

#### **Minor Components**

#### Sudbury

Percent of map unit: 5 percent

Landform: Outwash plains, terraces, deltas
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Hinckley

Percent of map unit: 5 percent

Landform: Deltas, outwash plains, eskers, kames

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Nose slope, side slope, crest, head slope,

rise

Down-slope shape: Convex

Across-slope shape: Convex, linear

Hydric soil rating: No

#### Windsor

Percent of map unit: 3 percent

Landform: Outwash plains, deltas, dunes, outwash terraces

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Tread, riser

Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Hydric soil rating: No

#### **Agawam**

Percent of map unit: 2 percent

Landform: Outwash terraces, outwash plains, kames, eskers, stream terraces,

moraines

Landform position (three-dimensional): Rise

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

#### 38C—Hinckley loamy sand, 3 to 15 percent slopes

#### Map Unit Setting

National map unit symbol: 2svmb

Elevation: 0 to 1,290 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

Hinckley and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Hinckley**

#### Setting

Landform: Moraines, outwash terraces, outwash deltas, kame terraces, outwash plains, kames, eskers

Landform position (two-dimensional): Shoulder, backslope, footslope, toeslope, summit

Landform position (three-dimensional): Nose slope, side slope, crest, head slope, riser, tread

Down-slope shape: Convex, linear, concave Across-slope shape: Linear, convex, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

#### **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand Bw2 - 11 to 16 inches: gravelly loamy sand BC - 16 to 19 inches: very gravelly loamy sand

C - 19 to 65 inches: very gravelly sand

#### Properties and qualities

Slope: 3 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

#### **Minor Components**

#### Merrimac

Percent of map unit: 5 percent

Landform: Outwash plains, kames, eskers, moraines, outwash terraces Landform position (two-dimensional): Backslope, footslope, shoulder, toeslope, summit

Landform position (three-dimensional): Side slope, crest, head slope, nose slope,

riser, tread

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Windsor

Percent of map unit: 5 percent

Landform: Eskers, moraines, kame terraces, outwash plains, outwash terraces, outwash deltas, kames

Landform position (two-dimensional): Shoulder, backslope, footslope, toeslope,

Landform position (three-dimensional): Crest, head slope, nose slope, side slope, riser, tread

Down-slope shape: Convex, concave, linear Across-slope shape: Concave, linear, convex

Hydric soil rating: No

**Agawam** 

Percent of map unit: 3 percent

Landform: Outwash deltas, kame terraces, outwash plains, kames, eskers, moraines, outwash terraces

Landform position (two-dimensional): Footslope, backslope, shoulder, toeslope, summit

Landform position (three-dimensional): Nose slope, side slope, crest, head slope, riser, tread

Down-slope shape: Linear, convex, concave Across-slope shape: Convex, linear, concave

Hydric soil rating: No

Sudburv

Percent of map unit: 2 percent

Landform: Outwash plains, moraines, outwash deltas, outwash terraces, kame terraces

Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, linear Across-slope shape: Linear, concave

Hydric soil rating: No

#### 38E—Hinckley loamy sand, 15 to 45 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2svmj

Elevation: 0 to 1,280 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Hinckley and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Hinckley**

#### Setting

Landform: Kames, eskers, kame terraces, outwash plains, moraines, outwash terraces, outwash deltas

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Nose slope, side slope, crest, head slope,

Down-slope shape: Linear, convex, concave Across-slope shape: Convex, linear, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

#### Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand Bw2 - 11 to 16 inches: gravelly loamy sand BC - 16 to 19 inches: very gravelly loamy sand

C - 19 to 65 inches: very gravelly sand

#### **Properties and qualities**

Slope: 15 to 45 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7e

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

#### **Minor Components**

#### Merrimac

Percent of map unit: 5 percent

Landform: Kames, eskers, moraines, outwash terraces, outwash plains

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Side slope, crest, head slope, nose slope,

riser

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

#### Windsor

Percent of map unit: 5 percent

Landform: Outwash deltas, moraines, kames, eskers, kame terraces, outwash

plains, outwash terraces

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

riser

Down-slope shape: Concave, linear, convex Across-slope shape: Linear, concave, convex

Hydric soil rating: No

#### **Agawam**

Percent of map unit: 3 percent

Landform: Kames, moraines, outwash terraces, outwash deltas, kame terraces,

eskers, outwash plains

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Nose slope, side slope, crest, head slope,

riser

Down-slope shape: Linear, convex, concave Across-slope shape: Convex, linear, concave

Hydric soil rating: No

#### **Sudbury**

Percent of map unit: 2 percent

Landform: Eskers, kames, moraines, outwash terraces, kame terraces, outwash

plains, outwash deltas

Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Linear, concave Across-slope shape: Linear, concave

Hydric soil rating: No

#### 46B—Woodbridge fine sandy loam, 0 to 8 percent slopes, very stony

#### Map Unit Setting

National map unit symbol: 2t2qr

Elevation: 0 to 1,440 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Woodbridge, very stony, and similar soils: 82 percent

Minor components: 18 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### Description of Woodbridge, Very Stony

#### Setting

Landform: Hills, ground moraines, drumlins

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Side slope

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

#### Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 9 inches: fine sandy loam
Bw1 - 9 to 20 inches: fine sandy loam
Bw2 - 20 to 32 inches: fine sandy loam
Cd - 32 to 67 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Moderately well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 19 to 27 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 4.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: C/D

Ecological site: F144AY037MA - Moist Dense Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Paxton. verv stonv

Percent of map unit: 10 percent

Landform: Drumlins, hills, ground moraines

Landform position (two-dimensional): Shoulder, backslope, summit

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Hydric soil rating: No

#### Ridgebury, very stony

Percent of map unit: 8 percent

Landform: Ground moraines, depressions, drumlins, drainageways, hills

Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Head slope, base slope

Down-slope shape: Concave

Across-slope shape: Concave

Hydric soil rating: Yes

#### 51B—Sutton fine sandy loam, 0 to 8 percent slopes, very stony

#### **Map Unit Setting**

National map unit symbol: 2xfff Elevation: 0 to 1,410 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Sutton, very stony, and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Sutton, Very Stony**

#### Setting

Landform: Hills, ground moraines

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Coarse-loamy melt-out till derived from gneiss, granite, and/or

schist

#### Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 7 inches: fine sandy loam
Bw1 - 7 to 19 inches: fine sandy loam
Bw2 - 19 to 27 inches: sandy loam
C1 - 27 to 41 inches: gravelly sandy loam
C2 - 41 to 62 inches: gravelly sandy loam

#### **Properties and qualities**

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 12 to 27 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water capacity: Moderate (about 8.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B/D

Ecological site: F144AY008CT - Moist Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Charlton, very stony

Percent of map unit: 7 percent

Landform: Hills, ground moraines, ridges

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Linear, convex Across-slope shape: Convex

Hydric soil rating: No

#### Canton, very stony

Percent of map unit: 4 percent Landform: Ridges, hills, moraines

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Hydric soil rating: No

#### Leicester, very stony

Percent of map unit: 3 percent

Landform: Hills, drainageways, ground moraines, depressions Landform position (two-dimensional): Footslope, toeslope

Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear Across-slope shape: Concave

Hydric soil rating: Yes

#### Whitman, very stony

Percent of map unit: 1 percent

Landform: Drainageways, hills, ground moraines, drumlins, depressions

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### 60B—Canton and Charlton fine sandy loams, 3 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 2w81s

Elevation: 0 to 1,460 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Canton and similar soils: 50 percent Charlton and similar soils: 35 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Canton**

#### Setting

Landform: Ridges, moraines, hills

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, nose slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy melt-out till derived from gneiss, granite, and/or schist

#### **Typical profile**

Ap - 0 to 7 inches: fine sandy loam
Bw1 - 7 to 15 inches: fine sandy loam

Bw2 - 15 to 26 inches: gravelly fine sandy loam 2C - 26 to 65 inches: gravelly loamy sand

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural

stratification

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Very low (about 2.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Description of Charlton**

#### Settina

Landform: Hills, ground moraines, ridges

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Linear, convex Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

#### **Typical profile**

Ap - 0 to 7 inches: fine sandy loam

Bw - 7 to 22 inches: gravelly fine sandy loam C - 22 to 65 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water capacity: Moderate (about 6.9 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Sutton

Percent of map unit: 5 percent

Landform: Hills, ridges, ground moraines
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Leicester

Percent of map unit: 5 percent

Landform: Drainageways, ground moraines, hills, depressions Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope

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Down-slope shape: Linear, concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Chatfield

Percent of map unit: 5 percent

Landform: Ridges, hills

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

### 60C—Canton and Charlton fine sandy loams, 8 to 15 percent slopes

#### Map Unit Setting

National map unit symbol: 2w81z

Elevation: 0 to 1,620 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

Canton and similar soils: 50 percent Charlton and similar soils: 35 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Canton**

#### Setting

Landform: Ridges, moraines, hills

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, nose slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy melt-out till derived from gneiss,

granite, and/or schist

#### Typical profile

Ap - 0 to 7 inches: fine sandy loam Bw1 - 7 to 15 inches: fine sandy loam

Bw2 - 15 to 26 inches: gravelly fine sandy loam 2C - 26 to 65 inches: gravelly loamy sand

#### Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural

stratification

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Very low (about 2.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Description of Charlton**

#### Setting

Landform: Hills, ground moraines, ridges
Landform position (two-dimensional): Backslope
Landform position (three-dimensional): Side slope

Down-slope shape: Linear, convex Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

schist

#### Typical profile

Ap - 0 to 7 inches: fine sandy loam

Bw - 7 to 22 inches: gravelly fine sandy loam C - 22 to 65 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water capacity: Moderate (about 6.9 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Chatfield

Percent of map unit: 5 percent

Landform: Hills, ridges

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

#### Leicester

Percent of map unit: 5 percent

Landform: Hills, depressions, drainageways, ground moraines Landform position (two-dimensional): Toeslope, footslope

Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear

Across-slope shape: Concave

Hydric soil rating: Yes

#### Sutton

Percent of map unit: 5 percent

Landform: Ground moraines, hills, ridges

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

# 61B—Canton and Charlton fine sandy loams, 0 to 8 percent slopes, very stony

#### **Map Unit Setting**

National map unit symbol: 2w81v

Elevation: 0 to 1,480 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Canton, very stony, and similar soils: 50 percent Charlton, very stony, and similar soils: 35 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Canton, Very Stony**

#### Setting

Landform: Ridges, hills, moraines

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Crest, nose slope, side slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy melt-out till derived from gneiss,

granite, and/or schist

#### Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 5 inches: fine sandy loam Bw1 - 5 to 16 inches: fine sandy loam

Bw2 - 16 to 22 inches: gravelly fine sandy loam 2C - 22 to 67 inches: gravelly loamy sand

#### Properties and qualities

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural

stratification

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Description of Charlton, Very Stony**

#### Setting

Landform: Hills, ground moraines, ridges

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Linear, convex Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

schist

#### Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 4 inches: fine sandy loam

Bw - 4 to 27 inches: gravelly fine sandy loam C - 27 to 65 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water capacity: Moderate (about 8.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Leicester, very stony

Percent of map unit: 5 percent

Landform: Ground moraines, depressions, drainageways, hills Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear Across-slope shape: Concave

Hydric soil rating: Yes

#### Chatfield, very stony

Percent of map unit: 5 percent

Landform: Hills, ridges

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Nose slope, crest, side slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

#### Sutton, very stony

Percent of map unit: 5 percent Landform: Hills, ground moraines

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

# 61C—Canton and Charlton fine sandy loams, 8 to 15 percent slopes, very stony

#### **Map Unit Setting**

National map unit symbol: 2w820

Elevation: 0 to 1,540 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Canton, very stony, and similar soils: 50 percent Charlton, very stony, and similar soils: 35 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Canton, Very Stony**

#### Setting

Landform: Ridges, hills, moraines

Landform position (two-dimensional): Backslope, summit, shoulder Landform position (three-dimensional): Side slope, crest, nose slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy melt-out till derived from gneiss, granite, and/or schist

#### Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 5 inches: fine sandy loam Bw1 - 5 to 16 inches: fine sandy loam

Bw2 - 16 to 22 inches: gravelly fine sandy loam 2C - 22 to 67 inches: gravelly loamy sand

#### **Properties and qualities**

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural

stratification

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Description of Charlton, Very Stony**

#### Settina

Landform: Hills, ground moraines, ridges

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Linear, convex Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

schist

#### Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 4 inches: fine sandy loam

Bw - 4 to 27 inches: gravelly fine sandy loam C - 27 to 65 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Moderate (about 8.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Chatfield, very stony

Percent of map unit: 5 percent

Landform: Hills, ridges

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

#### Leicester, very stony

Percent of map unit: 5 percent

Landform: Hills, ground moraines, depressions, drainageways Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear

Across-slope shape: Concave

Hydric soil rating: Yes

#### Sutton, very stony

Percent of map unit: 5 percent Landform: Hills, ground moraines

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

## 73C—Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky

#### **Map Unit Setting**

National map unit symbol: 2w698

Elevation: 0 to 1,550 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Charlton, very stony, and similar soils: 50 percent Chatfield, very stony, and similar soils: 30 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Charlton, Very Stony**

#### Setting

Landform: Hills, ridges

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Linear, convex Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

schist

#### Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 4 inches: fine sandy loam

Bw - 4 to 27 inches: gravelly fine sandy loam C - 27 to 65 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Moderate (about 8.7 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Description of Chatfield, Very Stony**

#### Setting

Landform: Ridges, hills

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

schist

#### **Typical profile**

Oi - 0 to 1 inches: slightly decomposed plant material

A - 1 to 2 inches: fine sandy loam

Bw - 2 to 30 inches: gravelly fine sandy loam

2R - 30 to 40 inches: bedrock

#### **Properties and qualities**

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 20 to 41 inches to lithic bedrock

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 4.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Sutton, very stony

Percent of map unit: 5 percent Landform: Ground moraines, hills

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### **Rock outcrop**

Percent of map unit: 5 percent

Hydric soil rating: No

#### Hollis, very stony

Percent of map unit: 5 percent

Landform: Ridges, hills

Landform position (two-dimensional): Backslope, shoulder, summit Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

#### Leicester, very stony

Percent of map unit: 5 percent Landform: Drainageways, depressions

Down-slope shape: Linear
Across-slope shape: Concave

Hydric soil rating: Yes

#### 84B—Paxton and Montauk fine sandy loams, 3 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2t2qn

Elevation: 0 to 1,570 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Paxton and similar soils: 55 percent Montauk and similar soils: 30 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Paxton**

#### Setting

Landform: Hills, drumlins, ground moraines

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Side slope, crest, nose slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or schist

#### **Typical profile**

Ap - 0 to 8 inches: fine sandy loam
Bw1 - 8 to 15 inches: fine sandy loam
Bw2 - 15 to 26 inches: fine sandy loam
Cd - 26 to 65 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: 18 to 39 inches to densic material

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

#### **Description of Montauk**

#### Setting

Landform: Drumlins, hills Down-slope shape: Convex Across-slope shape: Linear

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

#### **Typical profile**

A - 0 to 4 inches: fine sandy loam
Bw1 - 4 to 14 inches: fine sandy loam
Bw2 - 14 to 25 inches: sandy loam

2Cd1 - 25 to 39 inches: gravelly loamy coarse sand 2Cd2 - 39 to 60 inches: gravelly sandy loam

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: 20 to 38 inches to densic material

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: About 24 to 30 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 3.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Ridgebury

Percent of map unit: 5 percent

Landform: Hills, ground moraines, depressions, drainageways
Landform position (two-dimensional): Toeslope, backslope, footslope
Landform position (three-dimensional): Base slope, head slope, dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Woodbridge

Percent of map unit: 5 percent

Landform: Hills, drumlins, ground moraines

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Side slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Charlton

Percent of map unit: 5 percent

Landform: Hills

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

# 85B—Paxton and Montauk fine sandy loams, 3 to 8 percent slopes, very stony

#### **Map Unit Setting**

National map unit symbol: 2w679

Elevation: 0 to 1,530 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Paxton, very stony, and similar soils: 55 percent Montauk, very stony, and similar soils: 30 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Paxton, Very Stony**

#### Setting

Landform: Drumlins, ground moraines, hills

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Linear, convex Across-slope shape: Convex

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

#### **Typical profile**

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 10 inches: fine sandy loam

Bw1 - 10 to 17 inches: fine sandy loam

Bw2 - 17 to 28 inches: fine sandy loam

Cd - 28 to 67 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 3 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 4.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

#### **Description of Montauk, Very Stony**

#### Setting

Landform: Ground moraines, recessionial moraines, drumlins, hills Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Linear, convex Across-slope shape: Convex

Parent material: Coarse-loamy over sandy lodgment till derived from gneiss,

granite, and/or schist

#### **Typical profile**

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 6 inches: fine sandy loam
Bw1 - 6 to 28 inches: fine sandy loam
Bw2 - 28 to 36 inches: sandy loam

2Cd - 36 to 74 inches: gravelly loamy sand

#### **Properties and qualities**

Slope: 3 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 1.42 in/hr)

Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 5.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Woodbridge, very stony

Percent of map unit: 8 percent

Landform: Drumlins, hills, ground moraines

Landform position (two-dimensional): Backslope, summit, footslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Charlton, very stony

Percent of map unit: 3 percent

Landform: Hills

Landform position (two-dimensional): Shoulder, summit, backslope

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Ridgebury, very stony

Percent of map unit: 3 percent

Landform: Ground moraines, depressions, drumlins, drainageways, hills

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, head slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Stockbridge, very stony

Percent of map unit: 1 percent

Landform: Hills

Landform position (two-dimensional): Shoulder, backslope, summit

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

# 86C—Paxton and Montauk fine sandy loams, 3 to 15 percent slopes, extremely stony

#### Map Unit Setting

National map unit symbol: 2w67d

Elevation: 20 to 1,490 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Paxton, extremely stony, and similar soils: 55 percent Montauk, extremely stony, and similar soils: 30 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Paxton, Extremely Stony**

#### Setting

Landform: Ground moraines, drumlins, hills

Landform position (two-dimensional): Summit, backslope, shoulder

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Linear, convex Across-slope shape: Convex

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

#### Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 10 inches: fine sandy loam

Bw1 - 10 to 17 inches: fine sandy loam

Bw2 - 17 to 28 inches: fine sandy loam

Cd - 28 to 67 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 4.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

#### **Description of Montauk, Extremely Stony**

#### Setting

Landform: Drumlins, hills, ground moraines, recessionial moraines Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Linear, convex Across-slope shape: Convex

Parent material: Coarse-loamy over sandy lodgment till derived from gneiss,

granite, and/or schist

#### **Typical profile**

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 6 inches: fine sandy loam
Bw1 - 6 to 28 inches: fine sandy loam
Bw2 - 28 to 36 inches: sandy loam

2Cd - 36 to 74 inches: gravelly loamy sand

#### **Properties and qualities**

Slope: 3 to 15 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 1.42 in/hr)

Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 5.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Charlton, extremely stony

Percent of map unit: 6 percent

Landform: Hills

Landform position (two-dimensional): Shoulder, summit, backslope

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

#### Woodbridge, extremely stony

Percent of map unit: 5 percent

Landform: Hills, ground moraines, drumlins

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Ridgebury, extremely stony

Percent of map unit: 3 percent

Landform: Drainageways, hills, ground moraines, depressions, drumlins

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope, head slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Stockbridge, extremely stony

Percent of map unit: 1 percent

Landform: Hills

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

# 86D—Paxton and Montauk fine sandy loams, 15 to 35 percent slopes, extremely stony

#### **Map Unit Setting**

National map unit symbol: 2w67c

Elevation: 0 to 1,400 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Paxton, extremely stony, and similar soils: 55 percent Montauk, extremely stony, and similar soils: 30 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Paxton, Extremely Stony**

#### Setting

Landform: Drumlins, hills, ground moraines

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Linear, convex Across-slope shape: Convex

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

#### **Typical profile**

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 10 inches: fine sandy loam

Bw1 - 10 to 17 inches: fine sandy loam

Bw2 - 17 to 28 inches: fine sandy loam

Cd - 28 to 67 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 15 to 35 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 4.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

#### **Description of Montauk, Extremely Stony**

#### Setting

Landform: Drumlins, ground moraines, recessionial moraines, hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Linear, convex Across-slope shape: Convex

Parent material: Coarse-loamy over sandy lodgment till derived from gneiss,

granite, and/or schist

#### **Typical profile**

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 6 inches: fine sandy loam
Bw1 - 6 to 28 inches: fine sandy loam
Bw2 - 28 to 36 inches: sandy loam

2Cd - 36 to 74 inches: gravelly loamy sand

#### **Properties and qualities**

Slope: 15 to 35 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 1.42 in/hr)

Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 5.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Charlton, extremely stony

Percent of map unit: 6 percent

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Woodbridge, extremely stony

Percent of map unit: 5 percent

Landform: Drumlins, hills, ground moraines

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Ridgebury, extremely stony

Percent of map unit: 3 percent

Landform: Drainageways, hills, ground moraines, depressions, drumlins

Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope, head slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Stockbridge, extremely stony

Hydric soil rating: No

Percent of map unit: 1 percent

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

#### 306—Udorthents-Urban land complex

#### **Map Unit Setting**

National map unit symbol: 9lmg

Elevation: 0 to 2,000 feet

Mean annual precipitation: 43 to 56 inches Mean annual air temperature: 45 to 55 degrees F

Frost-free period: 120 to 185 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Udorthents and similar soils: 50 percent

Urban land: 35 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Udorthents**

#### Setting

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Drift

#### **Typical profile**

A - 0 to 5 inches: loam

C1 - 5 to 21 inches: gravelly loam

C2 - 21 to 80 inches: very gravelly sandy loam

#### Properties and qualities

Slope: 0 to 25 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00

to 1.98 in/hr)

Depth to water table: About 54 to 72 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Moderate (about 6.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: B Hydric soil rating: No

#### **Description of Urban Land**

#### Typical profile

H - 0 to 6 inches: material

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydrologic Soil Group: D Hydric soil rating: Unranked

### **Minor Components**

#### Unnamed, undisturbed soils

Percent of map unit: 8 percent

Hydric soil rating: No

#### Udorthents, wet substratum

Percent of map unit: 5 percent Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### **Rock outcrop**

Percent of map unit: 2 percent

Hydric soil rating: No

#### 703A—Haven silt loam, 0 to 3 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2y07k

Elevation: 0 to 1,200 feet

Mean annual precipitation: 43 to 54 inches Mean annual air temperature: 45 to 55 degrees F

Frost-free period: 140 to 185 days

Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Haven and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Haven**

#### Setting

Landform: Outwash terraces, outwash plains Landform position (three-dimensional): Tread

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Coarse-loamy eolian deposits over sandy and gravelly glaciofluvial deposits derived from granite and/or schist and/or gneiss

#### Typical profile

Ap - 0 to 7 inches: silt loam
Bw1 - 7 to 14 inches: silt loam
Bw2 - 14 to 20 inches: silt loam
BC - 20 to 24 inches: fine sandy loam

2C - 24 to 60 inches: stratified very gravelly sand to gravelly fine sand

#### **Properties and qualities**

Slope: 0 to 3 percent

Depth to restrictive feature: 18 to 36 inches to strongly contrasting textural

stratification

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 4.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 1

Hydrologic Soil Group: B

Ecological site: F144AY023CT - Well Drained Outwash

Hydric soil rating: No

#### **Minor Components**

#### **Enfield**

Percent of map unit: 5 percent

Landform: Outwash plains, outwash terraces Landform position (three-dimensional): Tread

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### **Tisbury**

Percent of map unit: 5 percent

Landform: Deltas, valley trains, outwash terraces, outwash plains

Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: No

#### **Agawam**

Percent of map unit: 3 percent

Landform: Moraines, outwash terraces, outwash plains, kame terraces, kames

Landform position (two-dimensional): Shoulder, summit

Landform position (three-dimensional): Side slope, crest, tread

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

## Raypol

Percent of map unit: 2 percent
Landform: Depressions, drainageways
Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

## Soil Information for All Uses

## Suitabilities and Limitations for Use

The Suitabilities and Limitations for Use section includes various soil interpretations displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each interpretation.

### **Land Classifications**

Land Classifications are specified land use and management groupings that are assigned to soil areas because combinations of soil have similar behavior for specified practices. Most are based on soil properties and other factors that directly influence the specific use of the soil. Example classifications include ecological site classification, farmland classification, irrigated and nonirrigated land capability classification, and hydric rating.

## **Hydric Rating by Map Unit**

This rating indicates the percentage of map units that meets the criteria for hydric soils. Map units are composed of one or more map unit components or soil types, each of which is rated as hydric soil or not hydric. Map units that are made up dominantly of hydric soils may have small areas of minor nonhydric components in the higher positions on the landform, and map units that are made up dominantly of nonhydric soils may have small areas of minor hydric components in the lower positions on the landform. Each map unit is rated based on its respective components and the percentage of each component within the map unit.

The thematic map is color coded based on the composition of hydric components. The five color classes are separated as 100 percent hydric components, 66 to 99 percent hydric components, 33 to 65 percent hydric components, 1 to 32 percent hydric components, and less than one percent hydric components.

In Web Soil Survey, the Summary by Map Unit table that is displayed below the map pane contains a column named 'Rating'. In this column the percentage of each map unit that is classified as hydric is displayed.

Hydric soils are defined by the National Technical Committee for Hydric Soils (NTCHS) as soils that formed under conditions of saturation, flooding, or ponding long enough during the growing season to develop anaerobic conditions in the upper part (Federal Register, 1994). Under natural conditions, these soils are either saturated or inundated long enough during the growing season to support the growth and reproduction of hydrophytic vegetation.

The NTCHS definition identifies general soil properties that are associated with wetness. In order to determine whether a specific soil is a hydric soil or nonhydric soil, however, more specific information, such as information about the depth and duration of the water table, is needed. Thus, criteria that identify those estimated soil properties unique to hydric soils have been established (Federal Register, 2002). These criteria are used to identify map unit components that normally are associated with wetlands. The criteria used are selected estimated soil properties that are described in "Soil Taxonomy" (Soil Survey Staff, 1999) and "Keys to Soil Taxonomy" (Soil Survey Staff, 2006) and in the "Soil Survey Manual" (Soil Survey Division Staff, 1993).

If soils are wet enough for a long enough period of time to be considered hydric, they should exhibit certain properties that can be easily observed in the field. These visible properties are indicators of hydric soils. The indicators used to make onsite determinations of hydric soils are specified in "Field Indicators of Hydric Soils in the United States" (Hurt and Vasilas, 2006).

#### References:

Federal Register. July 13, 1994. Changes in hydric soils of the United States.

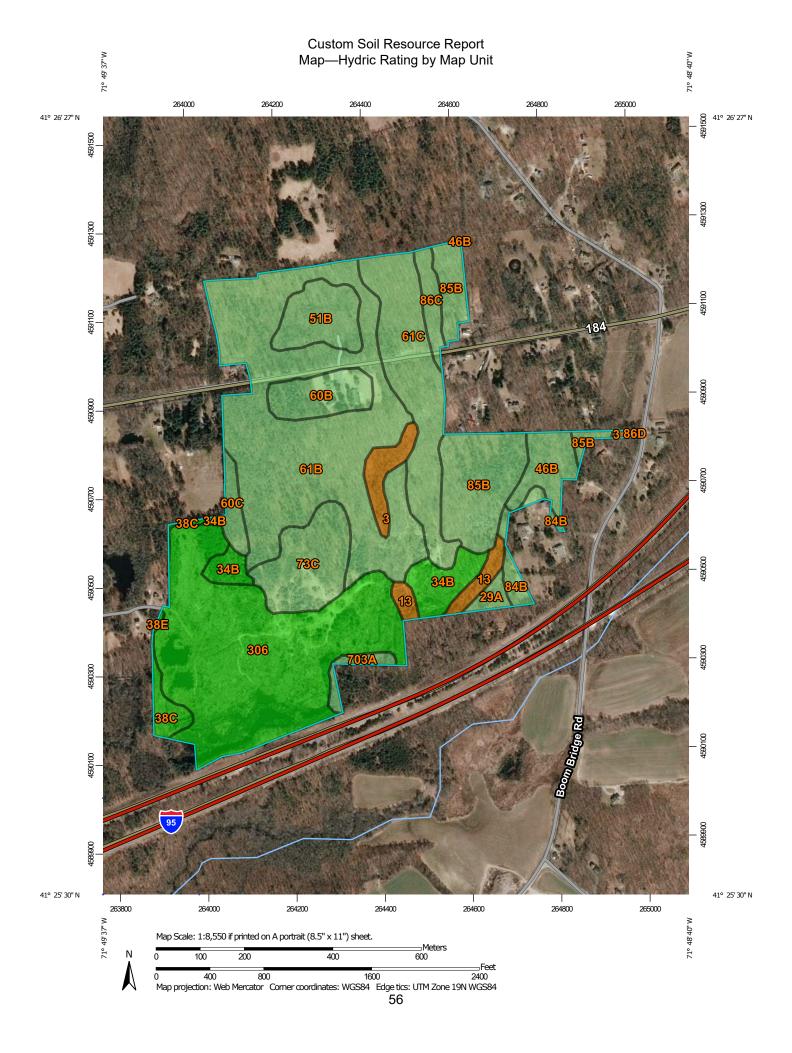
Federal Register. September 18, 2002. Hydric soils of the United States.

Hurt, G.W., and L.M. Vasilas, editors. Version 6.0, 2006. Field indicators of hydric soils in the United States.

Soil Survey Division Staff. 1993. Soil survey manual. Soil Conservation Service. U.S. Department of Agriculture Handbook 18.

Soil Survey Staff. 1999. Soil taxonomy: A basic system of soil classification for making and interpreting soil surveys. 2nd edition. Natural Resources Conservation Service. U.S. Department of Agriculture Handbook 436.

Soil Survey Staff. 2006. Keys to soil taxonomy. 10th edition. U.S. Department of Agriculture, Natural Resources Conservation Service.



#### MAP LEGEND MAP INFORMATION Area of Interest (AOI) The soil surveys that comprise your AOI were mapped at Transportation 1:12.000. Area of Interest (AOI) Rails Soils Interstate Highways Please rely on the bar scale on each map sheet for map Soil Rating Polygons measurements. **US Routes** Hydric (100%) Major Roads Source of Map: Natural Resources Conservation Service Hydric (66 to 99%) Web Soil Survey URL: Local Roads $\sim$ Hydric (33 to 65%) Coordinate System: Web Mercator (EPSG:3857) Background Hydric (1 to 32%) Aerial Photography Maps from the Web Soil Survey are based on the Web Mercator Not Hydric (0%) projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Not rated or not available Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. Soil Rating Lines Hydric (100%) This product is generated from the USDA-NRCS certified data as Hydric (66 to 99%) of the version date(s) listed below. Hydric (33 to 65%) Soil Survey Area: State of Connecticut Hydric (1 to 32%) Survey Area Data: Version 20, Jun 9, 2020 Not Hydric (0%) Soil map units are labeled (as space allows) for map scales Not rated or not available 1:50,000 or larger. **Soil Rating Points** Date(s) aerial images were photographed: Mar 20, 2019—Mar Hydric (100%) 27, 2019 Hydric (66 to 99%) Hydric (33 to 65%) The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background Hydric (1 to 32%) imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. Not Hydric (0%) Not rated or not available **Water Features** Streams and Canals

## Table—Hydric Rating by Map Unit

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
3	Ridgebury, Leicester, and Whitman soils, 0 to 8 percent slopes, extremely stony	94	3.0	1.9%
13	Walpole sandy loam, 0 to 3 percent slopes	90	2.6	1.6%
29A	Agawam fine sandy loam, 0 to 3 percent slopes	3	1.2	0.7%
34B	Merrimac fine sandy loam, 3 to 8 percent slopes	0	5.7	3.5%
38C	Hinckley loamy sand, 3 to 15 percent slopes	0	2.2	1.3%
38E	Hinckley loamy sand, 15 to 45 percent slopes	0	0.1	0.1%
46B	Woodbridge fine sandy loam, 0 to 8 percent slopes, very stony	8	4.3	2.6%
51B	Sutton fine sandy loam, 0 to 8 percent slopes, very stony	4	6.1	3.7%
60B	Canton and Charlton fine sandy loams, 3 to 8 percent slopes	5	5.3	3.2%
60C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes	5	2.0	1.2%
61B	Canton and Charlton fine sandy loams, 0 to 8 percent slopes, very stony	5	45.5	27.7%
61C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes, very stony	5	15.8	9.7%
73C	Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky	5	9.2	5.6%
84B	Paxton and Montauk fine sandy loams, 3 to 8 percent slopes	5	2.0	1.2%
85B	Paxton and Montauk fine sandy loams, 3 to 8 percent slopes, very stony	3	14.2	8.7%

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI	
86C	Paxton and Montauk fine sandy loams, 3 to 15 percent slopes, extremely stony	3	2.4	1.5%	
86D	Paxton and Montauk fine sandy loams, 15 to 35 percent slopes, extremely stony	3	0.1	0.0%	
306	Udorthents-Urban land complex	0	40.9	24.9%	
703A	Haven silt loam, 0 to 3 percent slopes	2	1.3	0.8%	
Totals for Area of Interest			164.1	100.0%	

## Rating Options—Hydric Rating by Map Unit

Aggregation Method: Percent Present

Component Percent Cutoff: None Specified

Tie-break Rule: Lower

## **Soil Properties and Qualities**

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

### Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

## **Hydrologic Soil Group**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

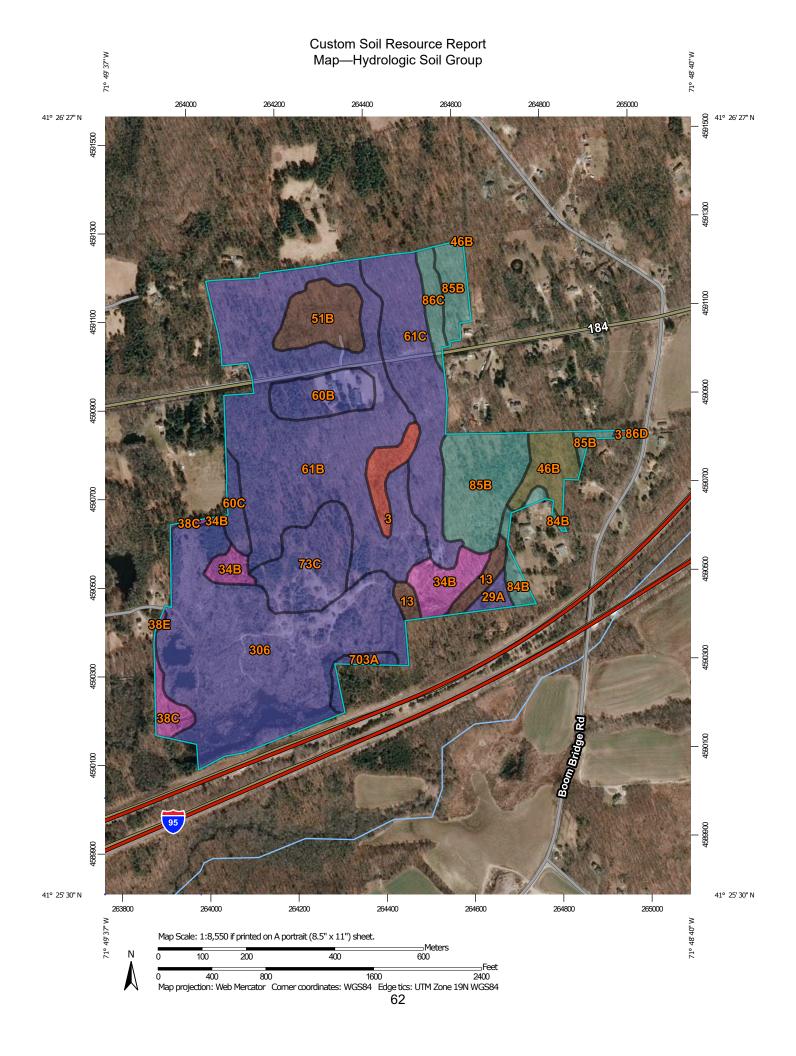
Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at

or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.



#### MAP LEGEND MAP INFORMATION Area of Interest (AOI) The soil surveys that comprise your AOI were mapped at С 1:12.000. Area of Interest (AOI) C/D Soils Please rely on the bar scale on each map sheet for map D Soil Rating Polygons measurements. Not rated or not available Α Source of Map: Natural Resources Conservation Service **Water Features** A/D Web Soil Survey URL: Streams and Canals В Coordinate System: Web Mercator (EPSG:3857) Transportation B/D Rails ---Maps from the Web Soil Survey are based on the Web Mercator С projection, which preserves direction and shape but distorts Interstate Highways distance and area. A projection that preserves area, such as the C/D **US Routes** Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. D Major Roads ~ Not rated or not available -Local Roads This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Rating Lines Background Aerial Photography Soil Survey Area: State of Connecticut Survey Area Data: Version 20, Jun 9, 2020 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Mar 20, 2019—Mar C/D 27, 2019 The orthophoto or other base map on which the soil lines were Not rated or not available compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor **Soil Rating Points** shifting of map unit boundaries may be evident. Α A/D B/D

## Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
3	Ridgebury, Leicester, and Whitman soils, 0 to 8 percent slopes, extremely stony	D	3.0	1.9%
13	Walpole sandy loam, 0 to 3 percent slopes	B/D	2.6	1.6%
29A	Agawam fine sandy loam, 0 to 3 percent slopes	В	1.2	0.7%
34B	Merrimac fine sandy loam, 3 to 8 percent slopes	A	5.7	3.5%
38C	Hinckley loamy sand, 3 to 15 percent slopes	A	2.2	1.3%
38E	Hinckley loamy sand, 15 to 45 percent slopes	A	0.1	0.1%
46B	Woodbridge fine sandy loam, 0 to 8 percent slopes, very stony	C/D	4.3	2.6%
51B	Sutton fine sandy loam, 0 to 8 percent slopes, very stony	B/D	6.1	3.7%
60B	Canton and Charlton fine sandy loams, 3 to 8 percent slopes	В	5.3	3.2%
60C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes	В	2.0	1.2%
61B	Canton and Charlton fine sandy loams, 0 to 8 percent slopes, very stony	В	45.5	27.7%
61C	Canton and Charlton fine sandy loams, 8 to 15 percent slopes, very stony	В	15.8	9.7%
73C	Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky	В	9.2	5.6%
84B	Paxton and Montauk fine sandy loams, 3 to 8 percent slopes	С	2.0	1.2%
85B	Paxton and Montauk fine sandy loams, 3 to 8 percent slopes, very stony	С	14.2	8.7%

#### Custom Soil Resource Report

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
86C	Paxton and Montauk fine sandy loams, 3 to 15 percent slopes, extremely stony	С	2.4	1.5%
86D	Paxton and Montauk fine sandy loams, 15 to 35 percent slopes, extremely stony	С	0.1	0.0%
306	Udorthents-Urban land complex	В	40.9	24.9%
703A	Haven silt loam, 0 to 3 percent slopes	В	1.3	0.8%
Totals for Area of Inter	est	•	164.1	100.0%

#### Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

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#### Custom Soil Resource Report

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### Appendix B

USGS & FEMA Firm Maps

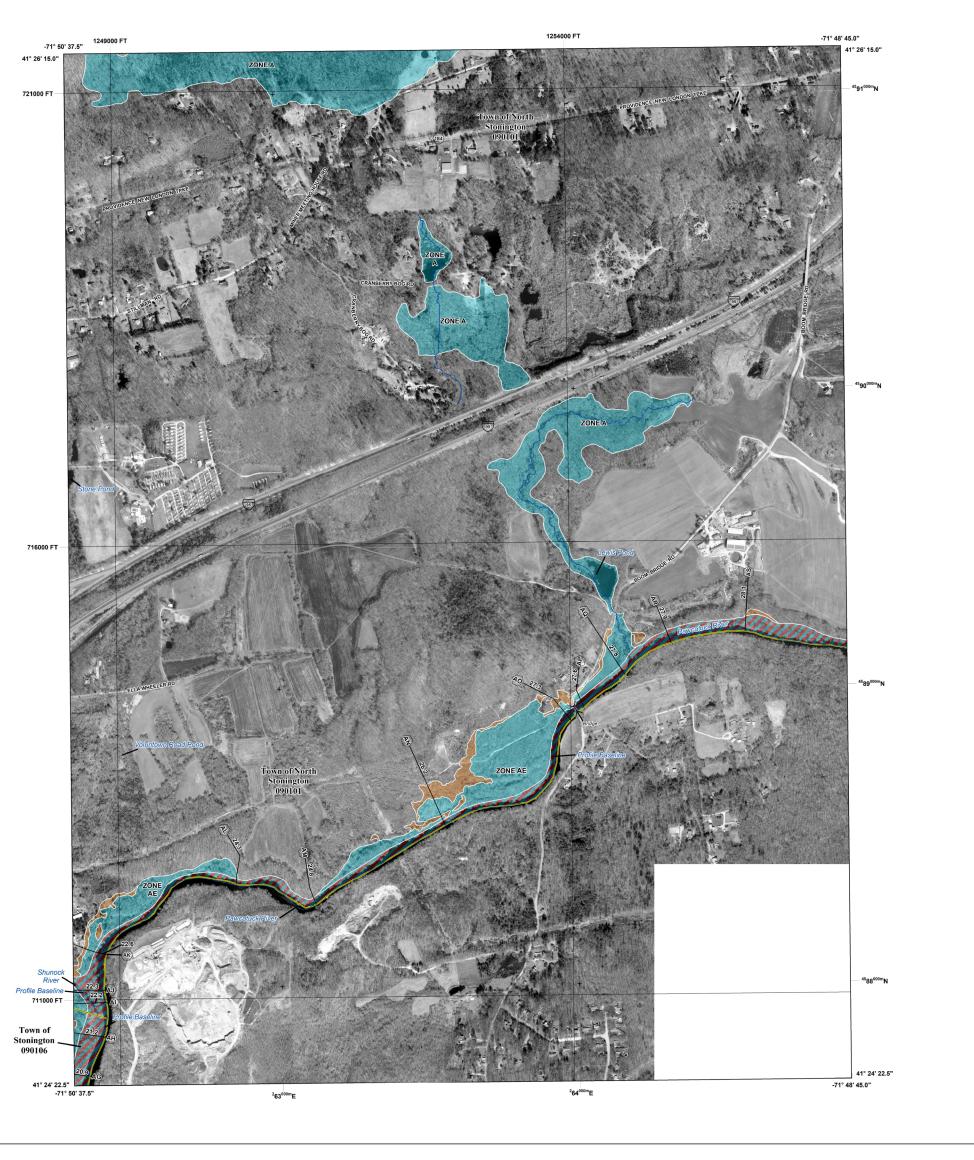


CONTOUR INTERVAL 10 FEET NORTH AMERICAN VERTICAL DATUM OF 1988

U.S. National Grid 100,000 - m Square ID

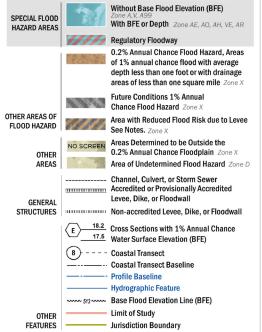


ASHAWAY, RI, CT 2018



#### FLOOD HAZARD INFORMATION

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT THE INFORMATION DEPICTED ON THIS MAP AND SUPPORTING DOCUMENTATION ARE ALSO AVAILABLE IN DIGITAL FORMAT AT HTTP://MSC.FEMA.GOV



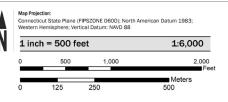
#### **NOTES TO USERS**

Communities annexing land on adjacent FIRM panels must obtain a current copy of the adjacent panel as well as the current FIRM Index. These may be ordered directly from the Map Service Center at the number listed above. For community and countywide map dates refer to the Flood Insurance Study report for this jurisdiction

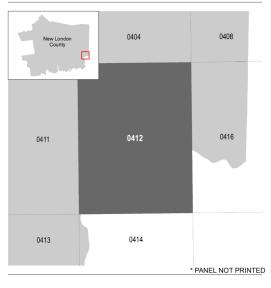
To determine if flood insurance is available in the community, contact your Insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

Base map information shown on this FIRM was provided in digital format in 2016 by the Capitol Region Council of Governments of Connecticut at a 0.25-foot resolution.

#### **SCALE**



#### PANEL LOCATOR

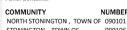


#### NATIONAL FLOOD INSURANCE PROGRAM

**NEW LONDON COUNTY, CT** 



National Flood Insurance Program



NORTH STONINGTON , TOWN OF 090101 STONINGTON , TOWN OF 090106



**VERSION NUMBER** 2.3.3.2 MAP NUMBER 09011C0412H MAP REVISED

April 3, 2020



### Appendix C

NOAA Precipitation Data



#### NOAA Atlas 14, Volume 10, Version 3 Location name: North Stonington, Connecticut, USA\*

Latitude: 41.4343°, Longitude: -71.8216° Elevation: 137.53 ft\*\*



\* source: ESRI Maps \*\* source: USGS

#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

#### PF tabular

F D 3-	6-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup> Average recurrence interval (years)									
Duration	1	2	5	10	25	50	100	200	500	1000
	<u> </u>									
5-min	<b>0.331</b> (0.255-0.430)	<b>0.399</b> (0.307-0.518)	<b>0.511</b> (0.391-0.665)	<b>0.603</b> (0.460-0.789)	<b>0.731</b> (0.541-0.987)	<b>0.826</b> (0.600-1.13)	<b>0.927</b> (0.656-1.31)	<b>1.04</b> (0.699-1.49)	<b>1.21</b> (0.782-1.77)	<b>1.35</b> (0.853-2.00)
10-min	<b>0.469</b> (0.361-0.609)	<b>0.566</b> (0.435-0.735)	<b>0.724</b> (0.554-0.942)	<b>0.855</b> (0.651-1.12)	<b>1.03</b> (0.766-1.40)	<b>1.17</b> (0.850-1.61)	<b>1.31</b> (0.930-1.86)	<b>1.48</b> (0.990-2.11)	<b>1.71</b> (1.11-2.51)	<b>1.91</b> (1.21-2.84)
15-min	<b>0.552</b> (0.424-0.716)	<b>0.666</b> (0.511-0.864)	<b>0.852</b> (0.652-1.11)	<b>1.01</b> (0.766-1.31)	<b>1.22</b> (0.901-1.65)	<b>1.38</b> (0.999-1.89)	<b>1.55</b> (1.09-2.18)	<b>1.74</b> (1.17-2.48)	<b>2.02</b> (1.30-2.95)	<b>2.25</b> (1.42-3.34)
30-min	<b>0.764</b> (0.588-0.992)	<b>0.924</b> (0.710-1.20)	<b>1.19</b> (0.908-1.54)	<b>1.40</b> (1.07-1.83)	<b>1.70</b> (1.26-2.30)	<b>1.92</b> (1.40-2.64)	<b>2.16</b> (1.53-3.05)	<b>2.43</b> (1.63-3.47)	<b>2.82</b> (1.82-4.13)	<b>3.14</b> (1.99-4.66)
60-min	<b>0.977</b> (0.751-1.27)	<b>1.18</b> (0.909-1.54)	<b>1.52</b> (1.16-1.98)	<b>1.80</b> (1.37-2.35)	<b>2.18</b> (1.61-2.95)	<b>2.47</b> (1.79-3.39)	<b>2.78</b> (1.96-3.92)	<b>3.12</b> (2.09-4.45)	<b>3.62</b> (2.34-5.30)	<b>4.03</b> (2.55-5.99)
2-hr	<b>1.28</b> (0.993-1.66)	<b>1.55</b> (1.20-2.01)	<b>1.99</b> (1.53-2.58)	<b>2.36</b> (1.80-3.06)	<b>2.86</b> (2.12-3.84)	<b>3.23</b> (2.36-4.41)	<b>3.63</b> (2.58-5.10)	<b>4.08</b> (2.75-5.79)	<b>4.74</b> (3.08-6.90)	<b>5.29</b> (3.36-7.80)
3-hr	<b>1.50</b> (1.16-1.93)	<b>1.81</b> (1.40-2.33)	<b>2.31</b> (1.79-2.98)	<b>2.73</b> (2.10-3.54)	<b>3.31</b> (2.47-4.43)	<b>3.74</b> (2.74-5.09)	<b>4.20</b> (2.99-5.88)	<b>4.72</b> (3.19-6.67)	<b>5.49</b> (3.57-7.94)	<b>6.12</b> (3.90-8.99)
6-hr	<b>1.93</b> (1.50-2.47)	<b>2.31</b> (1.80-2.96)	<b>2.94</b> (2.28-3.77)	<b>3.46</b> (2.67-4.46)	<b>4.18</b> (3.13-5.56)	<b>4.71</b> (3.46-6.37)	<b>5.28</b> (3.78-7.35)	<b>5.93</b> (4.02-8.32)	<b>6.89</b> (4.50-9.90)	<b>7.69</b> (4.91-11.2)
12-hr	<b>2.42</b> (1.90-3.09)	<b>2.89</b> (2.26-3.68)	<b>3.65</b> (2.84-4.66)	<b>4.28</b> (3.32-5.48)	<b>5.14</b> (3.87-6.81)	<b>5.79</b> (4.28-7.78)	<b>6.48</b> (4.66-8.95)	<b>7.27</b> (4.95-10.1)	<b>8.43</b> (5.53-12.0)	<b>9.39</b> (6.03-13.6)
24-hr	<b>2.87</b> (2.26-3.63)	<b>3.42</b> (2.69-4.34)	<b>4.33</b> (3.39-5.49)	<b>5.08</b> (3.96-6.47)	<b>6.11</b> (4.62-8.04)	<b>6.88</b> (5.11-9.19)	<b>7.70</b> (5.57-10.6)	<b>8.65</b> (5.91-12.0)	<b>10.0</b> (6.61-14.2)	<b>11.2</b> (7.21-16.1)
2-day	<b>3.21</b> (2.54-4.04)	<b>3.86</b> (3.05-4.86)	<b>4.92</b> (3.87-6.21)	<b>5.79</b> (4.54-7.34)	<b>7.00</b> (5.32-9.16)	<b>7.90</b> (5.89-10.5)	<b>8.86</b> (6.44-12.1)	<b>9.97</b> (6.85-13.7)	<b>11.6</b> (7.67-16.3)	<b>12.9</b> (8.37-18.4)
3-day	<b>3.48</b> (2.76-4.36)	<b>4.17</b> (3.30-5.24)	<b>5.30</b> (4.19-6.67)	<b>6.24</b> (4.90-7.88)	<b>7.54</b> (5.74-9.82)	<b>8.50</b> (6.36-11.2)	<b>9.53</b> (6.94-12.9)	<b>10.7</b> (7.37-14.7)	<b>12.4</b> (8.25-17.4)	<b>13.9</b> (8.99-19.7)
4-day	<b>3.72</b> (2.96-4.66)	<b>4.44</b> (3.53-5.57)	<b>5.63</b> (4.45-7.07)	<b>6.61</b> (5.20-8.33)	<b>7.96</b> (6.08-10.3)	<b>8.97</b> (6.72-11.8)	<b>10.0</b> (7.32-13.6)	<b>11.3</b> (7.77-15.4)	<b>13.1</b> (8.68-18.2)	<b>14.5</b> (9.44-20.6)
7-day	<b>4.41</b> (3.52-5.50)	<b>5.20</b> (4.14-6.48)	<b>6.48</b> (5.15-8.10)	<b>7.54</b> (5.96-9.46)	<b>9.00</b> (6.90-11.6)	<b>10.1</b> (7.59-13.2)	<b>11.3</b> (8.23-15.1)	<b>12.6</b> (8.70-17.0)	<b>14.5</b> (9.64-20.1)	<b>16.0</b> (10.4-22.5)
10-day	<b>5.10</b> (4.08-6.34)	<b>5.92</b> (4.73-7.37)	<b>7.26</b> (5.79-9.05)	<b>8.37</b> (6.63-10.5)	<b>9.90</b> (7.60-12.7)	<b>11.1</b> (8.32-14.4)	<b>12.3</b> (8.96-16.4)	<b>13.6</b> (9.44-18.4)	<b>15.5</b> (10.4-21.4)	<b>17.0</b> (11.1-23.9)
20-day	<b>7.23</b> (5.81-8.94)	<b>8.12</b> (6.52-10.0)	<b>9.57</b> (7.66-11.9)	<b>10.8</b> (8.58-13.4)	<b>12.4</b> (9.57-15.8)	<b>13.7</b> (10.3-17.6)	<b>15.0</b> (10.9-19.7)	<b>16.3</b> (11.4-21.8)	<b>18.0</b> (12.1-24.7)	<b>19.3</b> (12.6-26.8)
30-day	<b>9.00</b> (7.26-11.1)	<b>9.94</b> (8.01-12.3)	<b>11.5</b> (9.22-14.2)	<b>12.8</b> (10.2-15.8)	<b>14.5</b> (11.2-18.3)	<b>15.9</b> (12.0-20.3)	<b>17.2</b> (12.5-22.3)	<b>18.5</b> (12.9-24.6)	<b>20.0</b> (13.5-27.3)	<b>21.1</b> (13.9-29.2)
45-day	<b>11.2</b> (9.06-13.8)	<b>12.2</b> (9.87-15.0)	<b>13.9</b> (11.2-17.1)	<b>15.2</b> (12.2-18.8)	<b>17.1</b> (13.2-21.5)	<b>18.6</b> (14.1-23.6)	<b>20.0</b> (14.5-25.8)	<b>21.2</b> (15.0-28.2)	<b>22.7</b> (15.4-30.8)	<b>23.6</b> (15.5-32.5)
60-day	<b>13.0</b> (10.6-16.0)	<b>14.1</b> (11.4-17.3)	<b>15.9</b> (12.8-19.5)	<b>17.3</b> (13.9-21.4)	<b>19.3</b> (15.0-24.2)	<b>21.0</b> (15.8-26.5)	<b>22.5</b> (16.3-28.7)	<b>23.7</b> (16.7-31.3)	<b>25.1</b> (17.0-33.9)	<b>25.9</b> (17.1-35.5)

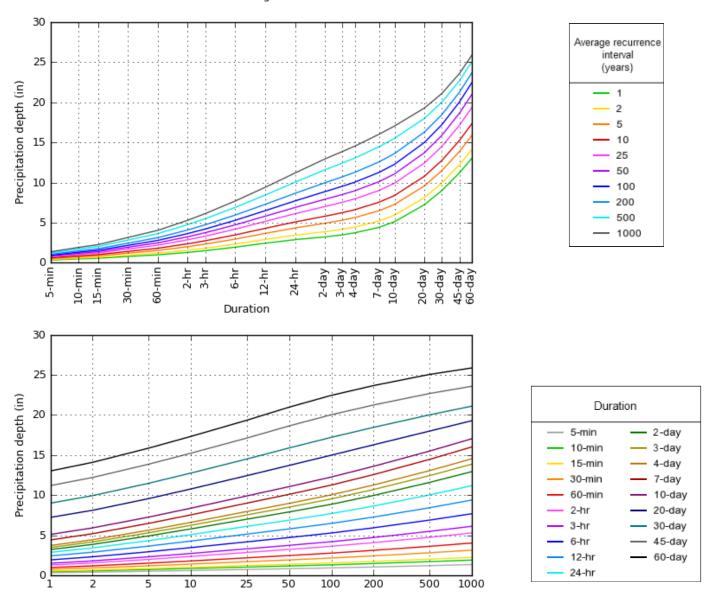
<sup>&</sup>lt;sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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#### PF graphical

#### PDS-based depth-duration-frequency (DDF) curves Latitude: 41.4343°, Longitude: -71.8216°



NOAA Atlas 14, Volume 10, Version 3

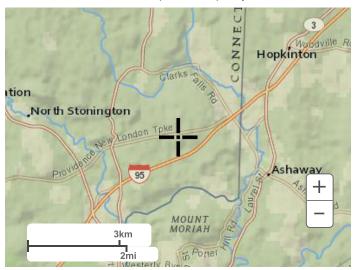
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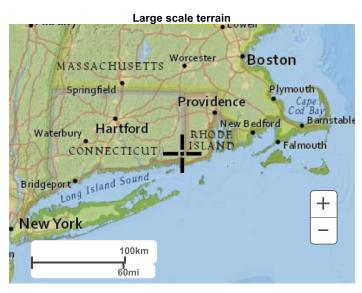
Back to Top

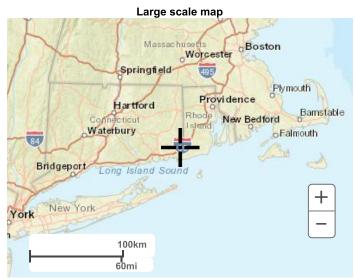
#### Maps & aerials

Small scale terrain

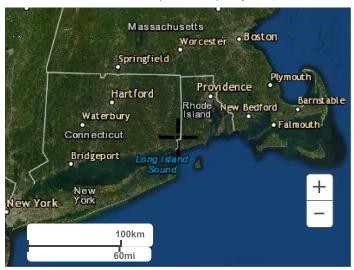
Average recurrence interval (years)







Large scale aerial



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US Department of Commerce

National Oceanic and Atmospheric Administration

National Weather Service

National Water Center

1325 East West Highway
Silver Spring, MD 20910

Questions?: HDSC.Questions@noaa.gov

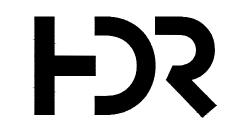
**Disclaimer** 



### Appendix D

Stormwater Drainage Area Map, Peak Flow Calculations, and Pond Design







# NOT FOR CONSTRUCTION

### STONINGTON SOLAR

428, PROVIDENCE-NEW LONDON TURNPIKE NORTH STONINGTON, CT 06359, USA LAT: 41.431830°N LON: 71.821514°W

STONINGTON, CT

3	RE-ISSUED FOR PERMIT	06/25/21
2	RE-ISSUED FOR PERMIT	05/28/21
1	RE-ISSUED FOR PERMIT	02/19/21
0	ISSUED FOR PERMIT	09/30/20
REV. NO	DESCRIPTION	DATE

SHEET TITLE:

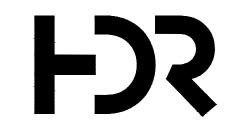
## DRAINAGE AREA EXHIBIT PRE-DEVELOPMENT

	PROJ. MGR.	PROJ. ENGR.	DATE:
	WK	MB	5/28/21
	DRAWN BY:	CHECKED BY:	SCALE:
	NC	CP	1:200

DRAWING NO.

**EXHIBIT** 







# NOT FOR CONSTRUCTION

### STONINGTON SOLAR

428, PROVIDENCE-NEW LONDON TURNPIKE NORTH STONINGTON, CT 06359, USA LAT: 41.431830°N LON: 71.821514°W

STONINGTON, CT

3	RE-ISSUED FOR PERMIT	06/25/21
2	RE-ISSUED FOR PERMIT	05/28/21
1	RE-ISSUED FOR PERMIT	02/19/21
0	ISSUED FOR PERMIT	09/30/20
REV. NO	DESCRIPTION	DATE

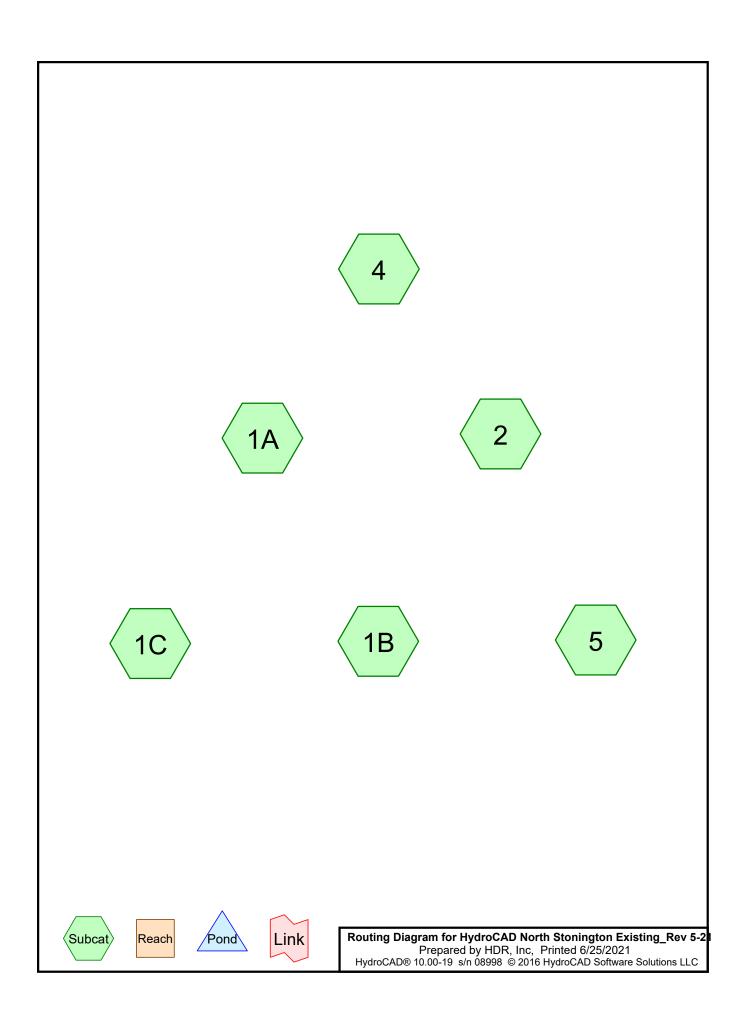
SHEET TITLE:

## DRAINAGE AREA EXHIBIT POST-DEVELOPMENT

	PROJ. MGR.	PROJ. ENGR.	DATE:
	WK	MB	5/28/21
	DRAWN BY:	CHECKED BY:	SCALE:
	NC	CP	1:200

DRAWING NO.

**EXHIBIT** 



HydroCAD North Stonington Existing\_Rev 5-21
Prepared by HDR, Inc
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#### **Area Listing (all nodes)**

Area	CN	Description
(acres)		(subcatchment-numbers)
20.610	60	(1A, 1B, 1C)
3.660	71	(2)
9.020	63	(4)
15.220	70	(5)
48.510	65	TOTAL AREA

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#### Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
0.000	HSG C	
0.000	HSG D	
48.510	Other	1A, 1B, 1C, 2, 4, 5
48.510		TOTAL AREA

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#### **Ground Covers (all nodes)**

 HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground	Subcatchment
(acres)	(acres)	(acres)	(acres)	(acres)	(acres)	Cover	Numbers
0.000 <b>0.000</b>	0.000 <b>0.000</b>	0.000 <b>0.000</b>	0.000 <b>0.000</b>	48.510 <b>48.510</b>	48.510 <b>48.510</b>	TOTAL ARE	

#### HydroCAD North Stonington Existing\_Rev 5-2Type III 24-hr 2-YEAR STORM Rainfall=3.42"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A: Runoff Area=4.190 ac Runoff Depth>0.49"

Tc=55.2 min CN=60 Runoff=0.71 cfs 0.170 af

Subcatchment1B: Runoff Area=4.570 ac Runoff Depth>0.49"

Tc=34.5 min CN=60 Runoff=0.99 cfs 0.187 af

**Subcatchment1C:** Runoff Area=11.850 ac Runoff Depth>0.49"

Tc=41.2 min CN=60 Runoff=2.36 cfs 0.483 af

Subcatchment2: Runoff Area=3.660 ac Runoff Depth>1.00"

Tc=33.0 min CN=71 Runoff=2.18 cfs 0.306 af

Subcatchment4: Runoff Area=9.020 ac Runoff Depth>0.62"

Tc=27.4 min CN=63 Runoff=3.02 cfs 0.463 af

Subcatchment5: Runoff Area=15.220 ac Runoff Depth>0.95"

Tc=48.8 min CN=70 Runoff=6.91 cfs 1.199 af

Total Runoff Area = 48.510 ac Runoff Volume = 2.808 af Average Runoff Depth = 0.69"

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#### **Summary for Subcatchment 1A:**

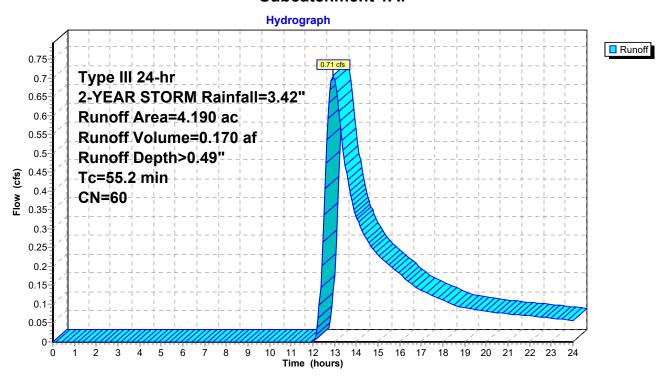
Runoff = 0.71 cfs @ 12.94 hrs, Volume=

0.170 af, Depth> 0.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YEAR STORM Rainfall=3.42"

_	Area	(ac)	CN	Desc	cription		
•	4.	190	60				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	55.2						Direct Entry, NRCS Part 630

#### **Subcatchment 1A:**



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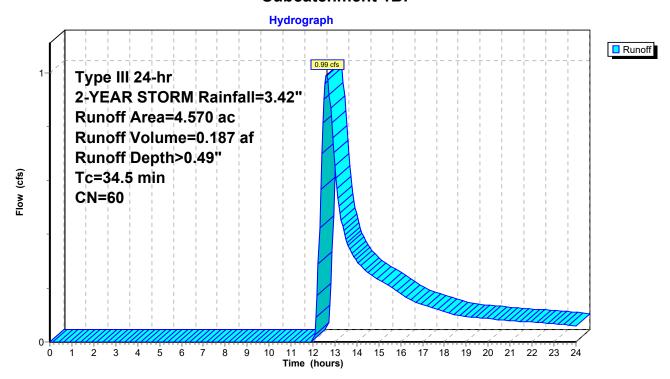
#### **Summary for Subcatchment 1B:**

Runoff = 0.99 cfs @ 12.62 hrs, Volume= 0.187 af, Depth> 0.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YEAR STORM Rainfall=3.42"

_	Area	(ac)	CN	Desc	cription		
*	4.	.570	60				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	34.5			, ,	, ,	, ,	Direct Entry, NRCS Part 630

#### **Subcatchment 1B:**



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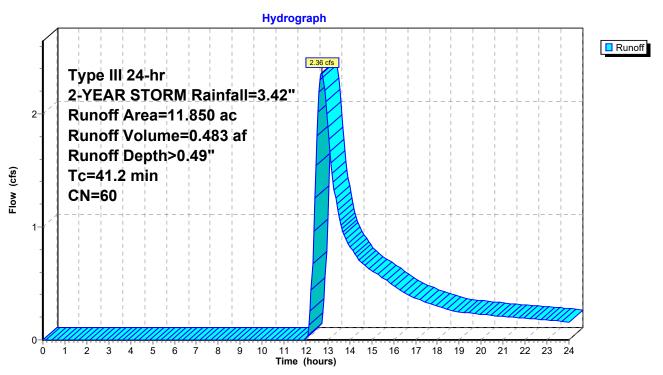
#### **Summary for Subcatchment 1C:**

Runoff = 2.36 cfs @ 12.72 hrs, Volume= 0.483 af, Depth> 0.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YEAR STORM Rainfall=3.42"

_	Area	(ac)	CN	Desc	cription		
*	11.	850	60				
	Tc	Leng	th :	Slope	Velocity	Capacity	Description
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	
	41.2						Direct Entry, NRCS Part 630

#### **Subcatchment 1C:**



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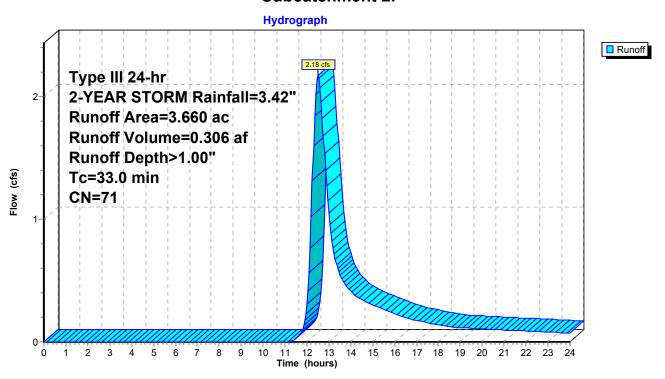
#### **Summary for Subcatchment 2:**

Runoff 2.18 cfs @ 12.51 hrs, Volume= 0.306 af, Depth> 1.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YEAR STORM Rainfall=3.42"

_	Area	(ac)	CN	Desc	cription		
*	3.	660	71				
	Tc	Leng	th	Slope	Velocity	Capacity	Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	33.0						Direct Entry, NRCS Part 630

#### **Subcatchment 2:**



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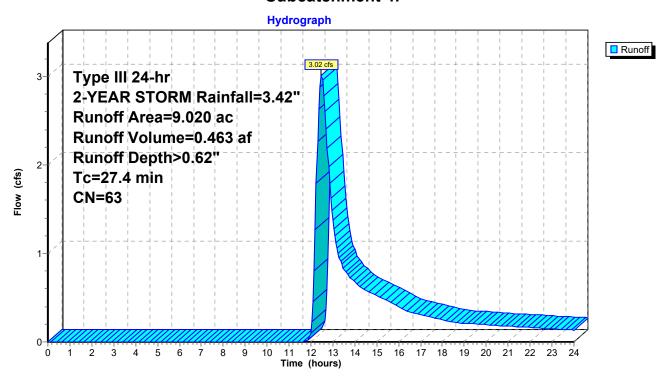
#### **Summary for Subcatchment 4:**

Runoff 3.02 cfs @ 12.48 hrs, Volume= 0.463 af, Depth> 0.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YEAR STORM Rainfall=3.42"

_	Area	(ac)	CN	Desc	cription		
*	9.	020	63				
	Tc	J		•	•		Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	27.4						Direct Entry, NRCS Part 630

#### Subcatchment 4:



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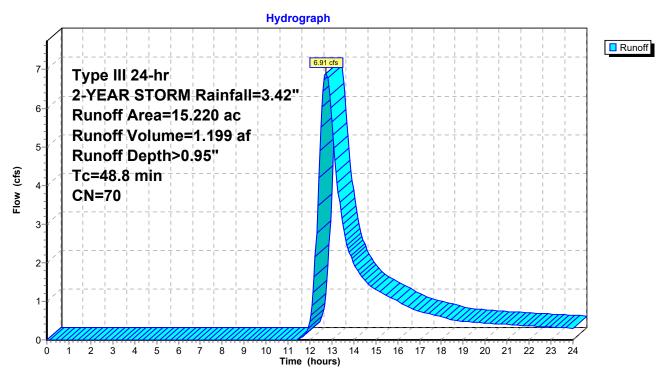
#### **Summary for Subcatchment 5:**

Runoff 6.91 cfs @ 12.74 hrs, Volume= 1.199 af, Depth> 0.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YEAR STORM Rainfall=3.42"

_	Area	(ac)	CN	Desc	cription		
,	15.	.220	70				
_	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	48.8			•	-		Direct Entry, NRCS Part 630

#### **Subcatchment 5:**



#### HydroCAD North Stonington Existing\_Rev 5-Type III 24-hr 10-YEAR STORM Rainfall=5.08"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A: Runoff Area=4.190 ac Runoff Depth>1.33"

Tc=55.2 min CN=60 Runoff=2.45 cfs 0.463 af

Subcatchment1B: Runoff Area=4.570 ac Runoff Depth>1.33"

Tc=34.5 min CN=60 Runoff=3.45 cfs 0.508 af

**Subcatchment1C:** Runoff Area=11.850 ac Runoff Depth>1.33"

Tc=41.2 min CN=60 Runoff=8.18 cfs 1.315 af

Subcatchment2: Runoff Area=3.660 ac Runoff Depth>2.16"

Tc=33.0 min CN=71 Runoff=4.97 cfs 0.659 af

Subcatchment4: Runoff Area=9.020 ac Runoff Depth>1.55"

Tc=27.4 min CN=63 Runoff=9.06 cfs 1.164 af

**Subcatchment5:** Runoff Area=15.220 ac Runoff Depth>2.07"

Tc=48.8 min CN=70 Runoff=16.19 cfs 2.627 af

Total Runoff Area = 48.510 ac Runoff Volume = 6.736 af Average Runoff Depth = 1.67"

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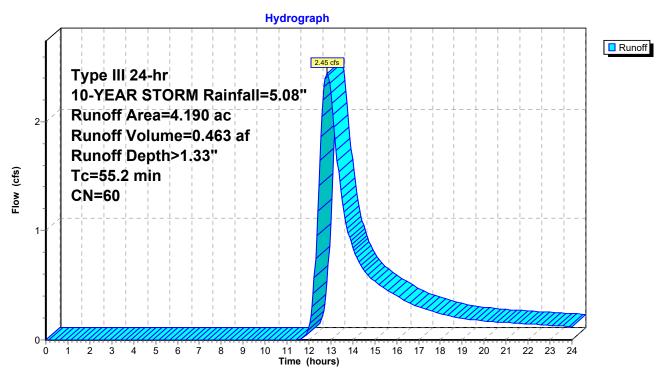
#### **Summary for Subcatchment 1A:**

Runoff 2.45 cfs @ 12.83 hrs, Volume= 0.463 af, Depth> 1.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YEAR STORM Rainfall=5.08"

	Area	(ac)	CN	Desc	cription		
•	<b>*</b> 4.	190	60				
-							
	Тс	Leng	th :	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
-	55.2						Direct Entry, NRCS Part 630

#### **Subcatchment 1A:**



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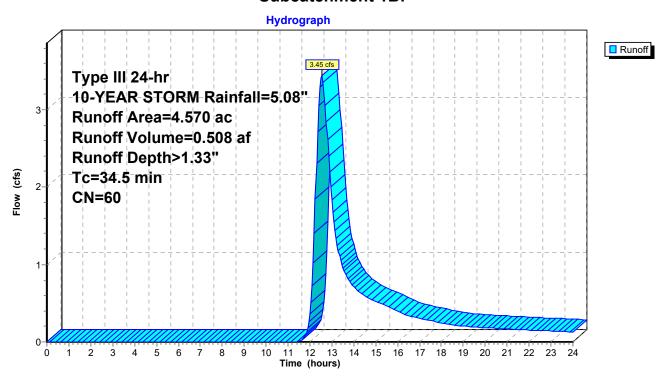
#### **Summary for Subcatchment 1B:**

Runoff 3.45 cfs @ 12.54 hrs, Volume= 0.508 af, Depth> 1.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YEAR STORM Rainfall=5.08"

_	Area	(ac)	CN	Desc	cription		
*	4.	570	60				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	34.5	•		,	,	,	Direct Entry, NRCS Part 630

#### **Subcatchment 1B:**



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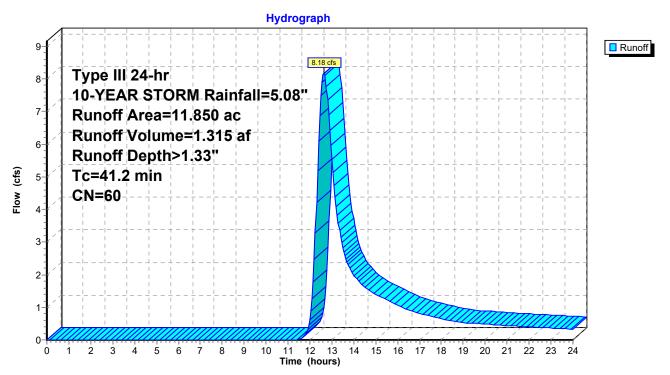
#### **Summary for Subcatchment 1C:**

Runoff 8.18 cfs @ 12.63 hrs, Volume= 1.315 af, Depth> 1.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YEAR STORM Rainfall=5.08"

	Area	(ac)	CN	Desc	cription		
•	<b>'</b> 11.	.850	60				
-							
	Tc	Leng	th :	Slope	Velocity	Capacity	Description
	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	
_	41.2						Direct Entry, NRCS Part 630

#### **Subcatchment 1C:**



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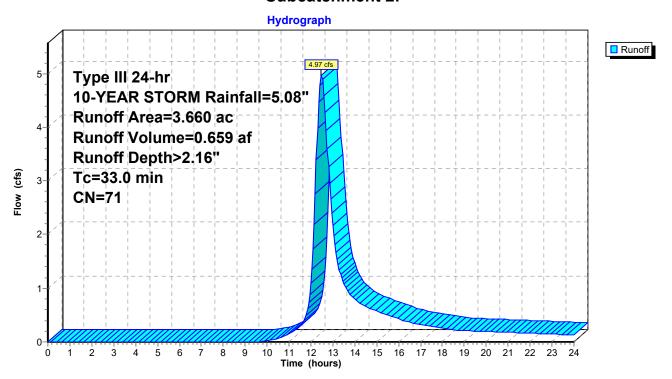
#### **Summary for Subcatchment 2:**

Runoff 4.97 cfs @ 12.48 hrs, Volume= 0.659 af, Depth> 2.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YEAR STORM Rainfall=5.08"

	Area	(ac)	CN	Desc	cription		
•	<b>'</b> 3.	660	71				
-							
	Tc	Leng	th	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
_	33.0						Direct Entry, NRCS Part 630

#### **Subcatchment 2:**



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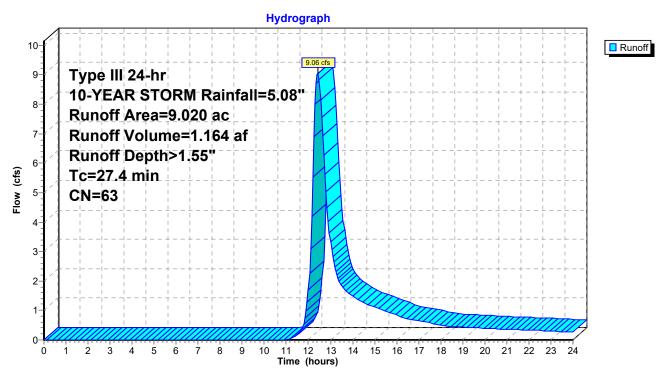
#### **Summary for Subcatchment 4:**

Runoff 9.06 cfs @ 12.42 hrs, Volume= 1.164 af, Depth> 1.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YEAR STORM Rainfall=5.08"

	Area	(ac)	CN	Desc	cription		
*	9.	020	63				
_	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	27.4	(	-/	(1411)	()	()	Direct Entry, NRCS Part 630

#### Subcatchment 4:



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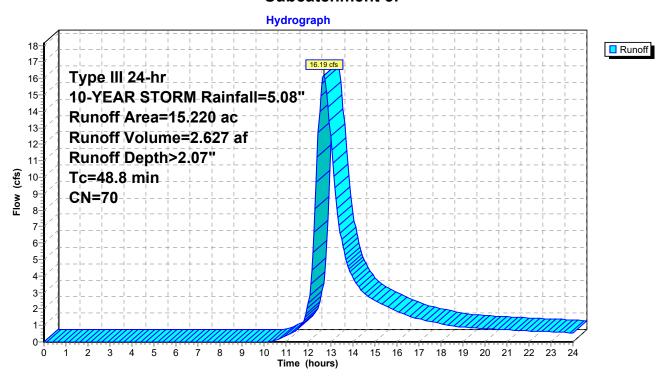
#### **Summary for Subcatchment 5:**

Runoff 16.19 cfs @ 12.70 hrs, Volume= 2.627 af, Depth> 2.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YEAR STORM Rainfall=5.08"

_	Area	(ac)	CN	Desc	cription		
,	15.	.220	70				
_	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	48.8			•	-		Direct Entry, NRCS Part 630

#### Subcatchment 5:



#### HydroCAD North Stonington Existing\_Rev 5-Type III 24-hr 25-YEAR STORM Rainfall=6.11"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A: Runoff Area=4.190 ac Runoff Depth>1.96"

Tc=55.2 min CN=60 Runoff=3.80 cfs 0.686 af

Subcatchment1B: Runoff Area=4.570 ac Runoff Depth>1.98"

Tc=34.5 min CN=60 Runoff=5.35 cfs 0.752 af

**Subcatchment1C:** Runoff Area=11.850 ac Runoff Depth>1.97"

Tc=41.2 min CN=60 Runoff=12.71 cfs 1.947 af

Subcatchment2: Runoff Area=3.660 ac Runoff Depth>2.97"

Tc=33.0 min CN=71 Runoff=6.90 cfs 0.905 af

Subcatchment4: Runoff Area=9.020 ac Runoff Depth>2.24"

Tc=27.4 min CN=63 Runoff=13.54 cfs 1.683 af

Subcatchment5: Runoff Area=15.220 ac Runoff Depth>2.86"

Tc=48.8 min CN=70 Runoff=22.66 cfs 3.628 af

Total Runoff Area = 48.510 ac Runoff Volume = 9.601 af Average Runoff Depth = 2.38"

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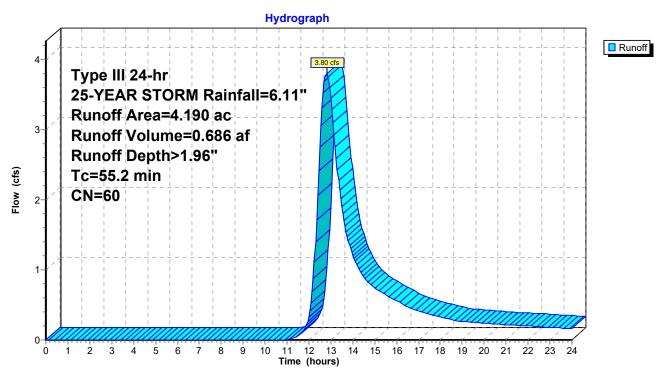
#### **Summary for Subcatchment 1A:**

Runoff 3.80 cfs @ 12.81 hrs, Volume= 0.686 af, Depth> 1.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR STORM Rainfall=6.11"

_	Area	(ac)	CN	Desc	cription		
*	4.	190	60				
	Tc	Leng	th	Slope	Velocity	Capacity	Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	55.2						Direct Entry, NRCS Part 630

#### **Subcatchment 1A:**



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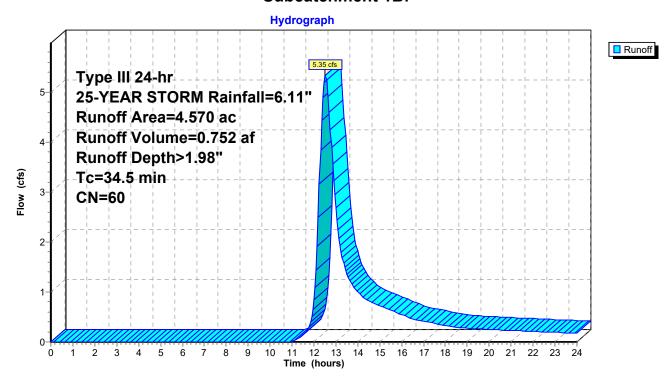
#### **Summary for Subcatchment 1B:**

Runoff 5.35 cfs @ 12.52 hrs, Volume= 0.752 af, Depth> 1.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR STORM Rainfall=6.11"

_	Area	(ac)	CN	Desc	cription		
*	4.	.570	60				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	34.5			, ,	, ,	, ,	Direct Entry, NRCS Part 630

#### **Subcatchment 1B:**



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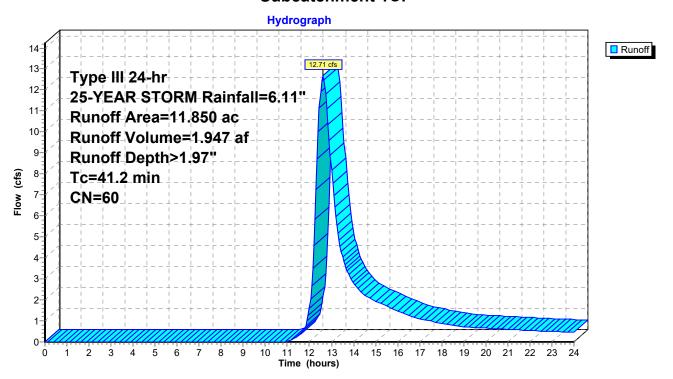
#### **Summary for Subcatchment 1C:**

Runoff 12.71 cfs @ 12.61 hrs, Volume= 1.947 af, Depth> 1.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR STORM Rainfall=6.11"

_	Area	(ac)	CN	Desc	cription		
,	11.	.850	60				
_							
	Tc	Leng	ıth -	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	41 2						Direct Entry NRCS Part 630

#### **Subcatchment 1C:**



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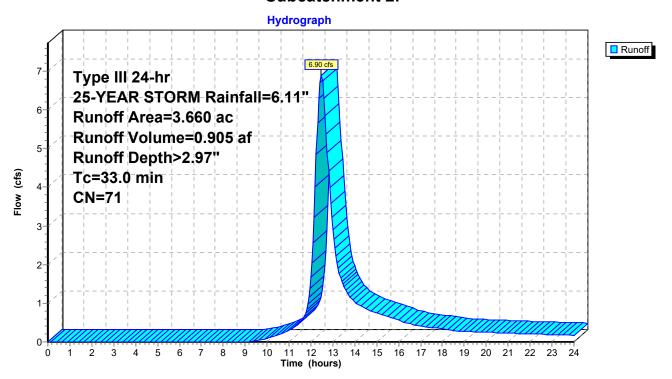
## **Summary for Subcatchment 2:**

Runoff 6.90 cfs @ 12.47 hrs, Volume= 0.905 af, Depth> 2.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR STORM Rainfall=6.11"

_	Area	(ac)	CN	Desc	cription		
*	3.	660	71				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	33.0						Direct Entry, NRCS Part 630

#### **Subcatchment 2:**



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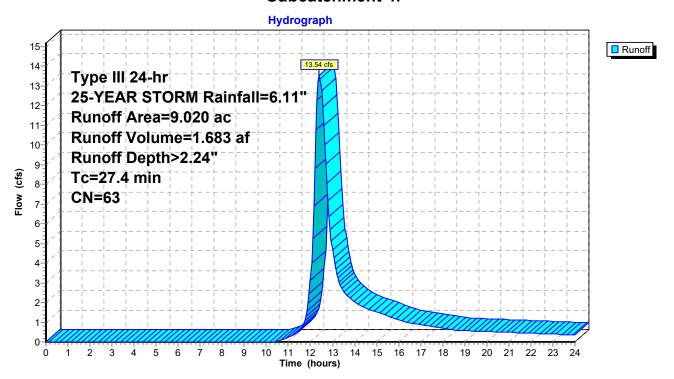
# **Summary for Subcatchment 4:**

Runoff 13.54 cfs @ 12.41 hrs, Volume= 1.683 af, Depth> 2.24"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR STORM Rainfall=6.11"

_	Area	(ac)	CN	Desc	cription		
4	9.	020	63				
_							
	Тс	Leng	th S	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
_	27.4	•	•				Direct Entry, NRCS Part 630

#### Subcatchment 4:



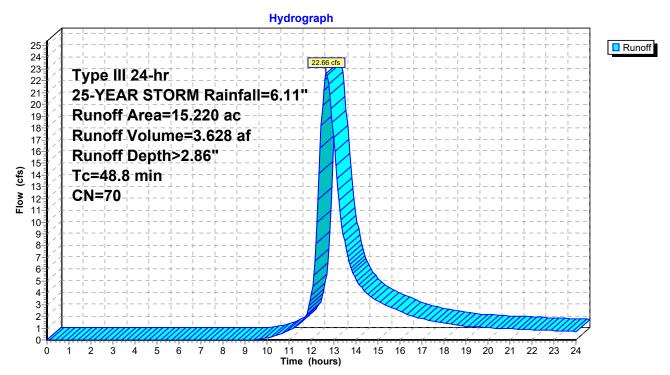
## **Summary for Subcatchment 5:**

Runoff 22.66 cfs @ 12.68 hrs, Volume= 3.628 af, Depth> 2.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR STORM Rainfall=6.11"

_	Area	(ac)	CN	Desc	cription		
•	' 15.	.220	70				
	Tc (min)	Lengt (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	1Q Q						Direct Entry NDCS Part 630

#### Subcatchment 5:



# HydroCAD North Stonington Existing\_Rev 5-Type III 24-hr 50-YEAR STORM Rainfall=6.88"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A: Runoff Area=4.190 ac Runoff Depth>2.48"

Tc=55.2 min CN=60 Runoff=4.91 cfs 0.867 af

Subcatchment1B: Runoff Area=4.570 ac Runoff Depth>2.50"

Tc=34.5 min CN=60 Runoff=6.89 cfs 0.951 af

**Subcatchment1C:** Runoff Area=11.850 ac Runoff Depth>2.49"

Tc=41.2 min CN=60 Runoff=16.38 cfs 2.462 af

Subcatchment2: Runoff Area=3.660 ac Runoff Depth>3.60"

Tc=33.0 min CN=71 Runoff=8.39 cfs 1.097 af

Subcatchment4: Runoff Area=9.020 ac Runoff Depth>2.79"

Tc=27.4 min CN=63 Runoff=17.12 cfs 2.100 af

Subcatchment5: Runoff Area=15.220 ac Runoff Depth>3.48"

Tc=48.8 min CN=70 Runoff=27.73 cfs 4.416 af

Total Runoff Area = 48.510 ac Runoff Volume = 11.892 af Average Runoff Depth = 2.94"

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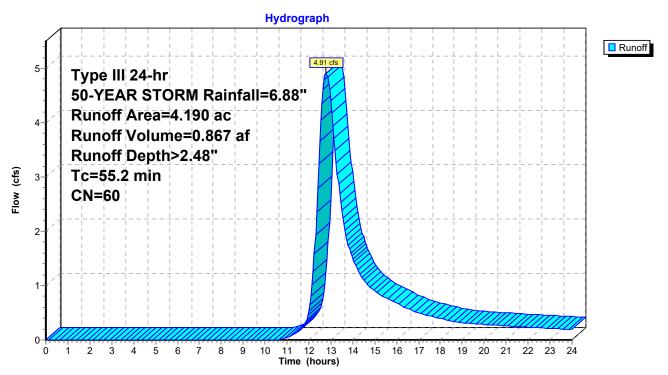
## **Summary for Subcatchment 1A:**

Runoff 4.91 cfs @ 12.80 hrs, Volume= 0.867 af, Depth> 2.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YEAR STORM Rainfall=6.88"

_	Area	(ac)	CN	Desc	cription		
•	4.	190	60				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	55.2						Direct Entry, NRCS Part 630

#### **Subcatchment 1A:**



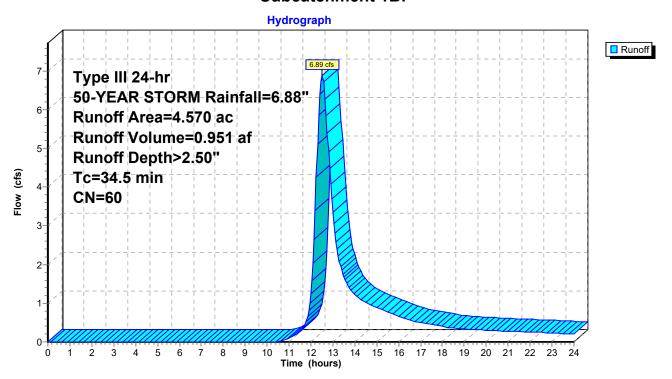
# **Summary for Subcatchment 1B:**

Runoff 6.89 cfs @ 12.51 hrs, Volume= 0.951 af, Depth> 2.50"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YEAR STORM Rainfall=6.88"

	Area	(ac)	CN	Desc	cription		
•	<b>'</b> 4.	570	60				
-							
	Tc	Leng	th S	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
_	34.5						Direct Entry, NRCS Part 630

#### **Subcatchment 1B:**



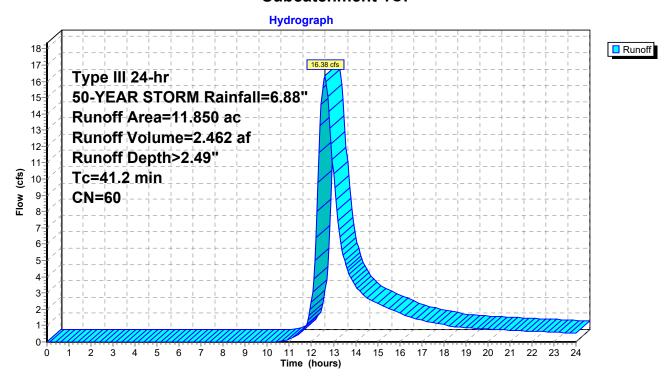
## **Summary for Subcatchment 1C:**

Runoff 16.38 cfs @ 12.60 hrs, Volume= 2.462 af, Depth> 2.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YEAR STORM Rainfall=6.88"

	Area	(ac)	CN	Desc	cription		
•	<b>'</b> 11.	.850	60				
-							
	Tc	Leng	th :	Slope	Velocity	Capacity	Description
	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	
_	41.2						Direct Entry, NRCS Part 630

### **Subcatchment 1C:**



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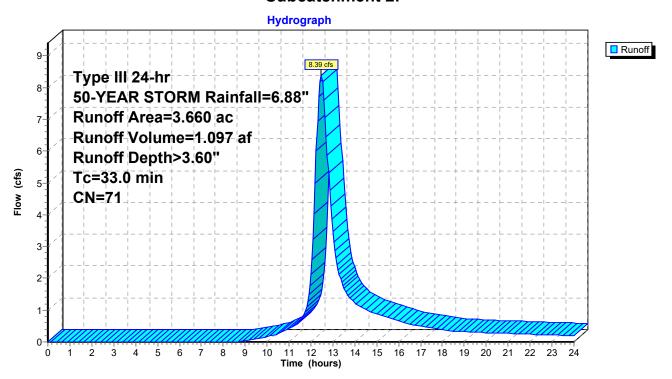
# **Summary for Subcatchment 2:**

Runoff 8.39 cfs @ 12.46 hrs, Volume= 1.097 af, Depth> 3.60"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YEAR STORM Rainfall=6.88"

Area	(ac)	CN	Desc	cription		
* 3.	.660	71				
Tc	Leng	th	Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
33.0						Direct Entry NRCS Part 630

### **Subcatchment 2:**



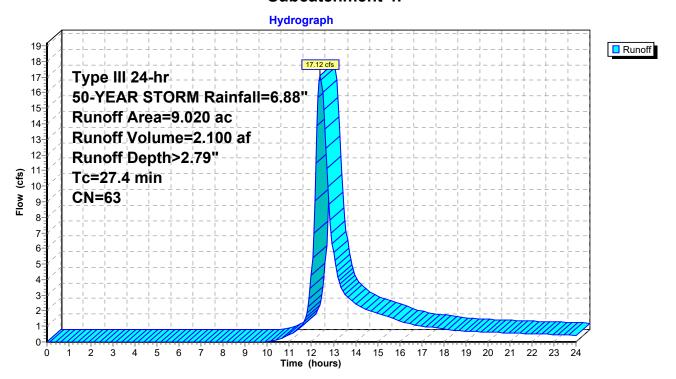
## **Summary for Subcatchment 4:**

Runoff 17.12 cfs @ 12.40 hrs, Volume= 2.100 af, Depth> 2.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YEAR STORM Rainfall=6.88"

Area	(ac)	CN	Desc	cription		
* 9	.020	63				
Tc	Leng	th S	Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
27 4						Direct Entry NRCS Part 630

#### Subcatchment 4:



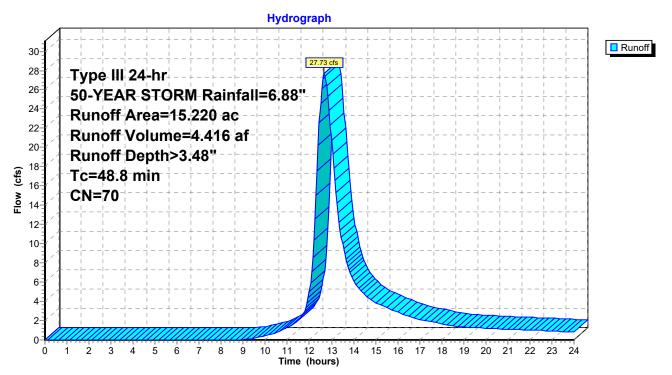
# **Summary for Subcatchment 5:**

Runoff 27.73 cfs @ 12.67 hrs, Volume= 4.416 af, Depth> 3.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YEAR STORM Rainfall=6.88"

Area	(ac)	CN	Desc	cription		
<sup>*</sup> 15.	.220	70				
Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
48.8						Direct Entry, NRCS Part 630

#### **Subcatchment 5:**



# HydroCAD North Stonington Existing\_Rev 5 ype III 24-hr 100-YEAR STORM Rainfall=7.70"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A: Runoff Area=4.190 ac Runoff Depth>3.07"

Tc=55.2 min CN=60 Runoff=6.15 cfs 1.071 af

Subcatchment1B: Runoff Area=4.570 ac Runoff Depth>3.08"

Tc=34.5 min CN=60 Runoff=8.62 cfs 1.175 af

**Subcatchment1C:** Runoff Area=11.850 ac Runoff Depth>3.08"

Tc=41.2 min CN=60 Runoff=20.49 cfs 3.041 af

Subcatchment2: Runoff Area=3.660 ac Runoff Depth>4.29"

Tc=33.0 min CN=71 Runoff=10.02 cfs 1.309 af

Subcatchment4: Runoff Area=9.020 ac Runoff Depth>3.41"

Tc=27.4 min CN=63 Runoff=21.11 cfs 2.566 af

Subcatchment5: Runoff Area=15.220 ac Runoff Depth>4.16"

Tc=48.8 min CN=70 Runoff=33.24 cfs 5.282 af

Total Runoff Area = 48.510 ac Runoff Volume = 14.443 af Average Runoff Depth = 3.57"

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## **Summary for Subcatchment 1A:**

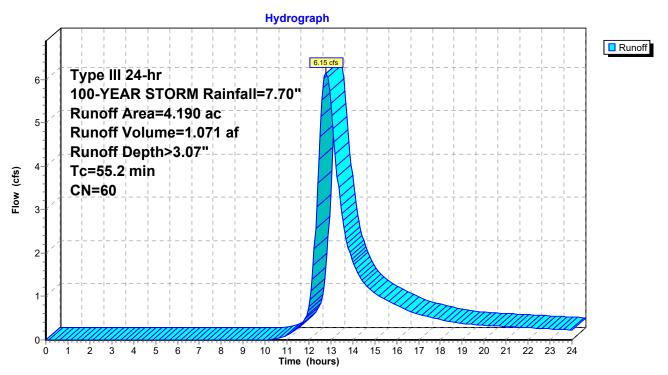
Runoff = 6.15 cfs @ 12.79 hrs, Volume=

1.071 af, Depth> 3.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YEAR STORM Rainfall=7.70"

_	Area	(ac)	CN	Desc	cription		
4	4.	190	60				
_		_					
	Tc	Leng	ıth	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
_	55.2				•		Direct Entry NRCS Part 630

#### **Subcatchment 1A:**



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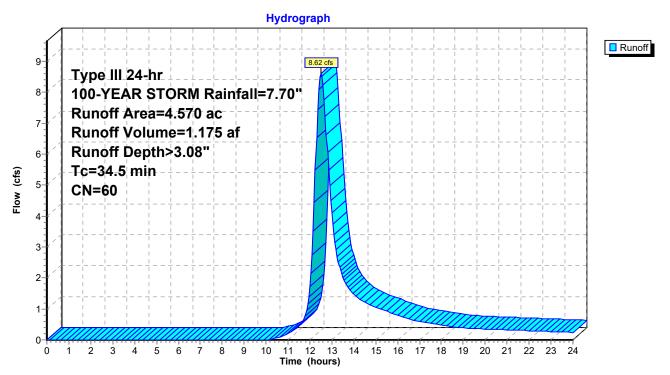
## **Summary for Subcatchment 1B:**

Runoff = 8.62 cfs @ 12.50 hrs, Volume= 1.175 af, Depth> 3.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YEAR STORM Rainfall=7.70"

_	Area	(ac)	CN	Desc	cription		
,	4.	.570	60				
-							
	Tc	Leng	th :	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
-	34.5			•		-	Direct Entry NRCS Part 630

#### **Subcatchment 1B:**



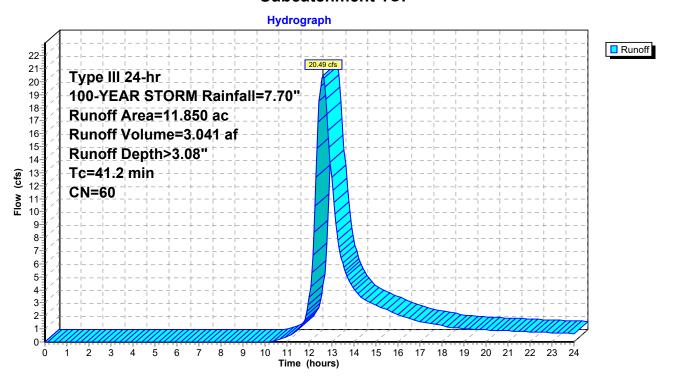
## **Summary for Subcatchment 1C:**

Runoff 20.49 cfs @ 12.60 hrs, Volume= 3.041 af, Depth> 3.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YEAR STORM Rainfall=7.70"

Area	(ac)	CN	Desc	cription		
* 11.	.850	60				
Тс	Leng	th S	Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	·
11.2		,	,			Direct Entry NPCS Part 630

### **Subcatchment 1C:**



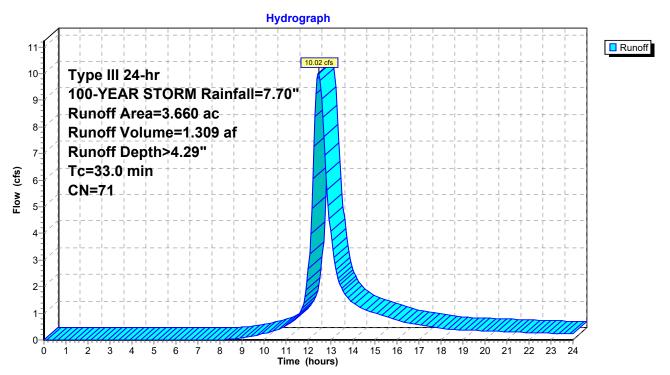
# **Summary for Subcatchment 2:**

Runoff 10.02 cfs @ 12.46 hrs, Volume= 1.309 af, Depth> 4.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YEAR STORM Rainfall=7.70"

	Area	(ac)	CN	Desc	cription		
*	3.	660	71				
	Tc	Leng	th	Slope	Velocity	Capacity	Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	33.0						Direct Entry, NRCS Part 630

#### **Subcatchment 2:**



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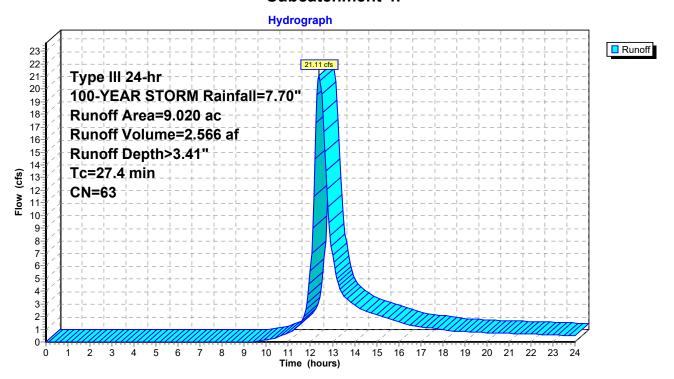
# **Summary for Subcatchment 4:**

Runoff 21.11 cfs @ 12.40 hrs, Volume= 2.566 af, Depth> 3.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YEAR STORM Rainfall=7.70"

Area	(ac)	CN	Desc	cription		
* 9.	.020	63				
Tc	Leng	th S	Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
27 4					•	Direct Entry NRCS Part 630

### Subcatchment 4:



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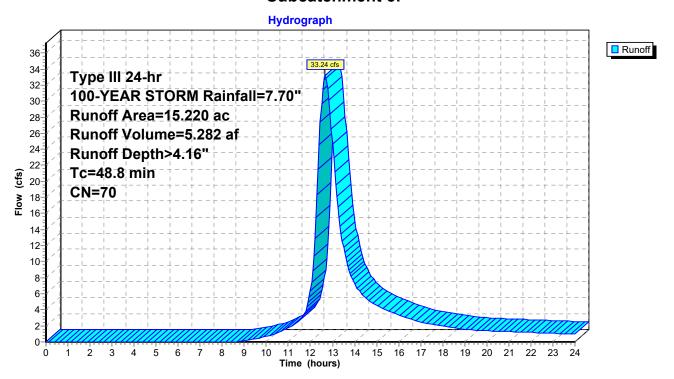
## **Summary for Subcatchment 5:**

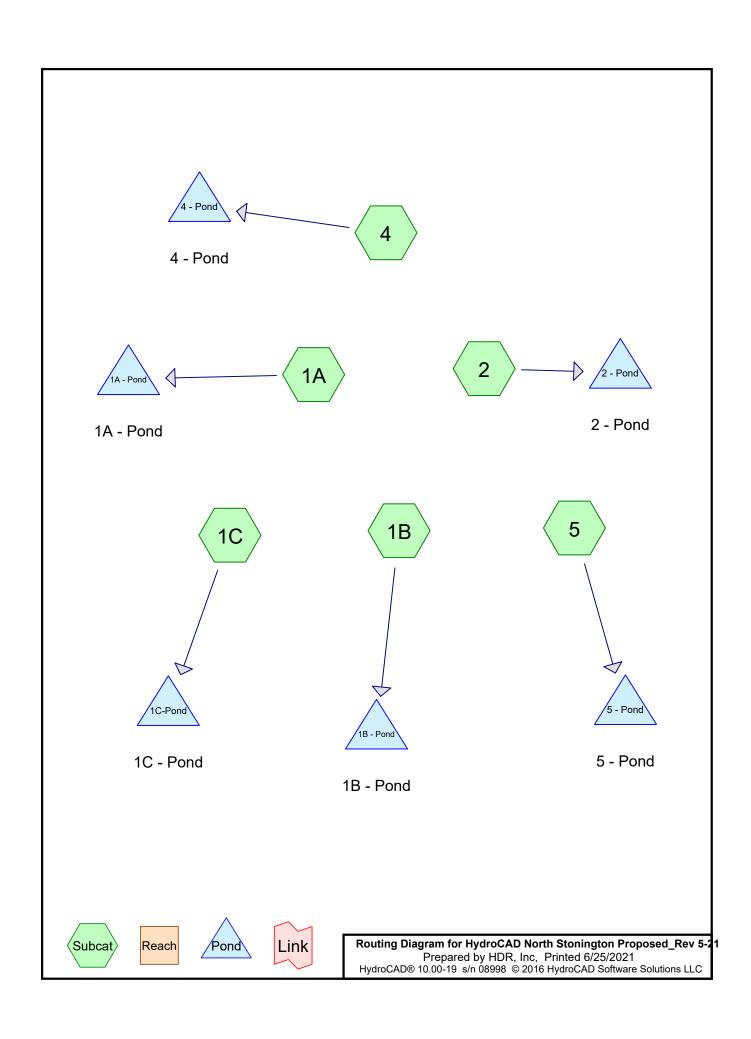
Runoff = 33.24 cfs @ 12.67 hrs, Volume= 5.282 af, Depth> 4.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YEAR STORM Rainfall=7.70"

	Area	(ac)	CN	Desc	cription		
•	' 15.	.220	70				
-	Тс	Leng	th S	Slope	Velocity	Capacity	Description
	(min)	(fee		(ft/ft)	(ft/sec)	(cfs)	'
	48.8					-	Direct Entry NRCS Part 630

### **Subcatchment 5:**





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# **Area Listing (all nodes)**

Area	CN	Description
(acres)		(subcatchment-numbers)
4.190	77	(1A)
4.570	81	(1B)
11.850	83	(1C)
3.660	82	(2)
9.080	75	(4)
15.220	85	(5)
48.570	81	TOTAL AREA

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# Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
0.000	HSG C	
0.000	HSG D	
48.570	Other	1A, 1B, 1C, 2, 4, 5
48.570		TOTAL AREA

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# **Ground Covers (all nodes)**

	0.000 <b>0.000</b>	0.000 <b>0.000</b>	0.000 <b>0.000</b>	0.000 <b>0.000</b>	48.570 <b>48.570</b>	48.570 <b>48.570</b>	TOTAL AF	1A, 1B, 1C, 2, 4, 5
_	, ,	,	,	,	,	()	COVEI	
	(acres)	(acres)	(acres)	(acres)	(acres)	(acres)	Cover	Numbers
	HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground	Subcatchment

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# Pipe Listing (all nodes)

Line#	Node	In-Invert	Out-Invert	Length	Slope	n	Diam/Width	Height	Inside-Fill	
	Number	(feet)	(feet)	(feet)	(ft/ft)		(inches)	(inches)	(inches)	
 1	1A - Pond	125.80	123.80	401.4	0.0050	0.012	24.0	0.0	0.0	
2	1B - Pond	120.20	119.00	88.0	0.0136	0.012	15.0	0.0	0.0	
3	1C-Pond	115.70	115.00	91.6	0.0076	0.012	18.0	0.0	0.0	
4	2 - Pond	170.50	170.00	42.0	0.0119	0.012	12.0	0.0	0.0	
5	4 - Pond	120.40	120.00	53.0	0.0075	0.012	18.0	0.0	0.0	
6	5 - Pond	121.30	115.25	81.5	0.0742	0.012	24.0	0.0	0.0	

# HydroCAD North Stonington Proposed\_Rev 5Type III 24-hr 2-YEAR STORM Rainfall=3.42"

Prepared by HDR, Inc

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A: Runoff Area=4.190 ac Runoff Depth>1.37"

Tc=13.2 min CN=77 Runoff=5.18 cfs 0.477 af

Subcatchment1B: Runoff Area=4.570 ac Runoff Depth>1.64"

Tc=18.7 min CN=81 Runoff=6.05 cfs 0.624 af

Subcatchment1C: Runoff Area=11.850 ac Runoff Depth>1.78"

Tc=19.3 min CN=83 Runoff=16.97 cfs 1.762 af

Subcatchment2: Runoff Area=3.660 ac Runoff Depth>1.71"

Tc=16.2 min CN=82 Runoff=5.35 cfs 0.522 af

Subcatchment4: Runoff Area=9.080 ac Runoff Depth>1.24"

Tc=12.4 min CN=75 Runoff=10.24 cfs 0.940 af

Subcatchment5: Runoff Area=15.220 ac Runoff Depth>1.94"

Tc=15.3 min CN=85 Runoff=26.00 cfs 2.462 af

**Pond 1A - Pond: 1A - Pond**Peak Elev=126.93' Storage=9,488 cf Inflow=5.18 cfs 0.477 af

Primary=0.83 cfs 0.335 af Secondary=0.00 cfs 0.000 af Outflow=0.83 cfs 0.335 af

Pond 1B - Pond: 1B - Pond Peak Elev=121.11' Storage=14,279 cf Inflow=6.05 cfs 0.624 af

Primary=0.77 cfs 0.414 af Secondary=0.00 cfs 0.000 af Outflow=0.77 cfs 0.414 af

Pond 1C-Pond: 1C - Pond Peak Elev=116.83' Storage=41,248 cf Inflow=16.97 cfs 1.762 af

Primary=2.22 cfs 1.141 af Secondary=0.00 cfs 0.000 af Outflow=2.22 cfs 1.141 af

**Pond 2 - Pond: 2 - Pond**Peak Elev=172.68' Storage=14,084 cf Inflow=5.35 cfs 0.522 af

Primary=0.34 cfs 0.300 af Secondary=0.00 cfs 0.000 af Outflow=0.34 cfs 0.300 af

Pond 4 - Pond: 4 - Pond Peak Elev=123.22' Storage=28,735 cf Inflow=10.24 cfs 0.940 af

Primary=0.34 cfs 0.317 af Secondary=0.00 cfs 0.000 af Outflow=0.34 cfs 0.317 af

**Pond 5 - Pond: 5 - Pond**Peak Elev=123.16' Storage=57,476 cf Inflow=26.00 cfs 2.462 af

Primary=3.15 cfs 1.811 af Secondary=0.00 cfs 0.000 af Outflow=3.15 cfs 1.811 af

Total Runoff Area = 48.570 ac Runoff Volume = 6.788 af Average Runoff Depth = 1.68"

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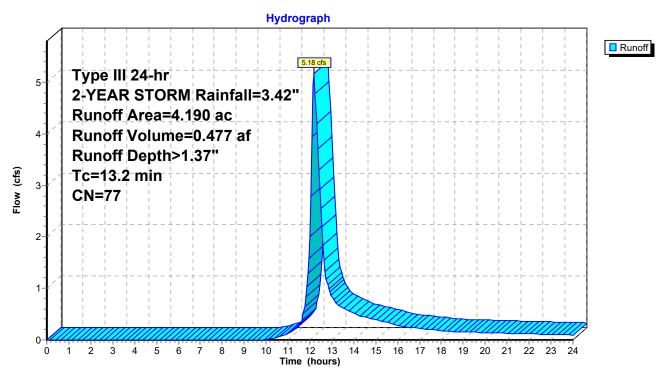
## **Summary for Subcatchment 1A:**

Runoff 5.18 cfs @ 12.19 hrs, Volume= 0.477 af, Depth> 1.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YEAR STORM Rainfall=3.42"

	Area	(ac)	CN	Desc	cription		
*	4.	190	77				
	Tc	Leng	th	Slope	Velocity	Capacity	Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
_	13.2						Direct Entry, NRCS Part 630

#### **Subcatchment 1A:**



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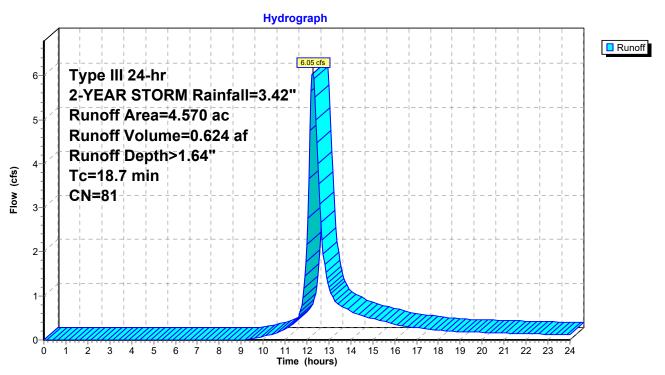
# **Summary for Subcatchment 1B:**

Runoff = 6.05 cfs @ 12.26 hrs, Volume= 0.624 af, Depth> 1.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YEAR STORM Rainfall=3.42"

	Area	(ac)	CN	Desc	cription		
*	4.	570	81				
	Tc	Leng	th	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	18.7						Direct Entry, NRCS Part 630

#### **Subcatchment 1B:**



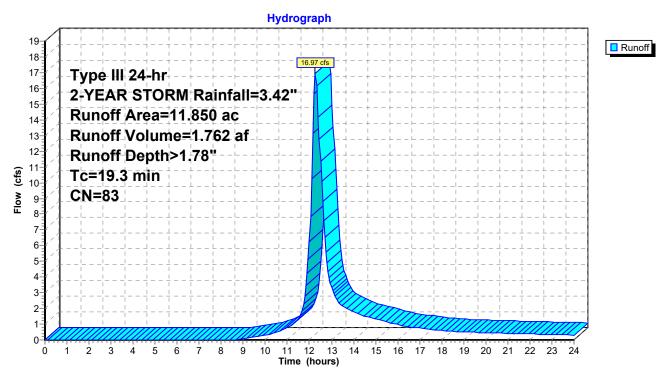
## **Summary for Subcatchment 1C:**

Runoff 16.97 cfs @ 12.27 hrs, Volume= 1.762 af, Depth> 1.78"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YEAR STORM Rainfall=3.42"

_	Area	(ac)	CN	Desc	cription		
•	<b>'</b> 11.	.850	83				
-	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	19.3						Direct Entry, NRCS Part 630

#### **Subcatchment 1C:**



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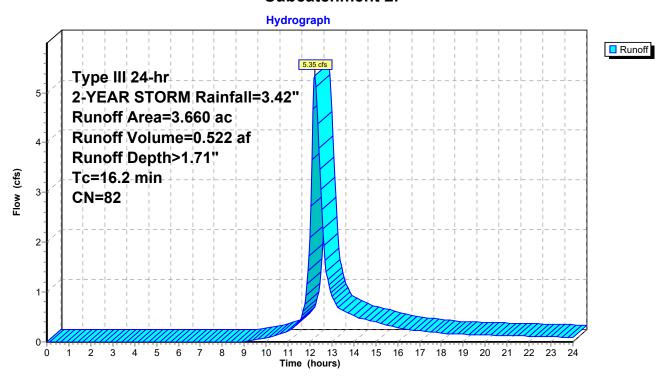
## **Summary for Subcatchment 2:**

Runoff 5.35 cfs @ 12.23 hrs, Volume= 0.522 af, Depth> 1.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YEAR STORM Rainfall=3.42"

	Area	(ac)	CN	Desc	cription		
*	3.	660	82				
	т.		41-	01	\/-li+.	0	Decembrish
	Tc	J			,	. ,	Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	16.2						Direct Entry, NRCS Part 630

#### **Subcatchment 2:**



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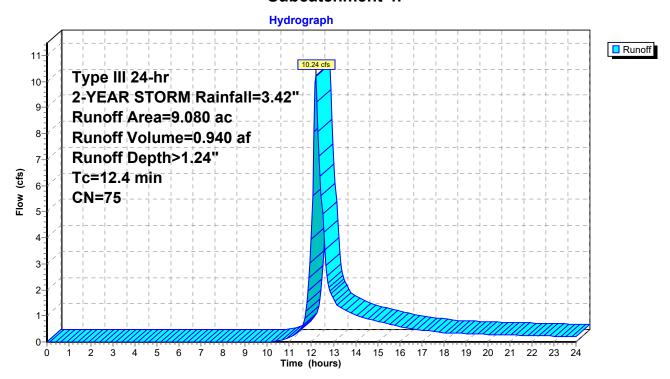
## **Summary for Subcatchment 4:**

Runoff 10.24 cfs @ 12.18 hrs, Volume= 0.940 af, Depth> 1.24"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YEAR STORM Rainfall=3.42"

_	Area	(ac)	CN	Desc	cription		
*	9.	080	75				
	Тс	Leng	th	Slope	Velocity	Capacity	Description
_	(min)	(fee		(ft/ft)	(ft/sec)	(cfs)	
_	12.4		•		•		Direct Entry, NRCS Part 630

### Subcatchment 4:



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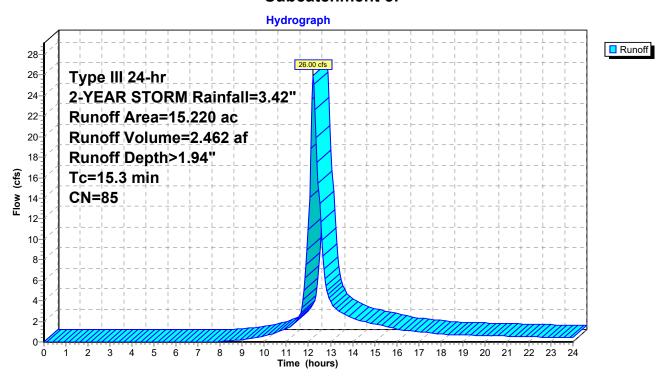
# **Summary for Subcatchment 5:**

Runoff = 26.00 cfs @ 12.21 hrs, Volume= 2.462 af, Depth> 1.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YEAR STORM Rainfall=3.42"

_	Area	(ac)	CN	Desc	cription		
•	15.	220	85				
-							
	Tc	Leng	th	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
-	15.3	•			•		Direct Entry, NRCS Part 630

### **Subcatchment 5:**



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## **Summary for Pond 1A - Pond: 1A - Pond**

Inflow Area = 4.190 ac, Inflow Depth > 1.37" for 2-YEAR STORM event
Inflow = 5.18 cfs @ 12.19 hrs, Volume= 0.477 af

Outflow = 0.83 cfs @ 13.01 hrs, Volume= 0.335 af, Atten= 84%, Lag= 48.7 min

Primary = 0.83 cfs @ 13.01 hrs, Volume= 0.335 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 126.93' @ 13.01 hrs Surf.Area= 4,377 sf Storage= 9,488 cf

Plug-Flow detention time= 199.6 min calculated for 0.335 af (70% of inflow)

Center-of-Mass det. time= 100.9 min ( 954.5 - 853.7 )

Volume	Invert	Avail.Storage	Storage Description
#1	123.00'	37,272 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation Surf.Area		Inc.Store	Cum.Store	
	(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
	123.00	692	0	0
	124.00	1,464	1,078	1,078
	125.00	2,382	1,923	3,001
	126.00	3,381	2,882	5,883
	127.00	4,452	3,917	9,799
	128.00	5,614	5,033	14,832
	129.00	6,826	6,220	21,052
	130.00	8,095	7,461	28,513
	131.00	9.424	8.760	37.272

Device	Routing	Invert	Outlet Devices
#1	Secondary	130.90'	20.0' long x 12.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#2 Primary 125.80' <b>24.0" Round Culvert</b>			24.0" Round Culvert
			L= 401.4' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 125.80' / 123.80' S= 0.0050 '/' Cc= 0.900
			n= 0.012, Flow Area= 3.14 sf
#3	Device 2	130.50'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 2	125.90'	6.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=0.83 cfs @ 13.01 hrs HW=126.93' (Free Discharge)

**—2=Culvert** (Passes 0.83 cfs of 6.04 cfs potential flow)

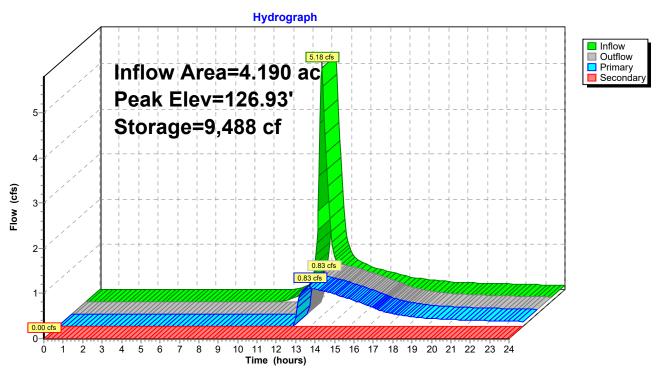
3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

4=Orifice/Grate (Orifice Controls 0.83 cfs @ 4.25 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=123.00' (Free Discharge)
1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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## Pond 1A - Pond: 1A - Pond



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## Summary for Pond 1B - Pond: 1B - Pond

Inflow Area = 4.570 ac, Inflow Depth > 1.64" for 2-YEAR STORM event

Inflow 6.05 cfs @ 12.26 hrs, Volume= 0.624 af

0.77 cfs @ 13.57 hrs, Volume= Outflow 0.414 af, Atten= 87%, Lag= 78.4 min

0.77 cfs @ 13.57 hrs, Volume= Primary 0.414 af 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 121.11' @ 13.57 hrs Surf.Area= 8,000 sf Storage= 14,279 cf

Plug-Flow detention time= 247.6 min calculated for 0.414 af (66% of inflow)

Center-of-Mass det. time= 145.9 min ( 991.6 - 845.7 )

Volume	Invert	Avail.Storage	Storage Description
#1	119.00'	83,261 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
119.00	5,600	0	0
120.00	6,708	6,154	6,154
121.00	7,871	7,290	13,444
122.00	9,092	8,482	21,925
123.00	10,369	9,731	31,656
124.00	11,703	11,036	42,692
125.00	12,160	11,932	54,623
126.00	14,538	13,349	67,972
127.00	16,040	15,289	83,261

Device	Routing	Invert	Outlet Devices	
#1	Primary	120.20'	15.0" Round Culvert	
	•		L= 88.0' RCP, square edge headwall, Ke= 0.500	
			Inlet / Outlet Invert= 120.20' / 119.00' S= 0.0136 '/' Cc= 0.900	
			n= 0.012, Flow Area= 1.23 sf	
#2	Secondary	126.90'	20.0' long x 12.0' breadth Broad-Crested Rectangular Weir	
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60	
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64	
#3	Device 1	124.55'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)	
			0.5' Crest Height	
#4	Device 1	120.20'	6.0" Vert. Orifice/Grate C= 0.600	

Primary OutFlow Max=0.77 cfs @ 13.57 hrs HW=121.11' (Free Discharge)

**-1=Culvert** (Passes 0.77 cfs of 3.08 cfs potential flow)

3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

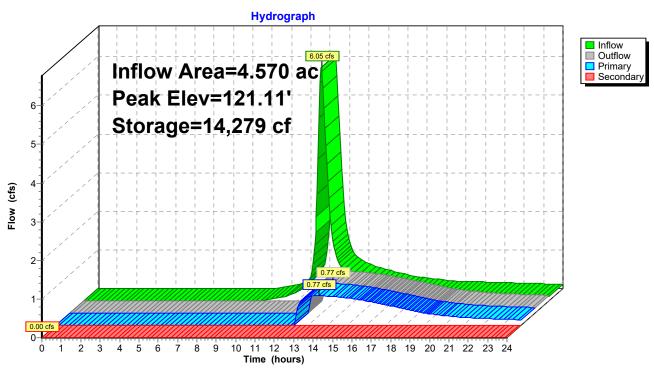
4=Orifice/Grate (Orifice Controls 0.77 cfs @ 3.90 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=119.00' (Free Discharge)

**2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

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Pond 1B - Pond: 1B - Pond



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## **Summary for Pond 1C-Pond: 1C - Pond**

Inflow Area = 11.850 ac, Inflow Depth > 1.78" for 2-YEAR STORM event

Inflow 16.97 cfs @ 12.27 hrs, Volume= 1.762 af

2.22 cfs @ 13.44 hrs, Volume= Outflow 1.141 af, Atten= 87%, Lag= 69.9 min

2.22 cfs @ 13.44 hrs, Volume= Primary = 1.141 af 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 116.83' @ 13.44 hrs Surf.Area= 18,815 sf Storage= 41,248 cf

Plug-Flow detention time= 248.7 min calculated for 1.138 af (65% of inflow)

Center-of-Mass det. time= 147.1 min ( 987.0 - 839.8 )

Volume	Invert	Avail.Storage	Storage Description
#1	114.00'	116,658 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
114.00	10,374	0	0
115.00	13,288	11,831	11,831
116.00	16,269	14,779	26,610
117.00	19,320	17,795	44,404
118.00	22,447	20,884	65,288
119.00	25,657	24,052	89,340
120.00	28,979	27,318	116,658

Jevice	Routing	invert	Outlet Devices
#1	Primary	115.70'	18.0" Round Culvert
			L= 91.6' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 115.70' / 115.00' S= 0.0076 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.77 sf
#2	Secondary	119.60'	30.0' long x 8.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.43 2.54 2.70 2.69 2.68 2.68 2.66 2.64 2.64
			2.64 2.65 2.65 2.66 2.66 2.68 2.70 2.74
#3	Device 1	116.90'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 1	115.70'	<b>10.0" Vert. Orifice/Grate</b> C= 0.600

**Primary OutFlow** Max=2.22 cfs @ 13.44 hrs HW=116.83' (Free Discharge)

**-1=Culvert** (Passes 2.22 cfs of 4.93 cfs potential flow)

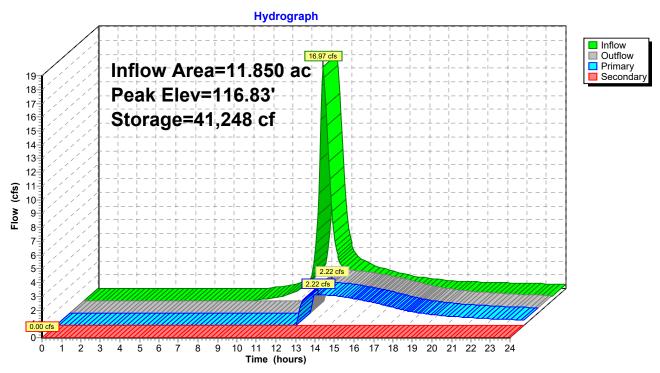
3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

4=Orifice/Grate (Orifice Controls 2.22 cfs @ 4.08 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=114.00' (Free Discharge)

**2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Pond 1C-Pond: 1C - Pond



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## Summary for Pond 2 - Pond: 2 - Pond

Inflow Area = 3.660 ac, Inflow Depth > 1.71" for 2-YEAR STORM event Inflow 5.35 cfs @ 12.23 hrs, Volume= 0.522 af 0.34 cfs @ 15.53 hrs, Volume= Outflow 0.300 af, Atten= 94%, Lag= 198.2 min Primary 0.34 cfs @ 15.53 hrs, Volume= 0.300 af 0.00 cfs @ 0.00 hrs, Volume= Secondary = 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 172.68' @ 15.53 hrs Surf.Area= 5,398 sf Storage= 14,084 cf

Plug-Flow detention time= 346.7 min calculated for 0.300 af (57% of inflow)

Center-of-Mass det. time= 236.6 min ( 1,077.1 - 840.6 )

Volume	Invert	Avail.Sto	rage Storage	e Description			
#1	169.00'	29,37	77 cf Custon	n Stage Data (P	rismatic)Listed below (Recalc)		
	•			0 01			
Elevation		ırf.Area	Inc.Store	Cum.Store			
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)			
169.0	00	2,429	0	0			
170.0	00	3,127	2,778	2,778			
171.0	00	3,912	3,520	6,298			
172.0	00	4,771	4,342	10,639			
173.0	00	5,697	5,234	15,873			
174.0	00	6,691	6,194	22,067			
175.0	00	7,929	7,310	29,377			
Device	Routing	Invert	Outlet Device	es			
#1 Device 2		172.70'	3.0' long Sh	arp-Crested Red	ctangular Weir 2 End Contraction(s)		
			0.5' Crest He	eight	. ,		
#2	Primary	170.50'	12.0" Round Culvert				
	•		L= 42.0' RC	P, square edge l	headwall, Ke= 0.500		
			Inlet / Outlet	Invert= 170.50' /	170.00' S= 0.0119 '/' Cc= 0.900		
				n= 0.012, Flow Area= 0.79 sf			
#3	Secondary	Secondary 174.60'		30.0' long x 12.0' breadth Broad-Crested Rectangular Weir			
	,			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60			
			` ,		70 2.67 2.66 2.67 2.66 2.64		
#4	Device 2	170.50'		rifice/Grate C=			

Primary OutFlow Max=0.34 cfs @ 15.53 hrs HW=172.68' (Free Discharge)

**-2=Culvert** (Passes 0.34 cfs of 4.90 cfs potential flow)

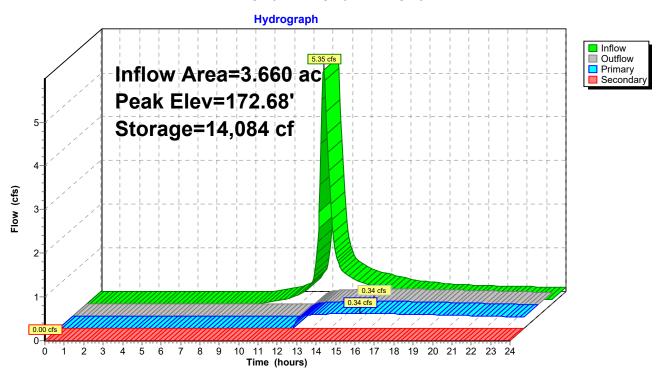
-1=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

**-4=Orifice/Grate** (Orifice Controls 0.34 cfs @ 6.90 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=169.00' (Free Discharge) 3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond 2 - Pond: 2 - Pond



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### **Summary for Pond 4 - Pond: 4 - Pond**

Inflow Area = 9.080 ac, Inflow Depth > 1.24" for 2-YEAR STORM event

Inflow 10.24 cfs @ 12.18 hrs, Volume= 0.940 af

0.34 cfs @ 18.17 hrs, Volume= Outflow 0.317 af, Atten= 97%, Lag= 358.9 min

Primary 0.34 cfs @ 18.17 hrs, Volume= 0.317 af 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 123.22' @ 18.17 hrs Surf.Area= 11,199 sf Storage= 28,735 cf

Plug-Flow detention time= 374.4 min calculated for 0.317 af (34% of inflow)

Center-of-Mass det. time= 239.3 min (1,098.5 - 859.2)

Volume	Inv	<u>ert Avai</u>	I.Storage	Storage	Description		
#1	120.	00'	79,242 cf	Custom	Stage Data (Prisn	natic)Listed below	(Recalc)
Elevatio	n	Surf.Area	Inc	:Store	Cum.Store		
(fee	t)	(sq-ft)	(cubi	c-feet)	(cubic-feet)		
120.0	00	6,749		0	0		
121.0	00	8,061		7,405	7,405		
122.0	00	9,434		8,748	16,153		
123.0	00	10,869	•	10,152	26,304		
124.0	00	12,365	•	11,617	37,921		
125.0	00	13,922	•	13,144	51,065		
126.0	00	15,541	•	14,732	65,796		
127.0	00	11,350	•	13,446	79,242		
Device	Routing	In	vert Outl	et Device	s		
#1	Drimary	120	40' 48 f	" Pound	Culvert		

			Guilot Bottoco
#1	Primary	120.40'	18.0" Round Culvert
	•		L= 53.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 120.40' / 120.00' S= 0.0075 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.77 sf
#2	Secondary	126.50'	20.0' long x 12.0' breadth Broad-Crested Rectangular Weir
	•		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#3	Device 1	125.00'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 1	121.00'	3.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=0.34 cfs @ 18.17 hrs HW=123.22' (Free Discharge)

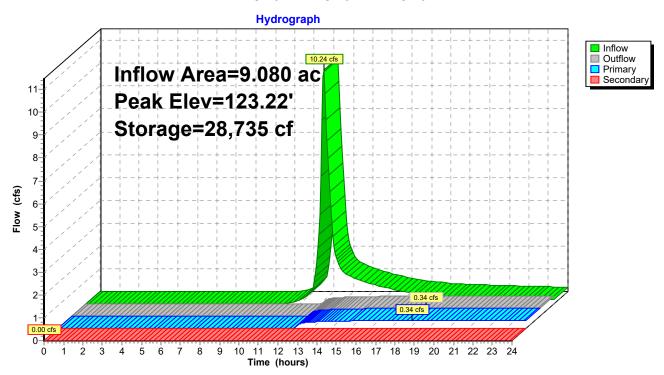
**-1=Culvert** (Passes 0.34 cfs of 12.20 cfs potential flow)

-3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs) 4=Orifice/Grate (Orifice Controls 0.34 cfs @ 6.97 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=120.00' (Free Discharge)

2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 4 - Pond: 4 - Pond



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# **Summary for Pond 5 - Pond: 5 - Pond**

Inflow Area = 15.220 ac, Inflow Depth > 1.94" for 2-YEAR STORM event

Inflow 26.00 cfs @ 12.21 hrs, Volume= 2.462 af

3.15 cfs @ 13.26 hrs, Volume= Outflow 1.811 af, Atten= 88%, Lag= 63.1 min

3.15 cfs @ 13.26 hrs, Volume= Primary 1.811 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 123.16' @ 13.26 hrs Surf.Area= 21,433 sf Storage= 57,476 cf

Plug-Flow detention time= 247.9 min calculated for 1.811 af (74% of inflow)

Center-of-Mass det. time= 159.1 min ( 989.1 - 830.1 )

Volume	Invert	Avail.Storage	Storage Description
#1	120.00'	187,159 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	15,063	0	0
121.00	17,014	16,039	16,039
122.00	19,025	18,020	34,058
123.00	21,096	20,061	54,119
124.00	23,228	22,162	76,281
125.00	25,421	24,325	100,605
126.00	27,674	26,548	127,153
127.00	29,988	28,831	155,984
128.00	32,362	31,175	187,159

Device	Routing	Invert	Outlet Devices
#1	Device 2	123.50'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#2	Primary	121.30'	24.0" Round Culvert
			L= 81.5' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 121.30' / 115.25' S= 0.0742 '/' Cc= 0.900
			n= 0.012, Flow Area= 3.14 sf
#3	Secondary	127.90'	30.0' long x 12.0' breadth Broad-Crested Rectangular Weir
	-		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#4	Device 2	121.30'	10.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=3.15 cfs @ 13.26 hrs HW=123.16' (Free Discharge)

**-2=Culvert** (Passes 3.15 cfs of 14.12 cfs potential flow)

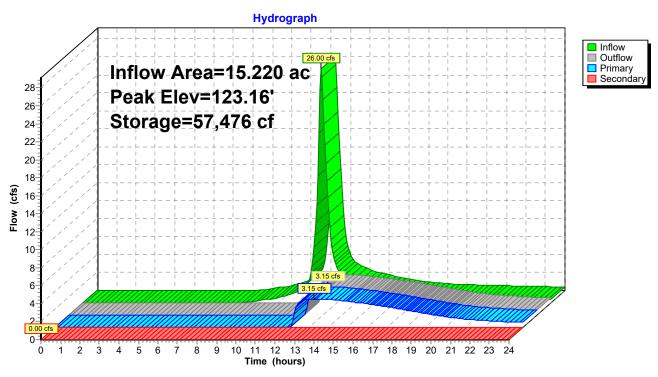
-1=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

4=Orifice/Grate (Orifice Controls 3.15 cfs @ 5.78 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=120.00' (Free Discharge)

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#### Pond 5 - Pond: 5 - Pond



# HydroCAD North Stonington Proposed\_Rev Type III 24-hr 10-YEAR STORM Rainfall=5.08"

Prepared by HDR, Inc

Printed 6/25/2021

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A: Runoff Area=4.190 ac Runoff Depth>2.68"

Tc=13.2 min CN=77 Runoff=10.38 cfs 0.937 af

Subcatchment1B: Runoff Area=4.570 ac Runoff Depth>3.05"

Tc=18.7 min CN=81 Runoff=11.32 cfs 1.160 af

Subcatchment1C: Runoff Area=11.850 ac Runoff Depth>3.24"

Tc=19.3 min CN=83 Runoff=30.71 cfs 3.195 af

Subcatchment2: Runoff Area=3.660 ac Runoff Depth>3.14"

Tc=16.2 min CN=82 Runoff=9.89 cfs 0.958 af

Subcatchment4: Runoff Area=9.080 ac Runoff Depth>2.51"

Tc=12.4 min CN=75 Runoff=21.38 cfs 1.898 af

Subcatchment5: Runoff Area=15.220 ac Runoff Depth>3.43"

Tc=15.3 min CN=85 Runoff=45.58 cfs 4.355 af

**Pond 1A - Pond: 1A - Pond**Peak Elev=128.80' Storage=19,701 cf Inflow=10.38 cfs 0.937 af

Primary=1.54 cfs 0.790 af Secondary=0.00 cfs 0.000 af Outflow=1.54 cfs 0.790 af

**Pond 1B - Pond: 1B - Pond**Peak Elev=122.58' Storage=27,461 cf Inflow=11.32 cfs 1.160 af

Primary=1.38 cfs 0.929 af Secondary=0.00 cfs 0.000 af Outflow=1.38 cfs 0.929 af

Pond 1C-Pond: 1C - Pond Peak Elev=117.94' Storage=63,859 cf Inflow=30.71 cfs 3.195 af

Primary=9.93 cfs 2.537 af Secondary=0.00 cfs 0.000 af Outflow=9.93 cfs 2.537 af

**Pond 2 - Pond: 2 - Pond**Peak Elev=173.29' Storage=17,550 cf Inflow=9.89 cfs 0.958 af

Primary=5.24 cfs 0.690 af Secondary=0.00 cfs 0.000 af Outflow=5.24 cfs 0.690 af

Pond 4 - Pond: 4 - Pond Peak Elev=125.21' Storage=54,059 cf Inflow=21.38 cfs 1.898 af

Primary=1.49 cfs 0.739 af Secondary=0.00 cfs 0.000 af Outflow=1.49 cfs 0.739 af

**Pond 5 - Pond: 5 - Pond**Peak Elev=124.71' Storage=93,318 cf Inflow=45.58 cfs 4.355 af

Primary=12.19 cfs 3.635 af Secondary=0.00 cfs 0.000 af Outflow=12.19 cfs 3.635 af

Total Runoff Area = 48.570 ac Runoff Volume = 12.503 af Average Runoff Depth = 3.09"

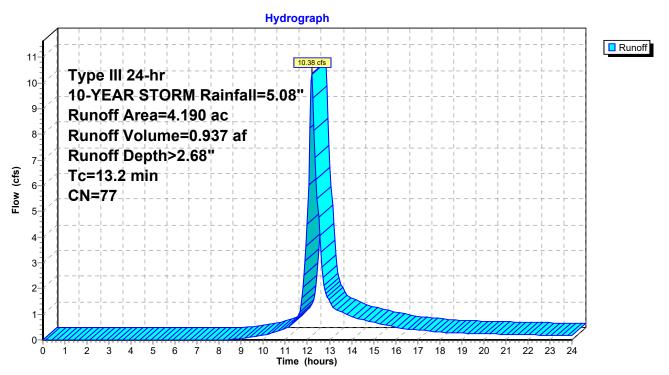
# **Summary for Subcatchment 1A:**

Runoff 10.38 cfs @ 12.19 hrs, Volume= 0.937 af, Depth> 2.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YEAR STORM Rainfall=5.08"

_	Area	(ac)	CN	Desc	cription		
•	4.	.190	77				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	13.2						Direct Entry, NRCS Part 630

#### **Subcatchment 1A:**



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# **Summary for Subcatchment 1B:**

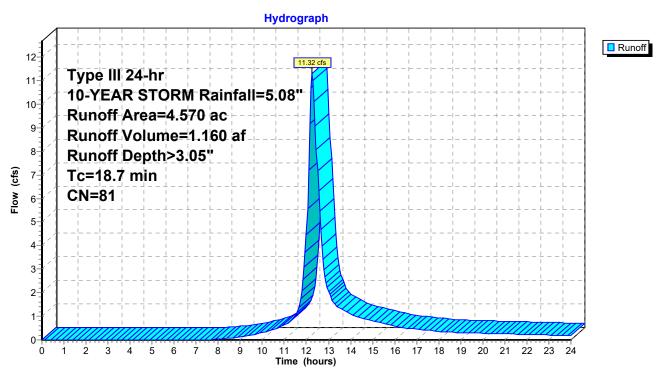
Runoff 11.32 cfs @ 12.26 hrs, Volume=

1.160 af, Depth> 3.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YEAR STORM Rainfall=5.08"

_	Area	(ac)	CN	Desc	cription		
,	4.	.570	81				
_							
	Tc	Leng	jth	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	18 7						Direct Entry NRCS Part 630

#### **Subcatchment 1B:**



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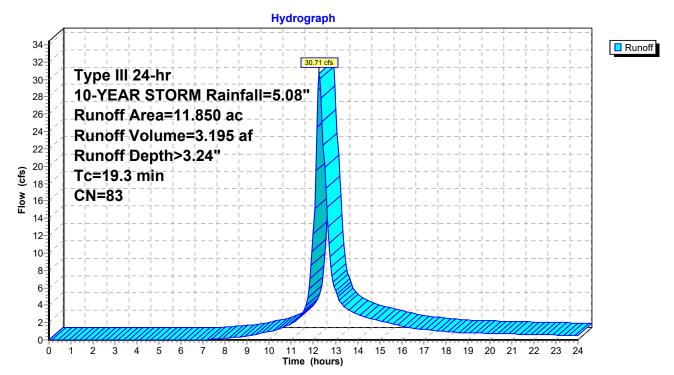
### **Summary for Subcatchment 1C:**

Runoff 30.71 cfs @ 12.26 hrs, Volume= 3.195 af, Depth> 3.24"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YEAR STORM Rainfall=5.08"

_	Area	(ac)	CN	Desc	cription		
•	<b>'</b> 11.	.850	83				
-	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	19.3						Direct Entry, NRCS Part 630

#### **Subcatchment 1C:**



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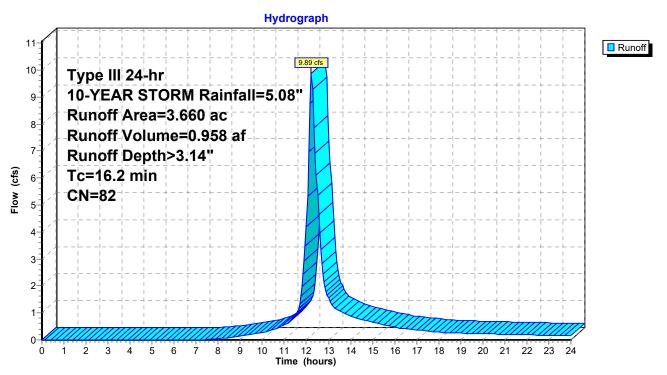
### **Summary for Subcatchment 2:**

Runoff 9.89 cfs @ 12.22 hrs, Volume= 0.958 af, Depth> 3.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YEAR STORM Rainfall=5.08"

	Area	(ac)	CN	Desc	cription		
*	3.	660	82				
	т.		41-	01	\/-li+.	0	Decembrish
	Tc	J			,	. ,	Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	16.2						Direct Entry, NRCS Part 630

#### **Subcatchment 2:**



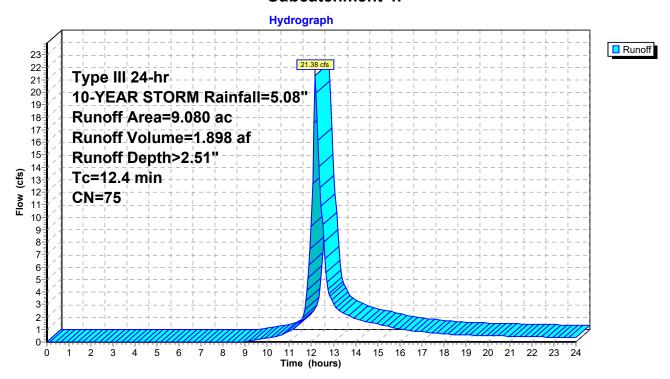
### **Summary for Subcatchment 4:**

Runoff 21.38 cfs @ 12.18 hrs, Volume= 1.898 af, Depth> 2.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YEAR STORM Rainfall=5.08"

_	Area	(ac)	CN	Desc	cription		
•	9.	.080	75				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	12.4						Direct Entry NDCS Part 630

#### Subcatchment 4:



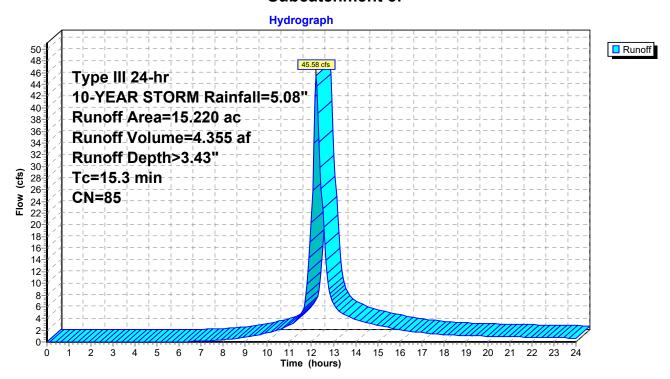
### **Summary for Subcatchment 5:**

Runoff 45.58 cfs @ 12.21 hrs, Volume= 4.355 af, Depth> 3.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YEAR STORM Rainfall=5.08"

_	Area	(ac)	CN	Desc	cription		
*	15.	220	85				
	Tc	J			,		Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	15.3						Direct Entry, NRCS Part 630

#### Subcatchment 5:



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### Summary for Pond 1A - Pond: 1A - Pond

Inflow Area = 4.190 ac, Inflow Depth > 2.68" for 10-YEAR STORM event

Inflow = 10.38 cfs @ 12.19 hrs, Volume= 0.937 af

Outflow = 1.54 cfs @ 12.98 hrs, Volume= 0.790 af, Atten= 85%, Lag= 47.8 min

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 128.80' @ 12.98 hrs Surf.Area= 6,582 sf Storage= 19,701 cf

Plug-Flow detention time= 188.7 min calculated for 0.788 af (84% of inflow)

Center-of-Mass det. time= 123.1 min ( 957.3 - 834.2 )

Volume	Invert	Avail.Storage	Storage Description
#1	123.00'	37,272 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
123.00	692	0	0
124.00	1,464	1,078	1,078
125.00	2,382	1,923	3,001
126.00	3,381	2,882	5,883
127.00	4,452	3,917	9,799
128.00	5,614	5,033	14,832
129.00	6,826	6,220	21,052
130.00	8,095	7,461	28,513
131.00	9,424	8,760	37,272

Device	Routing	Invert	Outlet Devices
#1	Secondary	130.90'	<b>20.0' long x 12.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#2	Primary	125.80'	24.0" Round Culvert
			L= 401.4' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 125.80' / 123.80' S= 0.0050 '/' Cc= 0.900
			n= 0.012, Flow Area= 3.14 sf
#3	Device 2	130.50'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 2	125.90'	6.0" Vert. Orifice/Grate C= 0.600

**Primary OutFlow** Max=1.54 cfs @ 12.98 hrs HW=128.80' (Free Discharge)

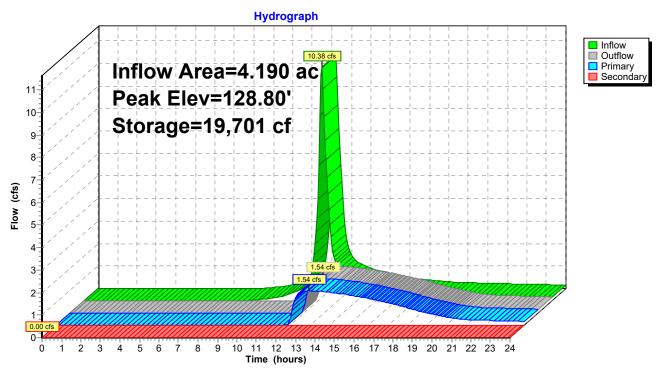
**2=Culvert** (Passes 1.54 cfs of 18.19 cfs potential flow)

3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

4=Orifice/Grate (Orifice Controls 1.54 cfs @ 7.84 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=123.00' (Free Discharge)

Pond 1A - Pond: 1A - Pond



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### Summary for Pond 1B - Pond: 1B - Pond

Inflow Area = 4.570 ac, Inflow Depth > 3.05" for 10-YEAR STORM event

Inflow 11.32 cfs @ 12.26 hrs, Volume= 1.160 af

1.38 cfs @ 13.43 hrs, Volume= Outflow 0.929 af, Atten= 88%, Lag= 70.2 min

1.38 cfs @ 13.43 hrs, Volume= Primary = 0.929 af 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 122.58' @ 13.43 hrs Surf.Area= 9,839 sf Storage= 27,461 cf

Plug-Flow detention time= 261.1 min calculated for 0.929 af (80% of inflow)

Center-of-Mass det. time= 185.9 min (1,014.0 - 828.1)

Volume	Invert	Avail.Storage	Storage Description
#1	119.00'	83,261 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
119.00	5,600	0	0
120.00	6,708	6,154	6,154
121.00	7,871	7,290	13,444
122.00	9,092	8,482	21,925
123.00	10,369	9,731	31,656
124.00	11,703	11,036	42,692
125.00	12,160	11,932	54,623
126.00	14,538	13,349	67,972
127.00	16,040	15,289	83,261

Device	Routing	Invert	Outlet Devices
#1	Primary	120.20'	15.0" Round Culvert
			L= 88.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 120.20' / 119.00' S= 0.0136 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.23 sf
#2	Secondary	126.90'	20.0' long x 12.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#3	Device 1	124.55'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 1	120.20'	6.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=1.38 cfs @ 13.43 hrs HW=122.58' (Free Discharge)

**-1=Culvert** (Passes 1.38 cfs of 7.84 cfs potential flow)

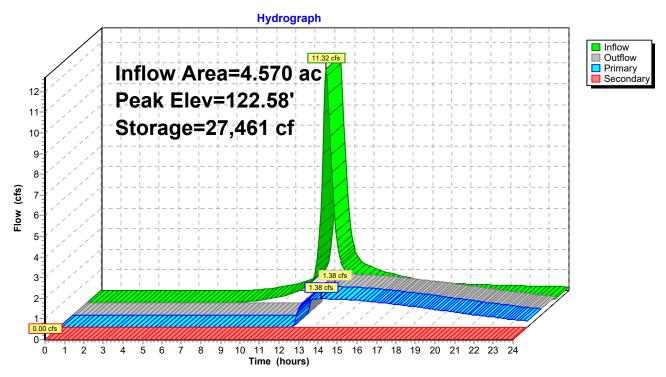
3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

**4=Orifice/Grate** (Orifice Controls 1.38 cfs @ 7.04 fps)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=119.00' (Free Discharge)

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#### Pond 1B - Pond: 1B - Pond



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### **Summary for Pond 1C-Pond: 1C - Pond**

Inflow Area = 11.850 ac, Inflow Depth > 3.24" for 10-YEAR STORM event

Inflow = 30.71 cfs @ 12.26 hrs, Volume= 3.195 af

Outflow = 9.93 cfs @ 12.74 hrs, Volume= 2.537 af, Atten= 68%, Lag= 28.6 min

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 117.94' @ 12.74 hrs Surf.Area= 22,247 sf Storage= 63,859 cf

Plug-Flow detention time= 180.1 min calculated for 2.537 af (79% of inflow)

Center-of-Mass det. time= 104.0 min ( 927.0 - 823.0 )

Volume	Invert	Avail.Storage	Storage Description
#1	114.00'	116.658 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
114.00	10,374	0	0
115.00	13,288	11,831	11,831
116.00	16,269	14,779	26,610
117.00	19,320	17,795	44,404
118.00	22,447	20,884	65,288
119.00	25,657	24,052	89,340
120.00	28,979	27,318	116,658

Jevice	Routing	invert	Outlet Devices
#1	Primary	115.70'	18.0" Round Culvert
			L= 91.6' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 115.70' / 115.00' S= 0.0076 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.77 sf
#2	Secondary	119.60'	30.0' long x 8.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.43 2.54 2.70 2.69 2.68 2.68 2.66 2.64 2.64
			2.64 2.65 2.65 2.66 2.66 2.68 2.70 2.74
#3	Device 1	116.90'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 1	115.70'	<b>10.0" Vert. Orifice/Grate</b> C= 0.600

Primary OutFlow Max=9.93 cfs @ 12.74 hrs HW=117.94' (Free Discharge)

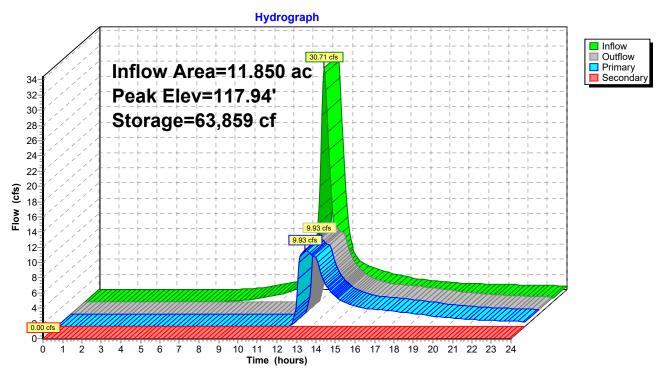
-1=Culvert (Barrel Controls 9.93 cfs @ 5.62 fps)

3=Sharp-Crested Rectangular Weir(Passes < 12.06 cfs potential flow)

**4=Orifice/Grate** (Passes < 3.54 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=114.00' (Free Discharge)

Pond 1C-Pond: 1C - Pond



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# **Summary for Pond 2 - Pond: 2 - Pond**

Inflow Area = 3.660 ac, Inflow Depth > 3.14" for 10-YEAR STORM event Inflow 9.89 cfs @ 12.22 hrs, Volume= 0.958 af

5.24 cfs @ 12.51 hrs, Volume= Outflow 0.690 af, Atten= 47%, Lag= 17.5 min

Primary 5.24 cfs @ 12.51 hrs, Volume= 0.690 af 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 173.29' @ 12.51 hrs Surf.Area= 5,982 sf Storage= 17,550 cf

Plug-Flow detention time= 197.6 min calculated for 0.690 af (72% of inflow)

Center-of-Mass det. time= 107.6 min ( 930.9 - 823.3 )

Volume	ln۱	∕ert Avail.S	Storage	Storage	Description	
#1	169.	.00' 29	,377 cf	Custon	n Stage Data (Pi	rismatic)Listed below (Recalc)
Elevation	on	Surf.Area	Inc	.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic	c-feet)	(cubic-feet)	
169.0	00	2,429		0	0	
170.0	00	3,127		2,778	2,778	
171.0	00	3,912		3,520	6,298	
172.0		4,771		4,342	10,639	
173.0		5,697		5,234	15,873	
174.0		6,691		6,194	22,067	
175.0	00	7,929		7,310	29,377	
Device	Routing	ı Inve	ert Outle	et Device	es	
#1	Device	2 172.7		_	<u>-</u>	ctangular Weir 2 End Contraction(s)
#2	Primary	170.5	0' <b>12.0</b> '		d Culvert	
					, ,	headwall, Ke= 0.500

			0.5 Crest reight
#2	Primary	170.50'	12.0" Round Culvert
			L= 42.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 170.50' / 170.00' S= 0.0119 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf
#3	Secondary	174.60'	30.0' long x 12.0' breadth Broad-Crested Rectangular Weir
	•		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#4	Device 2	170.50'	3.0" Vert. Orifice/Grate C= 0.600

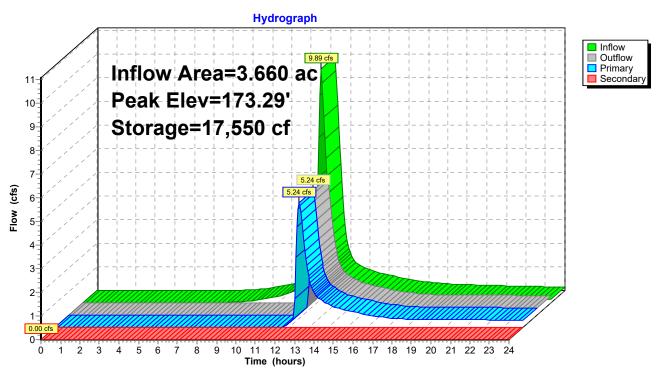
Primary OutFlow Max=5.20 cfs @ 12.51 hrs HW=173.28' (Free Discharge) **-2=Culvert** (Passes 5.20 cfs of 5.72 cfs potential flow)

-1=Sharp-Crested Rectangular Weir (Weir Controls 4.82 cfs @ 2.86 fps)

**-4=Orifice/Grate** (Orifice Controls 0.39 cfs @ 7.85 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=169.00' (Free Discharge) 3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 2 - Pond: 2 - Pond



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# **Summary for Pond 4 - Pond: 4 - Pond**

Inflow Area = 9.080 ac, Inflow Depth > 2.51" for 10-YEAR STORM event

Inflow 21.38 cfs @ 12.18 hrs, Volume= 1.898 af

1.49 cfs @ 14.84 hrs, Volume= Outflow 0.739 af, Atten= 93%, Lag= 160.0 min

1.49 cfs @ 14.84 hrs, Volume= Primary 0.739 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 125.21' @ 14.84 hrs Surf.Area= 14,266 sf Storage= 54,059 cf

Plug-Flow detention time= 324.9 min calculated for 0.737 af (39% of inflow)

Center-of-Mass det. time= 201.5 min ( 1,040.1 - 838.6 )

Volume	Invert A	Avail.Storage	Storage	e Description	
#1	120.00'	79,242 cf	Custom	m Stage Data (Prismatic)Listed below (Recalc)	
Elevation (feet)	Surf.Ar (sq		:.Store c-feet)	Cum.Store (cubic-feet)	
120.00	6.7	'//Q	Λ	0	

(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	6,749	0	0
121.00	8,061	7,405	7,405
122.00	9,434	8,748	16,153
123.00	10,869	10,152	26,304
124.00	12,365	11,617	37,921
125.00	13,922	13,144	51,065
126.00	15,541	14,732	65,796
127.00	11,350	13,446	79,242

Device	Routing	Invert	Outlet Devices
#1	Primary	120.40'	18.0" Round Culvert
			L= 53.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 120.40' / 120.00' S= 0.0075 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.77 sf
#2	Secondary	126.50'	20.0' long x 12.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#3	Device 1	125.00'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 1	121.00'	3.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=1.47 cfs @ 14.84 hrs HW=125.21' (Free Discharge)

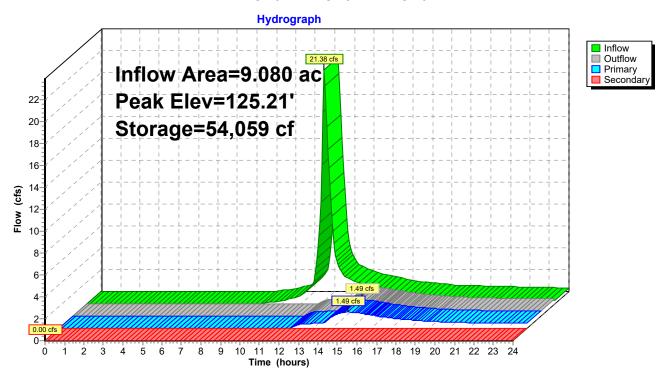
**-1=Culvert** (Passes 1.47 cfs of 17.15 cfs potential flow)

-3=Sharp-Crested Rectangular Weir (Weir Controls 1.00 cfs @ 1.59 fps) 

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=120.00' (Free Discharge)

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Pond 4 - Pond: 4 - Pond



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### **Summary for Pond 5 - Pond: 5 - Pond**

Inflow Area = 15.220 ac, Inflow Depth > 3.43" for 10-YEAR STORM event

Inflow 45.58 cfs @ 12.21 hrs, Volume= 4.355 af

12.19 cfs @ 12.69 hrs, Volume= Outflow 3.635 af, Atten= 73%, Lag= 29.0 min

12.19 cfs @ 12.69 hrs, Volume= Primary 3.635 af 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 124.71' @ 12.69 hrs Surf.Area= 24,784 sf Storage= 93,318 cf

Plug-Flow detention time= 206.7 min calculated for 3.628 af (83% of inflow)

Center-of-Mass det. time= 140.6 min ( 954.5 - 814.0 )

Volume	Invert	Avail.Storage	Storage Description
#1	120.00'	187,159 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	15,063	0	0
121.00	17,014	16,039	16,039
122.00	19,025	18,020	34,058
123.00	21,096	20,061	54,119
124.00	23,228	22,162	76,281
125.00	25,421	24,325	100,605
126.00	27,674	26,548	127,153
127.00	29,988	28,831	155,984
128.00	32,362	31,175	187,159

Device	Routing	Invert	Outlet Devices
#1	Device 2	123.50'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#2	Primary	121.30'	24.0" Round Culvert
			L= 81.5' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 121.30' / 115.25' S= 0.0742 '/' Cc= 0.900
			n= 0.012, Flow Area= 3.14 sf
#3	Secondary	127.90'	30.0' long x 12.0' breadth Broad-Crested Rectangular Weir
	-		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#4	Device 2	121.30'	10.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=12.18 cfs @ 12.69 hrs HW=124.71' (Free Discharge)

**-2=Culvert** (Passes 12.18 cfs of 23.48 cfs potential flow)

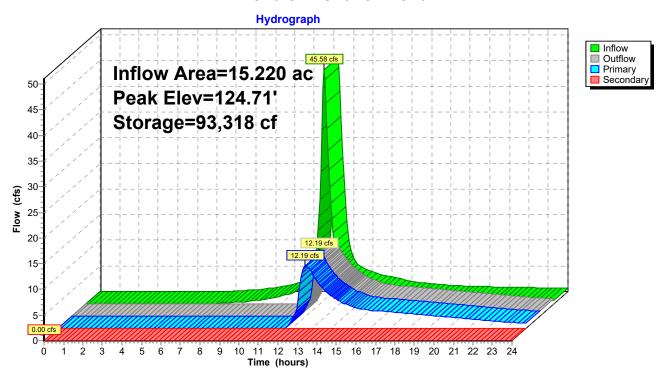
-1=Sharp-Crested Rectangular Weir (Weir Controls 7.64 cfs @ 3.60 fps)

4=Orifice/Grate (Orifice Controls 4.54 cfs @ 8.33 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=120.00' (Free Discharge) 3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond 5 - Pond: 5 - Pond



# HydroCAD North Stonington Proposed\_Rev Type III 24-hr 25-YEAR STORM Rainfall=6.11"

Prepared by HDR, Inc

Printed 6/25/2021

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A: Runoff Area=4.190 ac Runoff Depth>3.57"

Tc=13.2 min CN=77 Runoff=13.81 cfs 1.245 af

Subcatchment1B: Runoff Area=4.570 ac Runoff Depth>3.97"

Tc=18.7 min CN=81 Runoff=14.69 cfs 1.512 af

**Subcatchment1C:** Runoff Area=11.850 ac Runoff Depth>4.18"

Tc=19.3 min CN=83 Runoff=39.43 cfs 4.128 af

Subcatchment2: Runoff Area=3.660 ac Runoff Depth>4.08"

Tc=16.2 min CN=82 Runoff=12.76 cfs 1.244 af

Subcatchment4: Runoff Area=9.080 ac Runoff Depth>3.37"

Tc=12.4 min CN=75 Runoff=29.01 cfs 2.549 af

Subcatchment5: Runoff Area=15.220 ac Runoff Depth>4.40"

Tc=15.3 min CN=85 Runoff=57.87 cfs 5.575 af

**Pond 1A - Pond: 1A - Pond**Peak Elev=129.84' Storage=27,261 cf Inflow=13.81 cfs 1.245 af

Primary=1.82 cfs 1.095 af Secondary=0.00 cfs 0.000 af Outflow=1.82 cfs 1.095 af

**Pond 1B - Pond: 1B - Pond**Peak Elev=123.49' Storage=36,842 cf Inflow=14.69 cfs 1.512 af

Primary=1.65 cfs 1.234 af Secondary=0.00 cfs 0.000 af Outflow=1.65 cfs 1.234 af

Pond 1C-Pond: 1C - Pond Peak Elev=118.70' Storage=81,787 cf Inflow=39.43 cfs 4.128 af

Primary=12.29 cfs 3.449 af Secondary=0.00 cfs 0.000 af Outflow=12.29 cfs 3.449 af

**Pond 2 - Pond: 2 - Pond**Peak Elev=173.82' Storage=20,879 cf Inflow=12.76 cfs 1.244 af

Primary=6.35 cfs 0.954 af Secondary=0.00 cfs 0.000 af Outflow=6.35 cfs 0.954 af

Pond 4 - Pond: 4 - Pond Peak Elev=125.54' Storage=58,819 cf Inflow=29.01 cfs 2.549 af

Primary=4.75 cfs 1.372 af Secondary=0.00 cfs 0.000 af Outflow=4.75 cfs 1.372 af

**Pond 5 - Pond: 5 - Pond**Peak Elev=125.45' Storage=112,279 cf Inflow=57.87 cfs 5.575 af

Primary=19.41 cfs 4.812 af Secondary=0.00 cfs 0.000 af Outflow=19.41 cfs 4.812 af

Total Runoff Area = 48.570 ac Runoff Volume = 16.253 af Average Runoff Depth = 4.02"

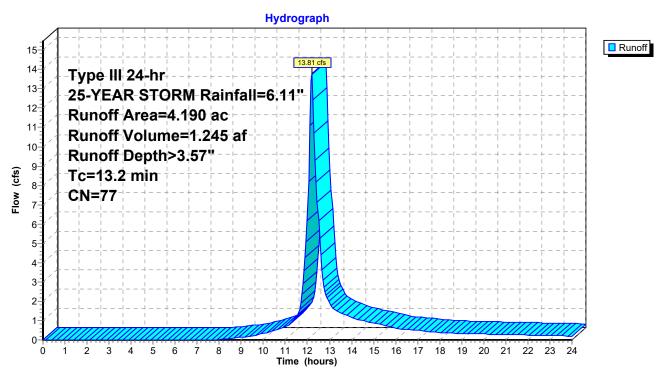
### **Summary for Subcatchment 1A:**

Runoff 13.81 cfs @ 12.18 hrs, Volume= 1.245 af, Depth> 3.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR STORM Rainfall=6.11"

_	Area	(ac)	CN	Desc	cription		
*	4.	190	77				
	Тс	J		•	•		Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
_	13.2						Direct Entry, NRCS Part 630

# **Subcatchment 1A:**



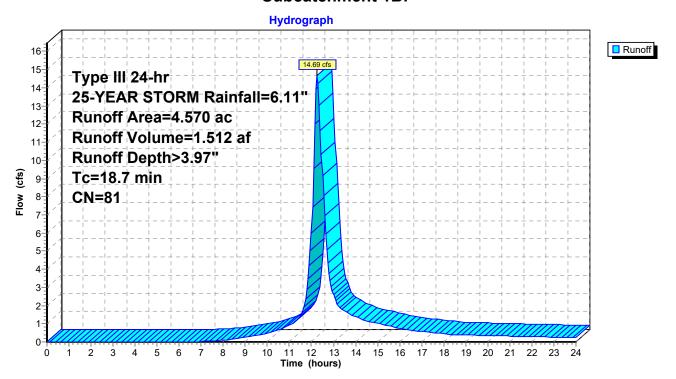
# **Summary for Subcatchment 1B:**

Runoff 14.69 cfs @ 12.26 hrs, Volume= 1.512 af, Depth> 3.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR STORM Rainfall=6.11"

_	Area	(ac)	CN	Desc	cription		
*	4.	570	81				
_	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	18.7	(100	<u>, , , , , , , , , , , , , , , , , , , </u>	(1411)	(1000)	(010)	Direct Entry, NRCS Part 630

# **Subcatchment 1B:**



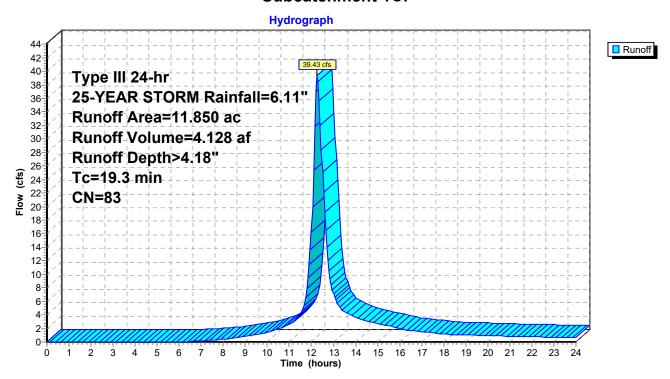
### **Summary for Subcatchment 1C:**

Runoff 39.43 cfs @ 12.26 hrs, Volume= 4.128 af, Depth> 4.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR STORM Rainfall=6.11"

	Area	(ac)	CN	Desc	cription		
•	<b>'</b> 11.	.850	83				
-	Tc			•	•		Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	19.3						Direct Entry, NRCS Part 630

#### **Subcatchment 1C:**



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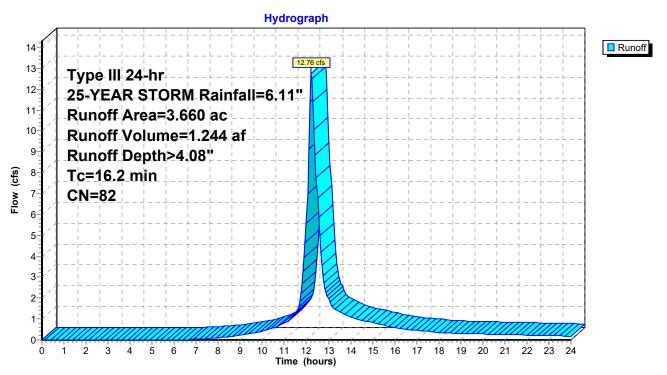
### **Summary for Subcatchment 2:**

Runoff = 12.76 cfs @ 12.22 hrs, Volume= 1.244 af, Depth> 4.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR STORM Rainfall=6.11"

Area	(ac)	CN	Desc	cription		
* 3.	.660	82				
Tc	Leng	th S	Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
16.2						Direct Entry NRCS Part 630

#### **Subcatchment 2:**



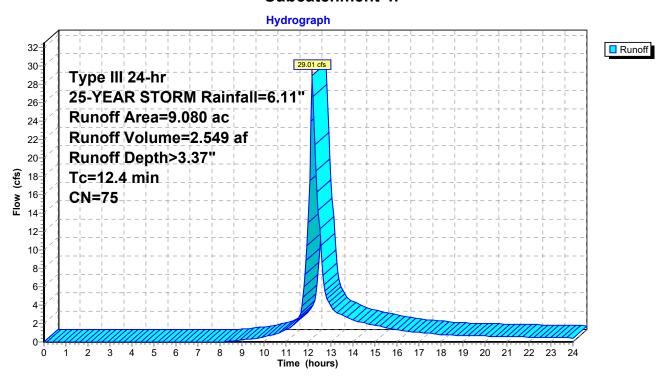
### **Summary for Subcatchment 4:**

Runoff 29.01 cfs @ 12.17 hrs, Volume= 2.549 af, Depth> 3.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR STORM Rainfall=6.11"

_	Area	(ac)	CN	Desc	cription		
•	9.	080	75				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	12.4						Direct Entry, NRCS Part 630

#### Subcatchment 4:



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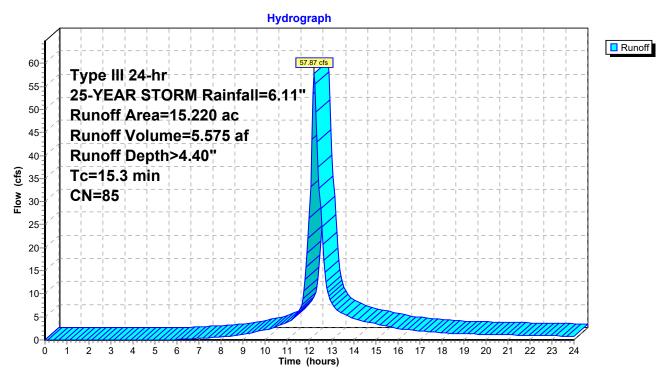
### **Summary for Subcatchment 5:**

Runoff 57.87 cfs @ 12.21 hrs, Volume= 5.575 af, Depth> 4.40"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YEAR STORM Rainfall=6.11"

_	Area	(ac)	CN	Desc	cription		
*	15.	220	85				
	Tc	J			,		Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	15.3						Direct Entry, NRCS Part 630

#### Subcatchment 5:



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# Summary for Pond 1A - Pond: 1A - Pond

Inflow Area = 4.190 ac, Inflow Depth > 3.57" for 25-YEAR STORM event

Inflow 13.81 cfs @ 12.18 hrs, Volume= 1.245 af

1.82 cfs @ 13.06 hrs, Volume= Outflow 1.095 af, Atten= 87%, Lag= 52.5 min

Primary 1.82 cfs @ 13.06 hrs, Volume= 1.095 af 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 129.84' @ 13.06 hrs Surf.Area= 7,896 sf Storage= 27,261 cf

Plug-Flow detention time= 205.5 min calculated for 1.093 af (88% of inflow)

Center-of-Mass det. time= 151.0 min ( 977.1 - 826.1 )

Volume	Invert	Avail.Storage	Storage Description
#1	123.00'	37,272 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
123.00	692	0	0
124.00	1,464	1,078	1,078
125.00	2,382	1,923	3,001
126.00	3,381	2,882	5,883
127.00	4,452	3,917	9,799
128.00	5,614	5,033	14,832
129.00	6,826	6,220	21,052
130.00	8,095	7,461	28,513
131.00	9,424	8,760	37,272

Device	Routing	Invert	Outlet Devices
#1	Secondary	130.90'	20.0' long x 12.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#2	Primary	125.80'	· • /
	,		L= 401.4' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 125.80' / 123.80' S= 0.0050 '/' Cc= 0.900
			n= 0.012, Flow Area= 3.14 sf
#3	Device 2	130.50'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 2	125.90'	6.0" Vert. Orifice/Grate C= 0.600
" '	DOVIGO E	120.00	old fold difficult of older

Primary OutFlow Max=1.82 cfs @ 13.06 hrs HW=129.84' (Free Discharge)

**-2=Culvert** (Passes 1.82 cfs of 21.12 cfs potential flow)

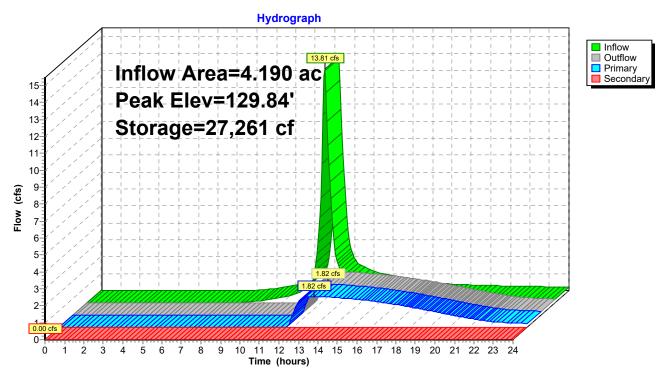
-3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

4=Orifice/Grate (Orifice Controls 1.82 cfs @ 9.25 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=123.00' (Free Discharge)

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Pond 1A - Pond: 1A - Pond



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### Summary for Pond 1B - Pond: 1B - Pond

Inflow Area = 4.570 ac, Inflow Depth > 3.97" for 25-YEAR STORM event

Inflow 14.69 cfs @ 12.26 hrs, Volume= 1.512 af

1.65 cfs @ 13.55 hrs, Volume= Outflow 1.234 af, Atten= 89%, Lag= 77.9 min

Primary = 1.65 cfs @ 13.55 hrs, Volume= 1.234 af 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 123.49' @ 13.55 hrs Surf.Area= 11,016 sf Storage= 36,842 cf

Plug-Flow detention time= 281.6 min calculated for 1.234 af (82% of inflow)

Center-of-Mass det. time= 210.4 min ( 1,031.0 - 820.6 )

Volume	Invert	Avail.Storage	Storage Description
#1	119.00'	83,261 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
119.00	5,600	0	0
120.00	6,708	6,154	6,154
121.00	7,871	7,290	13,444
122.00	9,092	8,482	21,925
123.00	10,369	9,731	31,656
124.00	11,703	11,036	42,692
125.00	12,160	11,932	54,623
126.00	14,538	13,349	67,972
127.00	16,040	15,289	83,261

Device	Routing	Invert	Outlet Devices
#1	Primary	120.20'	15.0" Round Culvert
	-		L= 88.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 120.20' / 119.00' S= 0.0136 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.23 sf
#2	Secondary	126.90'	20.0' long x 12.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#3	Device 1	124.55'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 1	120.20'	6.0" Vert. Orifice/Grate C= 0.600

**Primary OutFlow** Max=1.65 cfs @ 13.55 hrs HW=123.48' (Free Discharge)

**-1=Culvert** (Passes 1.65 cfs of 9.64 cfs potential flow)

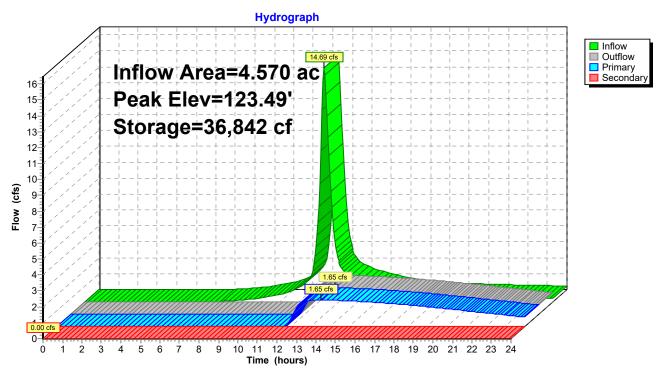
3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

4=Orifice/Grate (Orifice Controls 1.65 cfs @ 8.39 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=119.00' (Free Discharge)

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### Pond 1B - Pond: 1B - Pond



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# **Summary for Pond 1C-Pond: 1C - Pond**

Inflow Area = 11.850 ac, Inflow Depth > 4.18" for 25-YEAR STORM event

Inflow 39.43 cfs @ 12.26 hrs, Volume= 4.128 af

12.29 cfs @ 12.75 hrs, Volume= Outflow 3.449 af, Atten= 69%, Lag= 29.1 min

12.29 cfs @ 12.75 hrs, Volume= Primary 3.449 af 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 118.70' @ 12.75 hrs Surf.Area= 24,694 sf Storage= 81,787 cf

Plug-Flow detention time= 162.8 min calculated for 3.442 af (83% of inflow)

Center-of-Mass det. time= 97.3 min ( 913.2 - 815.8 )

Volume	Invert	Avail.Storage	Storage Description
#1	114.00'	116,658 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
114.00	10,374	0	0
115.00	13,288	11,831	11,831
116.00	16,269	14,779	26,610
117.00	19,320	17,795	44,404
118.00	22,447	20,884	65,288
119.00	25,657	24,052	89,340
120.00	28,979	27,318	116,658

Device	Routing	Invert	Outlet Devices
#1	Primary	115.70'	18.0" Round Culvert
			L= 91.6' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 115.70' / 115.00' S= 0.0076 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.77 sf
#2	Secondary	119.60'	30.0' long x 8.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.43 2.54 2.70 2.69 2.68 2.68 2.66 2.64 2.64
			2.64 2.65 2.65 2.66 2.66 2.68 2.70 2.74
#3	Device 1	116.90'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 1	115.70'	<b>10.0" Vert. Orifice/Grate</b> C= 0.600

Primary OutFlow Max=12.29 cfs @ 12.75 hrs HW=118.70' (Free Discharge)

-1=Culvert (Barrel Controls 12.29 cfs @ 6.96 fps)

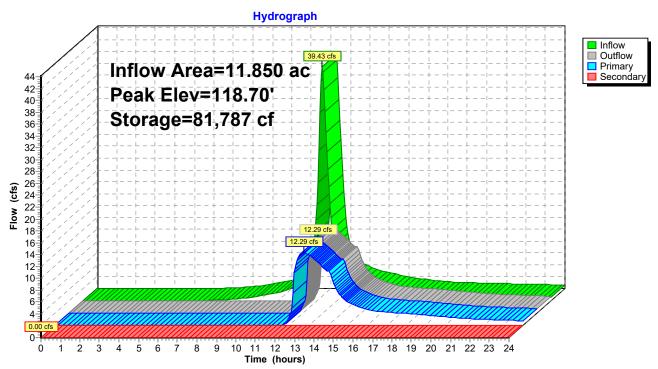
**3=Sharp-Crested Rectangular Weir**(Passes < 30.01 cfs potential flow)

**4=Orifice/Grate** (Passes < 4.22 cfs potential flow)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=114.00' (Free Discharge)

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## Pond 1C-Pond: 1C - Pond



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#### Summary for Pond 2 - Pond: 2 - Pond

Inflow Area = 3.660 ac, Inflow Depth > 4.08" for 25-YEAR STORM event

Inflow 12.76 cfs @ 12.22 hrs, Volume= 1.244 af

6.35 cfs @ 12.52 hrs, Volume= Outflow 0.954 af, Atten= 50%, Lag= 18.3 min

Primary 6.35 cfs @ 12.52 hrs, Volume= 0.954 af 0.00 cfs @ 0.00 hrs, Volume= Secondary = 0.000 af

Routing by Stor-Ind method. Time Span= 0.00-24.00 hrs. dt= 0.05 hrs. Peak Elev= 173.82' @ 12.52 hrs Surf.Area= 6,512 sf Storage= 20,879 cf

Plug-Flow detention time= 160.1 min calculated for 0.954 af (77% of inflow)

Center-of-Mass det. time= 78.9 min (894.8 - 816.0)

Volume	Inve	ert Avail.	Storage	Storage	Description	
#1	169.0	0' 2	9,377 cf	Custon	n Stage Data (Pi	rismatic)Listed below (Recalc)
Elevatio	on	Surf.Area	Inc	.Store	Cum.Store	
(fee		(sq-ft)		c-feet)	(cubic-feet)	
169.0	00	2,429		0	0	
170.0	00	3,127		2,778	2,778	
171.0	00	3,912		3,520	6,298	
172.0	00	4,771		4,342	10,639	
173.0	00	5,697		5,234	15,873	
174.0	00	6,691		6,194	22,067	
175.0	00	7,929		7,310	29,377	
Device	Routing	Inv	ert Outle	et Device	es	
#1	Device 2	172.7	70' <b>3.0'</b>	long Sha	arp-Crested Red	ctangular Weir 2 End Contraction(s)

D01100	rtouting	1111011	Guillet Beviece
#1	Device 2	172.70'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#2	Primary	170.50'	12.0" Round Culvert
	-		L= 42.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 170.50' / 170.00' S= 0.0119 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf
#3	Secondary	174.60'	30.0' long x 12.0' breadth Broad-Crested Rectangular Weir
	_		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#4	Device 2	170.50'	3.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=6.35 cfs @ 12.52 hrs HW=173.82' (Free Discharge)

-2=Culvert (Inlet Controls 6.35 cfs @ 8.08 fps)

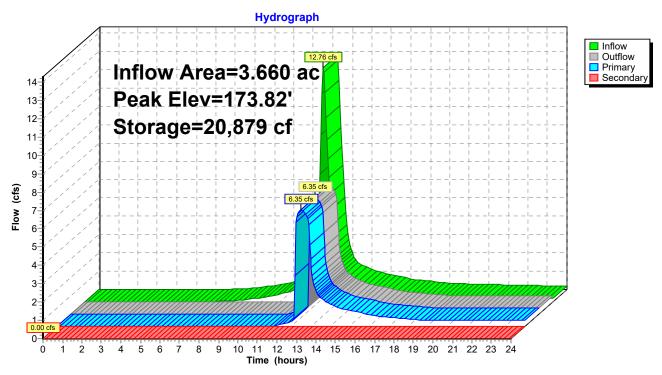
-1=Sharp-Crested Rectangular Weir (Passes < 13.64 cfs potential flow)

**-4=Orifice/Grate** (Passes < 0.42 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=169.00' (Free Discharge) 3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond 2 - Pond: 2 - Pond



Volume

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#### Summary for Pond 4 - Pond: 4 - Pond

Inflow Area = 9.080 ac, Inflow Depth > 3.37" for 25-YEAR STORM event

Inflow 29.01 cfs @ 12.17 hrs, Volume= 2.549 af

4.75 cfs @ 12.85 hrs, Volume= Outflow 1.372 af, Atten= 84%, Lag= 40.4 min

Primary 4.75 cfs @ 12.85 hrs, Volume= 1.372 af 0.00 cfs @ 0.00 hrs, Volume= Secondary = 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 125.54' @ 12.85 hrs Surf.Area= 14,796 sf Storage= 58,819 cf

Plug-Flow detention time= 238.6 min calculated for 1.372 af (54% of inflow)

Avail.Storage Storage Description

Center-of-Mass det. time= 126.7 min ( 956.9 - 830.2 )

Invert

#1	120.00'	79,242 cf <b>Custom</b>	Stage Data (Prismatic)Listed below	v (Recalc)
Elevation	Surf.Area	Inc.Store	Cum.Store	
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)	
120.00	6,749	0	0	
121.00	8,061	7,405	7,405	
122.00	9,434	8,748	16,153	
123.00	10,869	10,152	26,304	
124.00	12,365	11,617	37,921	
125.00	13,922	13,144	51,065	
126.00	15,541	14,732	65,796	
127.00	11,350	13,446	79,242	

Device	Routing	Invert	Outlet Devices
#1	Primary	120.40'	18.0" Round Culvert
			L= 53.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 120.40' / 120.00' S= 0.0075 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.77 sf
#2	Secondary	126.50'	
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#3	Device 1	125.00'	
			0.5' Crest Height
#4	Device 1	121.00'	3.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=4.74 cfs @ 12.85 hrs HW=125.54' (Free Discharge)

**-1=Culvert** (Passes 4.74 cfs of 17.83 cfs potential flow)

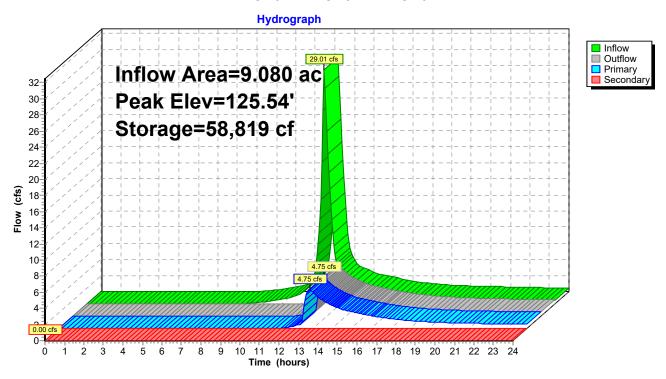
-3=Sharp-Crested Rectangular Weir (Weir Controls 4.25 cfs @ 2.72 fps)

4=Orifice/Grate (Orifice Controls 0.50 cfs @ 10.12 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=120.00' (Free Discharge)

2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 4 - Pond: 4 - Pond



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## **Summary for Pond 5 - Pond: 5 - Pond**

Inflow Area = 15.220 ac, Inflow Depth > 4.40" for 25-YEAR STORM event

Inflow 57.87 cfs @ 12.21 hrs, Volume= 5.575 af

19.41 cfs @ 12.62 hrs, Volume= Outflow 4.812 af, Atten= 66%, Lag= 24.8 min

19.41 cfs @ 12.62 hrs, Volume= Primary 4.812 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Peak Elev= 125.45' @ 12.62 hrs Surf.Area= 26,435 sf Storage= 112,279 cf

Plug-Flow detention time= 183.1 min calculated for 4.812 af (86% of inflow)

Center-of-Mass det. time= 124.0 min ( 931.0 - 807.1 )

Volume	Invert	Avail.Storage	Storage Description
#1	120.00'	187,159 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	15,063	0	0
121.00	17,014	16,039	16,039
122.00	19,025	18,020	34,058
123.00	21,096	20,061	54,119
124.00	23,228	22,162	76,281
125.00	25,421	24,325	100,605
126.00	27,674	26,548	127,153
127.00	29,988	28,831	155,984
128.00	32,362	31,175	187,159

Routing	Invert	Outlet Devices
Device 2	123.50'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
Primary	121.30'	24.0" Round Culvert
		L= 81.5' RCP, square edge headwall, Ke= 0.500
		Inlet / Outlet Invert= 121.30' / 115.25' S= 0.0742 '/' Cc= 0.900
		n= 0.012, Flow Area= 3.14 sf
Secondary	127.90'	30.0' long x 12.0' breadth Broad-Crested Rectangular Weir
		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
		Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
Device 2	121.30'	10.0" Vert. Orifice/Grate C= 0.600
	Device 2 Primary Secondary	Device 2 123.50' Primary 121.30' Secondary 127.90'

Primary OutFlow Max=19.38 cfs @ 12.62 hrs HW=125.45' (Free Discharge)

**-2=Culvert** (Passes 19.38 cfs of 26.84 cfs potential flow)

-1=Sharp-Crested Rectangular Weir (Weir Controls 14.31 cfs @ 4.56 fps)

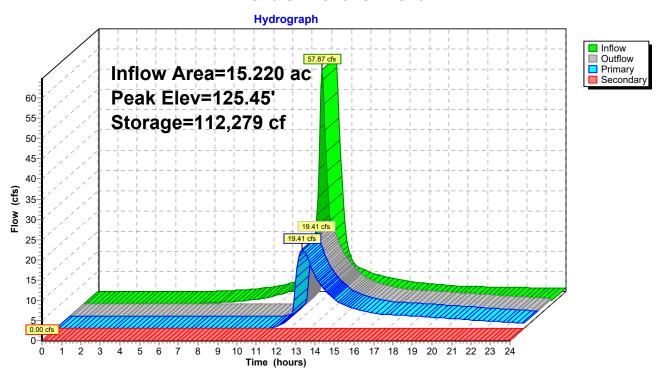
4=Orifice/Grate (Orifice Controls 5.07 cfs @ 9.30 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=120.00' (Free Discharge) 3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond 5 - Pond: 5 - Pond



# HydroCAD North Stonington Proposed\_Rev Type III 24-hr 50-YEAR STORM Rainfall=6.88"

Prepared by HDR, Inc

Printed 6/25/2021

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A: Runoff Area=4.190 ac Runoff Depth>4.25"

Tc=13.2 min CN=77 Runoff=16.42 cfs 1.483 af

Subcatchment1B: Runoff Area=4.570 ac Runoff Depth>4.68"

Tc=18.7 min CN=81 Runoff=17.24 cfs 1.782 af

**Subcatchment1C:** Runoff Area=11.850 ac Runoff Depth>4.90"

Tc=19.3 min CN=83 Runoff=45.97 cfs 4.838 af

Subcatchment2: Runoff Area=3.660 ac Runoff Depth>4.79"

Tc=16.2 min CN=82 Runoff=14.93 cfs 1.461 af

Subcatchment4: Runoff Area=9.080 ac Runoff Depth>4.04"

Tc=12.4 min CN=75 Runoff=34.74 cfs 3.053 af

Subcatchment5: Runoff Area=15.220 ac Runoff Depth>5.13"

Tc=15.3 min CN=85 Runoff=67.06 cfs 6.501 af

**Pond 1A - Pond: 1A - Pond**Peak Elev=130.54' Storage=33,114 cf Inflow=16.42 cfs 1.483 af

Primary=2.10 cfs 1.329 af Secondary=0.00 cfs 0.000 af Outflow=2.10 cfs 1.329 af

**Pond 1B - Pond: 1B - Pond**Peak Elev=124.12' Storage=44,133 cf Inflow=17.24 cfs 1.782 af

Primary=1.81 cfs 1.441 af Secondary=0.00 cfs 0.000 af Outflow=1.81 cfs 1.441 af

Pond 1C-Pond: 1C - Pond Peak Elev=119.25' Storage=95,892 cf Inflow=45.97 cfs 4.838 af

Primary=13.75 cfs 4.144 af Secondary=0.00 cfs 0.000 af Outflow=13.75 cfs 4.144 af

**Pond 2 - Pond: 2 - Pond**Peak Elev=174.32' Storage=24,291 cf Inflow=14.93 cfs 1.461 af

Primary=6.89 cfs 1.159 af Secondary=0.00 cfs 0.000 af Outflow=6.89 cfs 1.159 af

Pond 4 - Pond: 4 - Pond Peak Elev=125.90' Storage=64,317 cf Inflow=34.74 cfs 3.053 af

Primary=10.21 cfs 1.869 af Secondary=0.00 cfs 0.000 af Outflow=10.21 cfs 1.869 af

**Pond 5 - Pond: 5 - Pond**Peak Elev=125.96' Storage=126,080 cf Inflow=67.06 cfs 6.501 af

Primary=24.45 cfs 5.699 af Secondary=0.00 cfs 0.000 af Outflow=24.45 cfs 5.699 af

Total Runoff Area = 48.570 ac Runoff Volume = 19.119 af Average Runoff Depth = 4.72"

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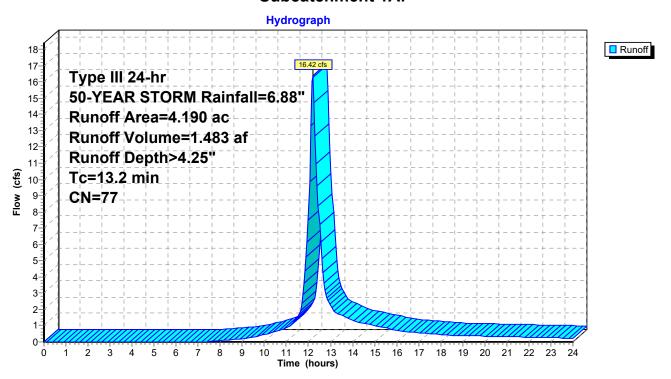
### **Summary for Subcatchment 1A:**

Runoff 16.42 cfs @ 12.18 hrs, Volume= 1.483 af, Depth> 4.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YEAR STORM Rainfall=6.88"

_	Area	(ac)	CN	Desc	cription		
*	4.	190	77				
	Тс	J		•	•		Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
_	13.2						Direct Entry, NRCS Part 630

#### **Subcatchment 1A:**



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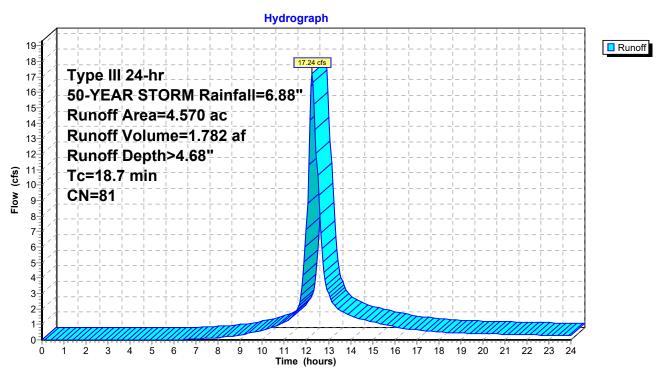
### **Summary for Subcatchment 1B:**

Runoff 17.24 cfs @ 12.25 hrs, Volume= 1.782 af, Depth> 4.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YEAR STORM Rainfall=6.88"

_	Area	(ac)	CN	Desc	cription		
*	4.	570	81				
_	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	18.7	(100	<u>, , , , , , , , , , , , , , , , , , , </u>	(1411)	(1000)	(010)	Direct Entry, NRCS Part 630

#### **Subcatchment 1B:**



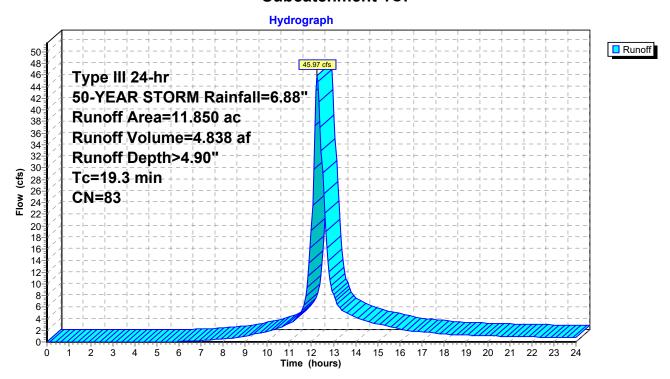
## **Summary for Subcatchment 1C:**

Runoff 45.97 cfs @ 12.26 hrs, Volume= 4.838 af, Depth> 4.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YEAR STORM Rainfall=6.88"

Area	(ac)	CN	Desc	cription		
* 11	.850	83				
Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10 3	,			•	` '	Direct Entry NRCS Part 630

#### **Subcatchment 1C:**



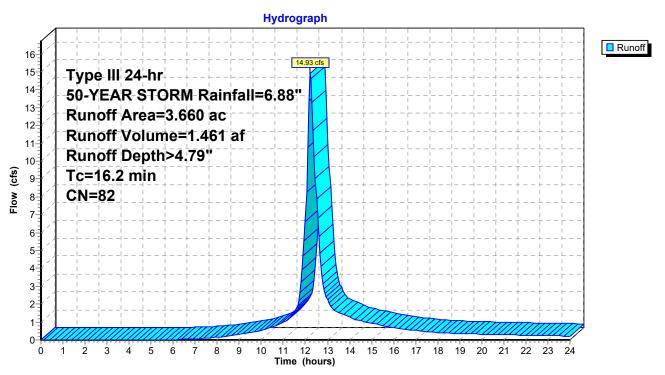
#### **Summary for Subcatchment 2:**

Runoff 14.93 cfs @ 12.22 hrs, Volume= 1.461 af, Depth> 4.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YEAR STORM Rainfall=6.88"

_	Area	(ac)	CN	Desc	cription		
,	3.	.660	82				
_							
	Tc	Leng	jth	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	16.2						Direct Entry NRCS Part 630

#### **Subcatchment 2:**



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### **Summary for Subcatchment 4:**

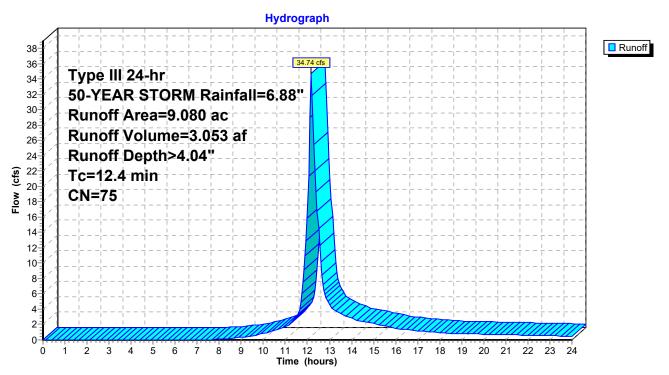
Runoff 34.74 cfs @ 12.17 hrs, Volume=

3.053 af, Depth> 4.04"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YEAR STORM Rainfall=6.88"

Area	(ac)	CN	Desc	cription		
* 9	.080	75				
Tc	Leng	th :	Slope	Velocity	Capacity	Description
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	<u> </u>
12.4						Direct Entry NRCS Part 630

#### Subcatchment 4:



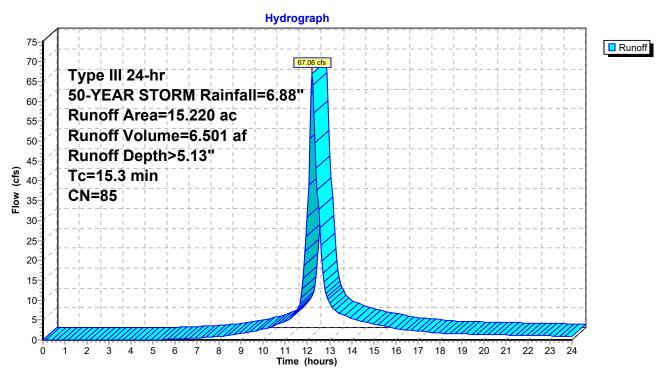
#### **Summary for Subcatchment 5:**

Runoff 67.06 cfs @ 12.21 hrs, Volume= 6.501 af, Depth> 5.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YEAR STORM Rainfall=6.88"

_	Area	(ac)	CN	Desc	cription		
*	15.	220	85				
	Tc	J			,		Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	15.3						Direct Entry, NRCS Part 630

#### Subcatchment 5:



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## **Summary for Pond 1A - Pond: 1A - Pond**

Inflow Area = 4.190 ac, Inflow Depth > 4.25" for 50-YEAR STORM event

Inflow = 16.42 cfs @ 12.18 hrs, Volume= 1.483 af

Outflow = 2.10 cfs @ 13.07 hrs, Volume= 1.329 af, Atten= 87%, Lag= 53.2 min

Primary = 2.10 cfs @ 13.07 hrs, Volume= 1.329 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 130.54' @ 13.07 hrs Surf.Area= 8,818 sf Storage= 33,114 cf

Plug-Flow detention time= 220.1 min calculated for 1.326 af (89% of inflow)

Center-of-Mass det. time= 171.2 min (992.3 - 821.1)

Volume	Invert	Avail.Storage	Storage Description
#1	123.00'	37,272 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
123.00	692	0	0
124.00	1,464	1,078	1,078
125.00	2,382	1,923	3,001
126.00	3,381	2,882	5,883
127.00	4,452	3,917	9,799
128.00	5,614	5,033	14,832
129.00	6,826	6,220	21,052
130.00	8,095	7,461	28,513
131.00	9,424	8,760	37,272

Routing	Invert	Outlet Devices
Secondary	130.90'	<b>20.0' long x 12.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
		Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
Primary	125.80'	24.0" Round Culvert
		L= 401.4' RCP, square edge headwall, Ke= 0.500
		Inlet / Outlet Invert= 125.80' / 123.80' S= 0.0050 '/' Cc= 0.900
		n= 0.012, Flow Area= 3.14 sf
Device 2	130.50'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
		0.5' Crest Height
Device 2	125.90'	6.0" Vert. Orifice/Grate C= 0.600
	Primary  Device 2	Secondary       130.90'         Primary       125.80'         Device 2       130.50'

Primary OutFlow Max=2.07 cfs @ 13.07 hrs HW=130.54' (Free Discharge)

**—2=Culvert** (Passes 2.07 cfs of 22.87 cfs potential flow)

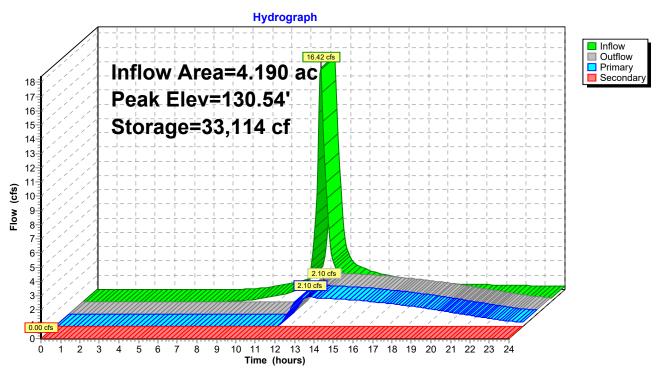
3=Sharp-Crested Rectangular Weir (Weir Controls 0.09 cfs @ 0.69 fps)

4=Orifice/Grate (Orifice Controls 1.98 cfs @ 10.09 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=123.00' (Free Discharge)

1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

#### Pond 1A - Pond: 1A - Pond



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## **Summary for Pond 1B - Pond: 1B - Pond**

Inflow Area = 4.570 ac, Inflow Depth > 4.68" for 50-YEAR STORM event

Inflow = 17.24 cfs @ 12.25 hrs, Volume= 1.782 af

Outflow = 1.81 cfs @ 13.67 hrs, Volume= 1.441 af, Atten= 89%, Lag= 85.2 min

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 124.12' @ 13.67 hrs Surf.Area= 11,759 sf Storage= 44,133 cf

Plug-Flow detention time= 295.1 min calculated for 1.441 af (81% of inflow)

Center-of-Mass det. time= 222.6 min ( 1,038.6 - 816.0 )

Volume	Invert	Avail.Storage	Storage Description
#1	119.00'	83.261 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
119.00	5,600	0	0
120.00	6,708	6,154	6,154
121.00	7,871	7,290	13,444
122.00	9,092	8,482	21,925
123.00	10,369	9,731	31,656
124.00	11,703	11,036	42,692
125.00	12,160	11,932	54,623
126.00	14,538	13,349	67,972
127.00	16,040	15,289	83,261

Device	Routing	Invert	Outlet Devices
#1	Primary	120.20'	15.0" Round Culvert
	•		L= 88.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 120.20' / 119.00' S= 0.0136 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.23 sf
#2	Secondary	126.90'	20.0' long x 12.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#3	Device 1	124.55'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 1	120.20'	6.0" Vert. Orifice/Grate C= 0.600

**Primary OutFlow** Max=1.81 cfs @ 13.67 hrs HW=124.12' (Free Discharge)

**—1=Culvert** (Passes 1.81 cfs of 10.73 cfs potential flow)

3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

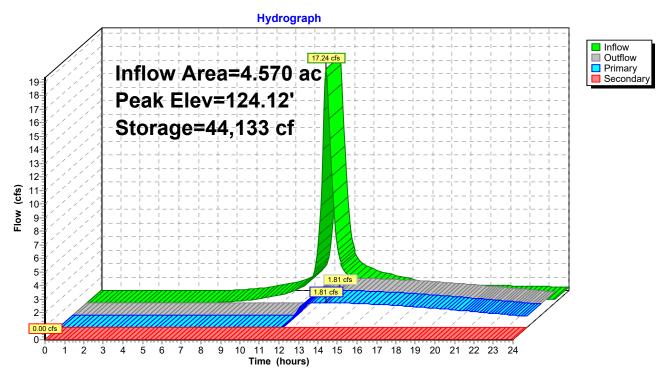
4=Orifice/Grate (Orifice Controls 1.81 cfs @ 9.23 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=119.00' (Free Discharge)

**2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

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Pond 1B - Pond: 1B - Pond



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## **Summary for Pond 1C-Pond: 1C - Pond**

Inflow Area = 11.850 ac, Inflow Depth > 4.90" for 50-YEAR STORM event

Inflow 45.97 cfs @ 12.26 hrs, Volume= 4.838 af

13.75 cfs @ 12.76 hrs, Volume= Outflow 4.144 af, Atten= 70%, Lag= 29.8 min

13.75 cfs @ 12.76 hrs, Volume= Primary = 4.144 af 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 119.25' @ 12.76 hrs Surf.Area= 26,492 sf Storage= 95,892 cf

Plug-Flow detention time= 157.1 min calculated for 4.144 af (86% of inflow)

Center-of-Mass det. time= 96.5 min ( 907.9 - 811.4 )

Volume	Invert	Avail.Storage	Storage Description
#1	114.00'	116,658 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
114.00	10,374	0	0
115.00	13,288	11,831	11,831
116.00	16,269	14,779	26,610
117.00	19,320	17,795	44,404
118.00	22,447	20,884	65,288
119.00	25,657	24,052	89,340
120.00	28,979	27,318	116,658

Jevice	Routing	invert	Outlet Devices
#1	Primary	115.70'	18.0" Round Culvert
			L= 91.6' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 115.70' / 115.00' S= 0.0076 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.77 sf
#2	Secondary	119.60'	30.0' long x 8.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.43 2.54 2.70 2.69 2.68 2.68 2.66 2.64 2.64
			2.64 2.65 2.65 2.66 2.66 2.68 2.70 2.74
#3	Device 1	116.90'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 1	115.70'	<b>10.0" Vert. Orifice/Grate</b> C= 0.600

Primary OutFlow Max=13.75 cfs @ 12.76 hrs HW=119.25' (Free Discharge)

-1=Culvert (Barrel Controls 13.75 cfs @ 7.78 fps)

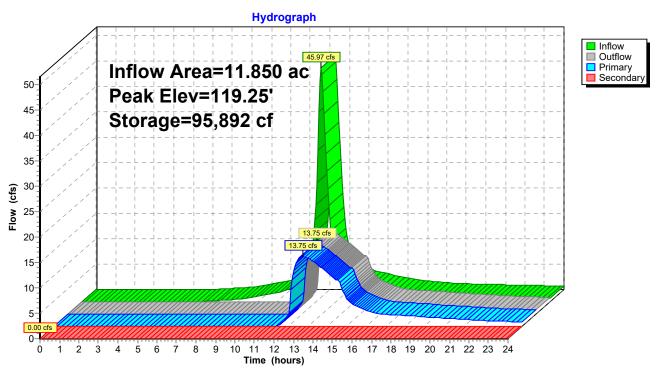
3=Sharp-Crested Rectangular Weir(Passes < 46.96 cfs potential flow)

**4=Orifice/Grate** (Passes < 4.65 cfs potential flow)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=114.00' (Free Discharge)

**2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Pond 1C-Pond: 1C - Pond



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## **Summary for Pond 2 - Pond: 2 - Pond**

Inflow Area = 3.660 ac, Inflow Depth > 4.79" for 50-YEAR STORM event

Inflow = 14.93 cfs @ 12.22 hrs, Volume= 1.461 af

Outflow = 6.89 cfs @ 12.55 hrs, Volume= 1.159 af, Atten= 54%, Lag= 19.7 min

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 174.32' @ 12.55 hrs Surf.Area= 7,091 sf Storage= 24,291 cf

Plug-Flow detention time= 143.4 min calculated for 1.157 af (79% of inflow)

Center-of-Mass det. time= 68.3 min ( 879.8 - 811.5 )

Volume	Inve	ert Avail.Sto	orage Storage	Description	
#1	169.0	00' 29,3	377 cf Custon	n Stage Data (Pr	rismatic)Listed below (Recalc)
Elevation	on	Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
169.0	00	2,429	0	0	
170.0	00	3,127	2,778	2,778	
171.0	00	3,912	3,520	6,298	
172.0	00	4,771	4,342	10,639	
173.0	00	5,697	5,234	15,873	
174.0	00	6,691	6,194	22,067	
175.0	00	7,929	7,310	29,377	
Device	Routing	Invert	Outlet Device	es	
#1	Device 2	172.70'	3.0' long Sha	arp-Crested Rec	ctangular Weir 2 End Contraction(s)
			0.5' Crest He	ight	- , ,
#2	Drimon	170 50'	12 0" Pound	1 Culvert	

			<del>•</del>
#1	Device 2	172.70'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#2	Primary	170.50'	12.0" Round Culvert
			L= 42.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 170.50' / 170.00' S= 0.0119 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf
#3	Secondary	174.60'	30.0' long x 12.0' breadth Broad-Crested Rectangular Weir
	_		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#4	Device 2	170.50'	3.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=6.89 cfs @ 12.55 hrs HW=174.32' (Free Discharge)

2=Culvert (Inlet Controls 6.89 cfs @ 8.78 fps)

1=Sharp-Crested Rectangular Weir(Passes < 25.24 cfs potential flow)

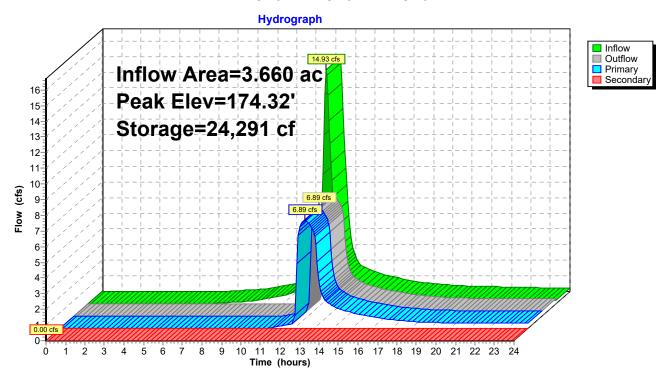
**-4=Orifice/Grate** (Passes < 0.45 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=169.00' (Free Discharge) 3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond 2 - Pond: 2 - Pond



Volume

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## Summary for Pond 4 - Pond: 4 - Pond

Inflow Area = 9.080 ac, Inflow Depth > 4.04" for 50-YEAR STORM event

Inflow 34.74 cfs @ 12.17 hrs, Volume= 3.053 af

10.21 cfs @ 12.60 hrs, Volume= Outflow 1.869 af, Atten= 71%, Lag= 26.0 min

10.21 cfs @ 12.60 hrs, Volume= Primary = 1.869 af 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 125.90' @ 12.60 hrs Surf.Area= 15,386 sf Storage= 64,317 cf

Plug-Flow detention time= 204.8 min calculated for 1.869 af (61% of inflow)

Avail.Storage Storage Description

Center-of-Mass det. time= 100.3 min ( 925.3 - 825.0 )

Invert

#1	120.00'	79,242 cf <b>Custon</b>	Stage Data (Prisma	atic)Listed below (Recalc)	
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
120.00	6,749	0	0		
121.00	8,061	7,405	7,405		
122.00	9,434	8,748	16,153		
123.00	10,869	10,152	26,304		
124.00	12,365	11,617	37,921		
125.00	13,922	13,144	51,065		
126.00	15,541	14,732	65,796		
127.00	11,350	13,446	79,242		

Device	Routing	Invert	Outlet Devices
#1	Primary	120.40'	18.0" Round Culvert
	•		L= 53.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 120.40' / 120.00' S= 0.0075 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.77 sf
#2	Secondary	126.50'	20.0' long x 12.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#3	Device 1	125.00'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 1	121.00'	3.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=10.18 cfs @ 12.60 hrs HW=125.90' (Free Discharge)

**-1=Culvert** (Passes 10.18 cfs of 18.55 cfs potential flow)

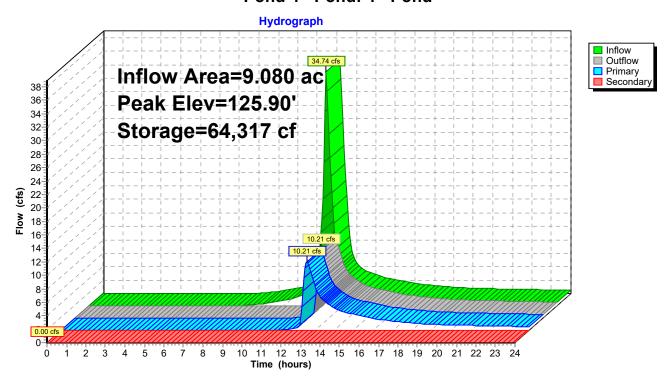
**-3=Sharp-Crested Rectangular Weir** (Weir Controls 9.66 cfs @ 3.79 fps)

4=Orifice/Grate (Orifice Controls 0.52 cfs @ 10.53 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=120.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond 4 - Pond: 4 - Pond



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#### **Summary for Pond 5 - Pond: 5 - Pond**

Inflow Area = 15.220 ac, Inflow Depth > 5.13" for 50-YEAR STORM event

Inflow = 67.06 cfs @ 12.21 hrs, Volume= 6.501 af

Outflow = 24.45 cfs @ 12.59 hrs, Volume= 5.699 af, Atten= 64%, Lag= 23.3 min

Primary = 24.45 cfs @ 12.59 hrs, Volume= 5.699 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Peak Elev= 125.96' @ 12.59 hrs Surf.Area= 27,587 sf Storage= 126,080 cf

Plug-Flow detention time= 169.3 min calculated for 5.688 af (87% of inflow)

Center-of-Mass det. time= 114.8 min ( 917.6 - 802.8 )

Volume	Invert	Avail.Storage	Storage Description
#1	120.00'	187,159 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	15,063	0	0
121.00	17,014	16,039	16,039
122.00	19,025	18,020	34,058
123.00	21,096	20,061	54,119
124.00	23,228	22,162	76,281
125.00	25,421	24,325	100,605
126.00	27,674	26,548	127,153
127.00	29,988	28,831	155,984
128.00	32,362	31,175	187,159

Device	Routing	Invert	Outlet Devices
#1	Device 2	123.50'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#2	Primary	121.30'	24.0" Round Culvert
			L= 81.5' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 121.30' / 115.25' S= 0.0742 '/' Cc= 0.900
			n= 0.012, Flow Area= 3.14 sf
#3	Secondary	127.90'	30.0' long x 12.0' breadth Broad-Crested Rectangular Weir
	-		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#4	Device 2	121.30'	10.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=24.43 cfs @ 12.59 hrs HW=125.96' (Free Discharge)

**2=Culvert** (Passes 24.43 cfs of 28.94 cfs potential flow)

1=Sharp-Crested Rectangular Weir (Weir Controls 19.02 cfs @ 5.13 fps)

4=Orifice/Grate (Orifice Controls 5.41 cfs @ 9.92 fps)

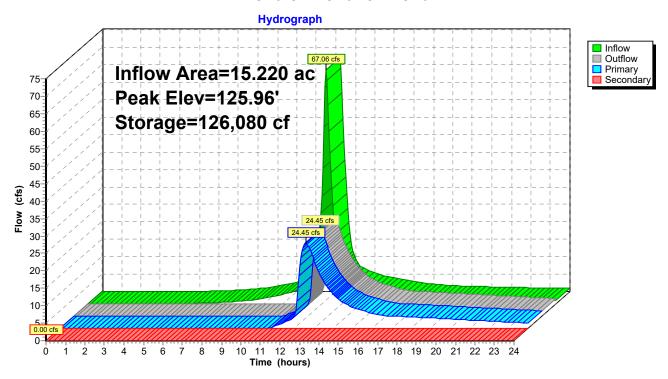
Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=120.00' (Free Discharge)

3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond 5 - Pond: 5 - Pond



# HydroCAD North Stonington Proposed\_RevType III 24-hr 100-YEAR STORM Rainfall=7.70"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1A: Runoff Area=4.190 ac Runoff Depth>4.99"

Tc=13.2 min CN=77 Runoff=19.22 cfs 1.742 af

Subcatchment1B: Runoff Area=4.570 ac Runoff Depth>5.44"

Tc=18.7 min CN=81 Runoff=19.96 cfs 2.073 af

**Subcatchment1C:** Runoff Area=11.850 ac Runoff Depth>5.67"

Tc=19.3 min CN=83 Runoff=52.94 cfs 5.603 af

Subcatchment2: Runoff Area=3.660 ac Runoff Depth>5.56"

Tc=16.2 min CN=82 Runoff=17.23 cfs 1.696 af

Subcatchment4: Runoff Area=9.080 ac Runoff Depth>4.76"

Tc=12.4 min CN=75 Runoff=40.93 cfs 3.603 af

Subcatchment5: Runoff Area=15.220 ac Runoff Depth>5.91"

Tc=15.3 min CN=85 Runoff=76.83 cfs 7.497 af

**Pond 1A - Pond: 1A - Pond**Peak Elev=130.91' Storage=36,406 cf Inflow=19.22 cfs 1.742 af

Primary=4.79 cfs 1.582 af Secondary=0.05 cfs 0.000 af Outflow=4.84 cfs 1.582 af

Pond 1B - Pond: 1B - Pond Peak Elev=124.70' Storage=50,963 cf Inflow=19.96 cfs 2.073 af

Primary=2.53 cfs 1.660 af Secondary=0.00 cfs 0.000 af Outflow=2.53 cfs 1.660 af

Pond 1C-Pond: 1C - Pond Peak Elev=119.74' Storage=109,182 cf Inflow=52.94 cfs 5.603 af

Primary=14.91 cfs 4.816 af Secondary=3.80 cfs 0.077 af Outflow=18.72 cfs 4.893 af

**Pond 2 - Pond: 2 - Pond**Peak Elev=174.71' Storage=27,099 cf Inflow=17.23 cfs 1.696 af

Primary=7.28 cfs 1.349 af Secondary=2.62 cfs 0.034 af Outflow=9.90 cfs 1.383 af

Pond 4 - Pond: 4 - Pond Peak Elev=126.25' Storage=69,489 cf Inflow=40.93 cfs 3.603 af

Primary=16.86 cfs 2.413 af Secondary=0.00 cfs 0.000 af Outflow=16.86 cfs 2.413 af

**Pond 5 - Pond: 5 - Pond**Peak Elev=126.48' Storage=140,738 cf Inflow=76.83 cfs 7.497 af

Primary=29.36 cfs 6.650 af Secondary=0.00 cfs 0.000 af Outflow=29.36 cfs 6.650 af

Total Runoff Area = 48.570 ac Runoff Volume = 22.214 af Average Runoff Depth = 5.49"

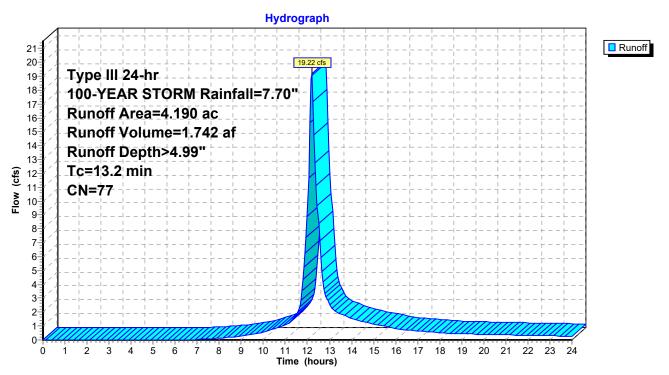
### **Summary for Subcatchment 1A:**

Runoff 19.22 cfs @ 12.18 hrs, Volume= 1.742 af, Depth> 4.99"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YEAR STORM Rainfall=7.70"

_	Area	(ac)	CN	Desc	cription		
,	4.	.190	77				
	Τ.		41.	01	\	0	Describetion
	IC	Leng	τn	Slope	velocity	Capacity	Description
_	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
	13.2						Direct Entry NRCS Part 630

#### **Subcatchment 1A:**



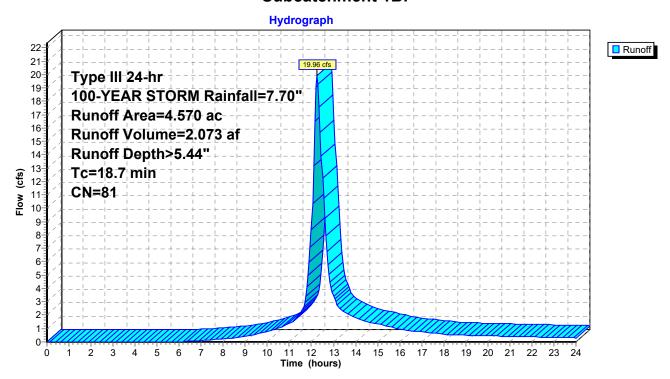
## **Summary for Subcatchment 1B:**

Runoff 19.96 cfs @ 12.25 hrs, Volume= 2.073 af, Depth> 5.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YEAR STORM Rainfall=7.70"

_	Area	(ac)	CN	Desc	cription		
*	4.	570	81				
_	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	18.7	(100	<u>, , , , , , , , , , , , , , , , , , , </u>	(1411)	(1000)	(010)	Direct Entry, NRCS Part 630

#### **Subcatchment 1B:**



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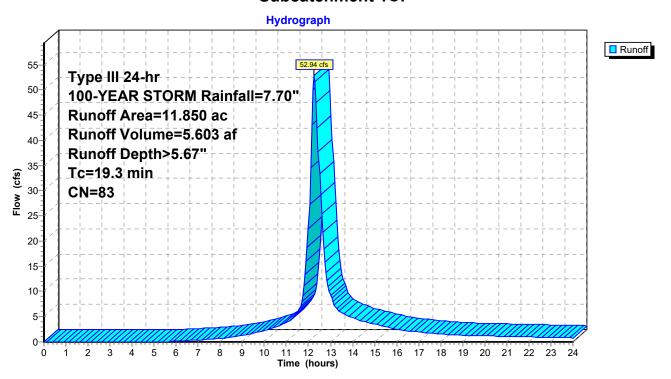
### **Summary for Subcatchment 1C:**

Runoff 52.94 cfs @ 12.26 hrs, Volume= 5.603 af, Depth> 5.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YEAR STORM Rainfall=7.70"

Area	(ac)	CN	Desc	cription		
* 11	.850	83				
Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10 3	,			•	` '	Direct Entry NRCS Part 630

#### **Subcatchment 1C:**



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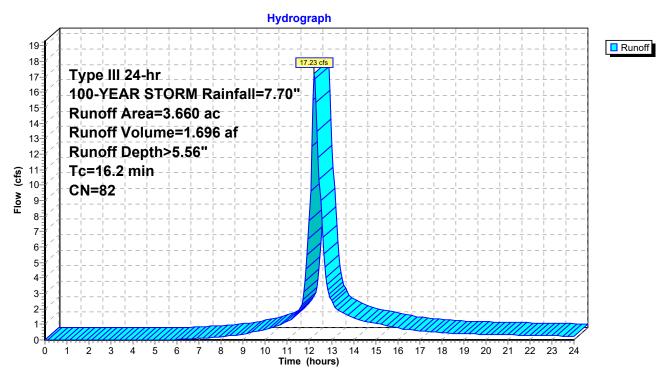
### **Summary for Subcatchment 2:**

Runoff 17.23 cfs @ 12.22 hrs, Volume= 1.696 af, Depth> 5.56"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YEAR STORM Rainfall=7.70"

_	Area	(ac)	CN	Desc	cription		
,	3.	660	82				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	16.2						Direct Entry, NRCS Part 630

# **Subcatchment 2:**



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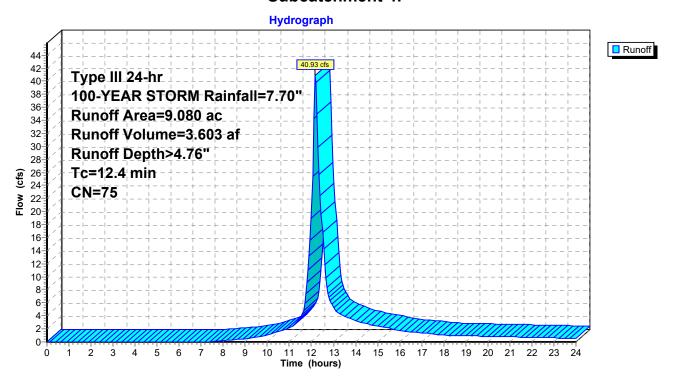
#### **Summary for Subcatchment 4:**

Runoff 40.93 cfs @ 12.17 hrs, Volume= 3.603 af, Depth> 4.76"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YEAR STORM Rainfall=7.70"

_	Area	(ac)	CN	Desc	cription		
•	9.	.080	75				
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	12.4						Direct Entry NDCS Part 630

#### Subcatchment 4:



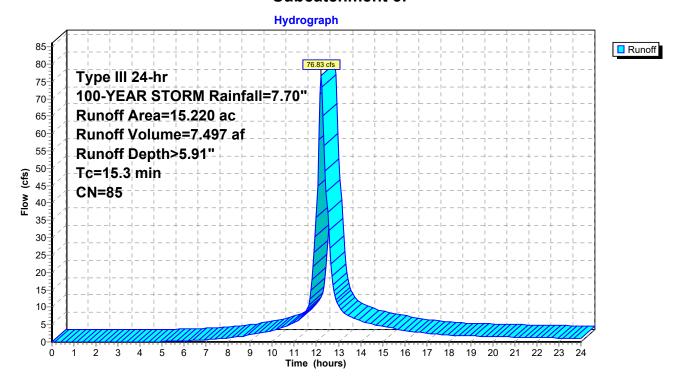
#### **Summary for Subcatchment 5:**

Runoff 76.83 cfs @ 12.21 hrs, Volume= 7.497 af, Depth> 5.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YEAR STORM Rainfall=7.70"

_	Area	(ac)	CN	Desc	cription		
,	15.	220	85				
_							
	Тс	Leng	th	Slope	Velocity	Capacity	Description
	(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)	
_	15.3						Direct Entry, NRCS Part 630

#### Subcatchment 5:



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# Summary for Pond 1A - Pond: 1A - Pond

Inflow Area = 4.190 ac, Inflow Depth > 4.99" for 100-YEAR STORM event

Inflow 19.22 cfs @ 12.18 hrs, Volume= 1.742 af

4.84 cfs @ 12.66 hrs, Volume= Outflow 1.582 af, Atten= 75%, Lag= 28.6 min

4.79 cfs @ 12.66 hrs, Volume= Primary = 1.582 af 0.05 cfs @ 12.65 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method. Time Span= 0.00-24.00 hrs. dt= 0.05 hrs Peak Elev= 130.91' @ 12.66 hrs Surf.Area= 9,301 sf Storage= 36,406 cf

Plug-Flow detention time= 205.2 min calculated for 1.582 af (91% of inflow)

Center-of-Mass det. time= 160.6 min ( 977.1 - 816.6 )

Volume	Invert	Avail.Storage	Storage Description
#1	123.00'	37,272 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
123.00	692	0	0
124.00	1,464	1,078	1,078
125.00	2,382	1,923	3,001
126.00	3,381	2,882	5,883
127.00	4,452	3,917	9,799
128.00	5,614	5,033	14,832
129.00	6,826	6,220	21,052
130.00	8,095	7,461	28,513
131.00	9,424	8,760	37,272

Device	Routing	Invert	Outlet Devices
#1	Secondary	130.90'	20.0' long x 12.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#2	Primary	125.80'	24.0" Round Culvert
	•		L= 401.4' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 125.80' / 123.80' S= 0.0050 '/' Cc= 0.900
			n= 0.012, Flow Area= 3.14 sf
#3	Device 2	130.50'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 2	125.90'	6.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=4.78 cfs @ 12.66 hrs HW=130.91' (Free Discharge)

**-2=Culvert** (Passes 4.78 cfs of 23.73 cfs potential flow)

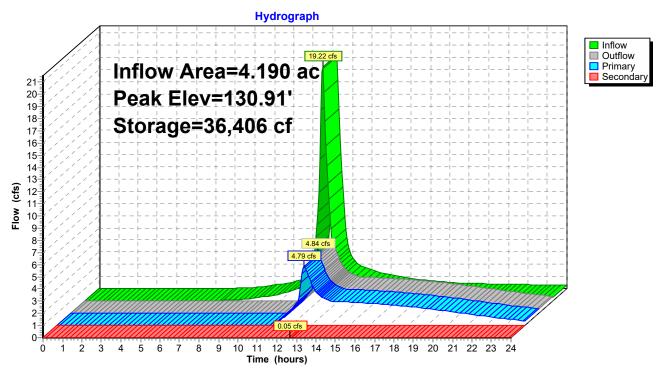
3=Sharp-Crested Rectangular Weir (Weir Controls 2.71 cfs @ 2.29 fps)

4=Orifice/Grate (Orifice Controls 2.06 cfs @ 10.50 fps)

Secondary OutFlow Max=0.03 cfs @ 12.65 hrs HW=130.91' (Free Discharge) 1=Broad-Crested Rectangular Weir (Weir Controls 0.03 cfs @ 0.21 fps)

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## Pond 1A - Pond: 1A - Pond



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# Summary for Pond 1B - Pond: 1B - Pond

Inflow Area = 4.570 ac, Inflow Depth > 5.44" for 100-YEAR STORM event

Inflow 19.96 cfs @ 12.25 hrs, Volume= 2.073 af

2.53 cfs @ 13.27 hrs, Volume= Outflow 1.660 af, Atten= 87%, Lag= 60.7 min

Primary 2.53 cfs @ 13.27 hrs, Volume= 1.660 af 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 124.70' @ 13.27 hrs Surf.Area= 12,022 sf Storage= 50,963 cf

Plug-Flow detention time= 296.4 min calculated for 1.656 af (80% of inflow)

Center-of-Mass det. time= 222.9 min ( 1,034.7 - 811.8 )

Volume	Invert	Avail.Storage	Storage Description
#1	119.00'	83,261 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
119.00	5,600	0	0
120.00	6,708	6,154	6,154
121.00	7,871	7,290	13,444
122.00	9,092	8,482	21,925
123.00	10,369	9,731	31,656
124.00	11,703	11,036	42,692
125.00	12,160	11,932	54,623
126.00	14,538	13,349	67,972
127.00	16,040	15,289	83,261

Device	Routing	Invert	Outlet Devices
#1	Primary	120.20'	15.0" Round Culvert
	•		L= 88.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 120.20' / 119.00' S= 0.0136 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.23 sf
#2	Secondary	126.90'	20.0' long x 12.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#3	Device 1	124.55'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 1	120.20'	6.0" Vert. Orifice/Grate C= 0.600

**Primary OutFlow** Max=2.52 cfs @ 13.27 hrs HW=124.70' (Free Discharge)

**-1=Culvert** (Passes 2.52 cfs of 11.52 cfs potential flow)

**3=Sharp-Crested Rectangular Weir** (Weir Controls 0.57 cfs @ 1.30 fps)

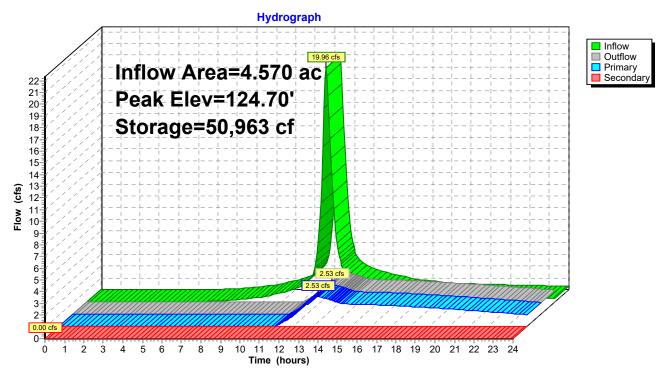
4=Orifice/Grate (Orifice Controls 1.95 cfs @ 9.92 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=119.00' (Free Discharge)

**2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

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## Pond 1B - Pond: 1B - Pond



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## **Summary for Pond 1C-Pond: 1C - Pond**

Inflow Area = 11.850 ac, Inflow Depth > 5.67" for 100-YEAR STORM event

Inflow 52.94 cfs @ 12.26 hrs, Volume= 5.603 af

18.72 cfs @ 12.70 hrs, Volume= Outflow 4.893 af, Atten= 65%, Lag= 26.5 min

14.91 cfs @ 12.70 hrs, Volume= Primary 4.816 af 3.80 cfs @ 12.70 hrs, Volume= Secondary = 0.077 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Peak Elev= 119.74' @ 12.70 hrs Surf.Area= 28,109 sf Storage= 109,182 cf

Plug-Flow detention time= 151.3 min calculated for 4.893 af (87% of inflow)

Center-of-Mass det. time= 95.5 min ( 902.8 - 807.3 )

Volume	Invert	Avail.Storage	Storage Description
#1	114.00'	116,658 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
114.00	10,374	0	0
115.00	13,288	11,831	11,831
116.00	16,269	14,779	26,610
117.00	19,320	17,795	44,404
118.00	22,447	20,884	65,288
119.00	25,657	24,052	89,340
120.00	28,979	27,318	116,658

Device	Routing	Invert	Outlet Devices
#1	Primary	115.70'	18.0" Round Culvert
			L= 91.6' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 115.70' / 115.00' S= 0.0076 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.77 sf
#2	Secondary	119.60'	30.0' long x 8.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.43 2.54 2.70 2.69 2.68 2.68 2.66 2.64 2.64
			2.64 2.65 2.65 2.66 2.66 2.68 2.70 2.74
#3	Device 1	116.90'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 1	115.70'	<b>10.0" Vert. Orifice/Grate</b> C= 0.600

Primary OutFlow Max=14.91 cfs @ 12.70 hrs HW=119.74' (Free Discharge)

-1=Culvert (Barrel Controls 14.91 cfs @ 8.44 fps)

**3=Sharp-Crested Rectangular Weir**(Passes < 64.42 cfs potential flow)

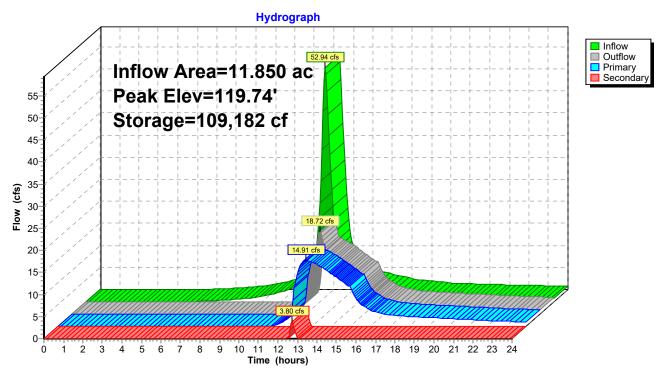
**4=Orifice/Grate** (Passes < 5.00 cfs potential flow)

Secondary OutFlow Max=3.73 cfs @ 12.70 hrs HW=119.74' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Weir Controls 3.73 cfs @ 0.90 fps)

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## Pond 1C-Pond: 1C - Pond



#3

Secondary

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## Summary for Pond 2 - Pond: 2 - Pond

Inflow Area = 3.660 ac, Inflow Depth > 5.56" for 100-YEAR STORM event
Inflow = 17.23 cfs @ 12.22 hrs, Volume= 1.696 af
Outflow = 9.90 cfs @ 12.47 hrs, Volume= 1.383 af, Atten= 43%, Lag= 15.4 min
Primary = 7.28 cfs @ 12.47 hrs, Volume= 1.349 af
Secondary = 2.62 cfs @ 12.47 hrs, Volume= 0.034 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 174.71' @ 12.47 hrs Surf.Area= 7,565 sf Storage= 27,099 cf

Plug-Flow detention time= 131.9 min calculated for 1.383 af (82% of inflow) Center-of-Mass det. time= 61.0 min (868.3 - 807.3)

Volume	Inv	vert Avail.	Storage	Storage	Description	
#1	169	.00' 2	9,377 cf	Custon	n Stage Data (Pr	rismatic)Listed below (Recalc)
Elevation	on	Surf.Area	Inc.	Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic	-feet)	(cubic-feet)	
169.0	00	2,429		0	0	
170.0	00	3,127	2	2,778	2,778	
171.0	00	3,912	;	3,520	6,298	
172.0	00	4,771	4	1,342	10,639	
173.0	00	5,697		5,234	15,873	
174.0	00	6,691		5,194	22,067	
175.0	00	7,929	•	7,310	29,377	
Device	Routing	j Inv	ert Outle	t Device	es	
#1	Device	2 172.	70' <b>3.0' l</b>	ong Sha	arp-Crested Red	ctangular Weir 2 End Contraction(s)
			0.5' (	rest He	ight	
#2	Primary	/ 170.	50' <b>12.0'</b> '	Round	d Culvert	
			L= 42	2.0' RC	P, square edge h	headwall, Ke= 0.500
			Inlet /	Outlet I	Invert= 170.50' /	170.00' S= 0.0119 '/' Cc= 0.900

n= 0.012, Flow Area= 0.79 sf

174.60' 30.0' long x 12.0' breadth Broad-Crested Rectangular Weir

Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64 #4 Device 2 170.50' **3.0" Vert. Orifice/Grate** C= 0.600

Primary OutFlow Max=7.27 cfs @ 12.47 hrs HW=174.70' (Free Discharge)

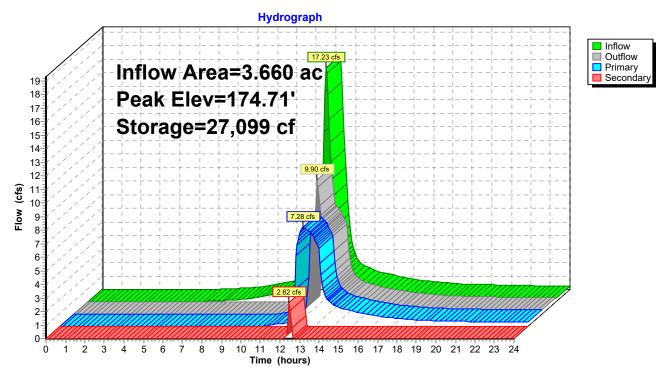
—2=Culvert (Inlet Controls 7.27 cfs @ 9.26 fps)

—1=Sharp-Crested Rectangular Weir (Passes < 35.80 cfs potential flow)</p>
—4=Orifice/Grate (Passes < 0.48 cfs potential flow)</p>

Secondary OutFlow Max=2.42 cfs @ 12.47 hrs HW=174.70' (Free Discharge)
—3=Broad-Crested Rectangular Weir (Weir Controls 2.42 cfs @ 0.81 fps)

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Pond 2 - Pond: 2 - Pond



Volume

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## Summary for Pond 4 - Pond: 4 - Pond

Inflow Area = 9.080 ac, Inflow Depth > 4.76" for 100-YEAR STORM event

Avail.Storage Storage Description

Inflow 40.93 cfs @ 12.17 hrs, Volume= 3.603 af

16.86 cfs @ 12.50 hrs, Volume= Outflow 2.413 af, Atten= 59%, Lag= 20.0 min

Primary 16.86 cfs @ 12.50 hrs, Volume= 2.413 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 126.25' @ 12.50 hrs Surf.Area= 14,511 sf Storage= 69,489 cf

Plug-Flow detention time= 181.2 min calculated for 2.413 af (67% of inflow)

Center-of-Mass det. time= 83.8 min ( 904.2 - 820.3 )

Invert

#1	120.00'	79,242 cf <b>Custo</b>	om Stage Data (P	rismatic)Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)		Cum.Store (cubic-feet)	
120.00	6,749	0	0	
121.00	8,061	7,405	7,405	
122.00	9,434	8,748	16,153	
123.00	10,869	10,152	26,304	
124.00	12,365	11,617	37,921	
125.00	13,922	13,144	51,065	
126.00	15,541	14,732	65,796	
127.00	11,350	13,446	79,242	

Device	Routing	Invert	Outlet Devices
#1	Primary	120.40'	18.0" Round Culvert
	•		L= 53.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 120.40' / 120.00' S= 0.0075 '/' Cc= 0.900
			n= 0.012, Flow Area= 1.77 sf
#2	Secondary	126.50'	20.0' long x 12.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#3	Device 1	125.00'	3.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
			0.5' Crest Height
#4	Device 1	121.00'	3.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=16.83 cfs @ 12.50 hrs HW=126.24' (Free Discharge)

**-1=Culvert** (Passes 16.83 cfs of 19.21 cfs potential flow)

-3=Sharp-Crested Rectangular Weir (Weir Controls 16.29 cfs @ 4.76 fps)

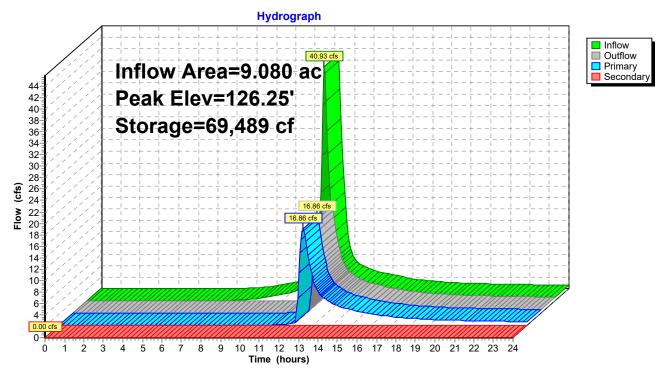
4=Orifice/Grate (Orifice Controls 0.53 cfs @ 10.89 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=120.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond 4 - Pond: 4 - Pond



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## **Summary for Pond 5 - Pond: 5 - Pond**

Inflow Area = 15.220 ac, Inflow Depth > 5.91" for 100-YEAR STORM event

Inflow 76.83 cfs @ 12.21 hrs, Volume= 7.497 af

29.36 cfs @ 12.58 hrs, Volume= Outflow 6.650 af, Atten= 62%, Lag= 22.3 min

29.36 cfs @ 12.58 hrs, Volume= Primary 6.650 af 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Peak Elev= 126.48' @ 12.58 hrs Surf.Area= 28,788 sf Storage= 140,738 cf

Plug-Flow detention time= 158.4 min calculated for 6.636 af (89% of inflow)

Center-of-Mass det. time= 107.1 min ( 906.0 - 798.9 )

Volume	Invert	Avail.Storage	Storage Description
#1	120.00'	187,159 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	15,063	0	0
121.00	17,014	16,039	16,039
122.00	19,025	18,020	34,058
123.00	21,096	20,061	54,119
124.00	23,228	22,162	76,281
125.00	25,421	24,325	100,605
126.00	27,674	26,548	127,153
127.00	29,988	28,831	155,984
128.00	32,362	31,175	187,159

Device	Routing	Invert	Outlet Devices
#1	Device 2	123.50'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#2	Primary	121.30'	24.0" Round Culvert
			L= 81.5' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 121.30' / 115.25' S= 0.0742 '/' Cc= 0.900
			n= 0.012, Flow Area= 3.14 sf
#3	Secondary	127.90'	30.0' long x 12.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.57 2.62 2.70 2.67 2.66 2.67 2.66 2.64
#4	Device 2	121.30'	10.0" Vert. Orifice/Grate C= 0.600

Primary OutFlow Max=29.33 cfs @ 12.58 hrs HW=126.48' (Free Discharge)

**-2=Culvert** (Passes 29.33 cfs of 30.92 cfs potential flow)

-1=Sharp-Crested Rectangular Weir (Weir Controls 23.60 cfs @ 5.64 fps)

4=Orifice/Grate (Orifice Controls 5.73 cfs @ 10.51 fps)

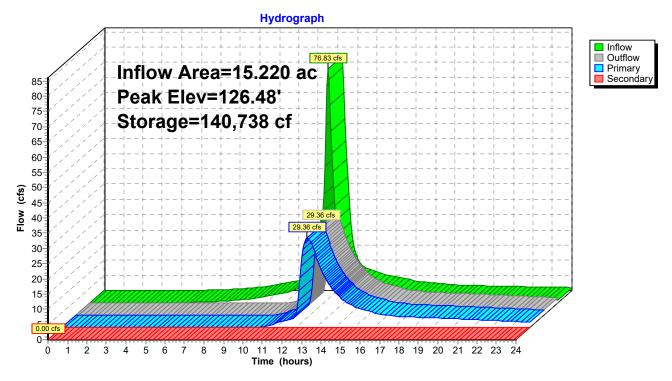
Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=120.00' (Free Discharge)

3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Printed 6/25/2021

Page 100

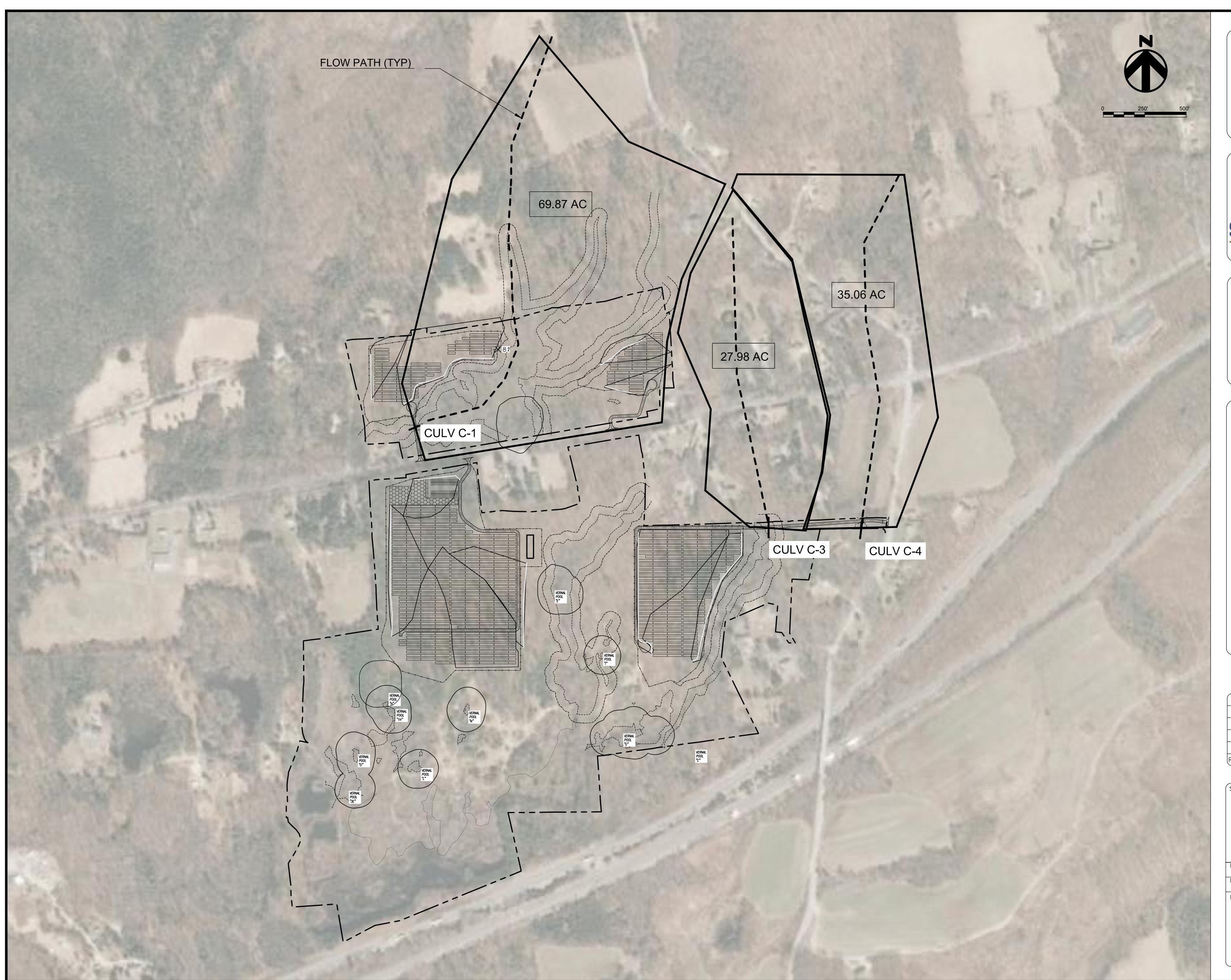
#### Pond 5 - Pond: 5 - Pond





# Appendix I

Culvert, Ditch, and Water Quality Calculations







# NOT FOR CONSTRUCTION

# STONINGTON SOLAR

428, PROVIDENCE-NEW LONDON TURNPIKE NORTH STONINGTON, CT 06359, USA LAT: 41.431830°N LON: 71.821514°W

STONINGTON, CT

	DE IONIED FOR DERIVIT	00/05/04
3	RE-ISSUED FOR PERMIT	06/25/21
2	RE-ISSUED FOR PERMIT	05/28/21
1	RE-ISSUED FOR PERMIT	02/19/21
0	ISSUED FOR PERMIT	09/30/20
REV. NO	DESCRIPTION	DATE

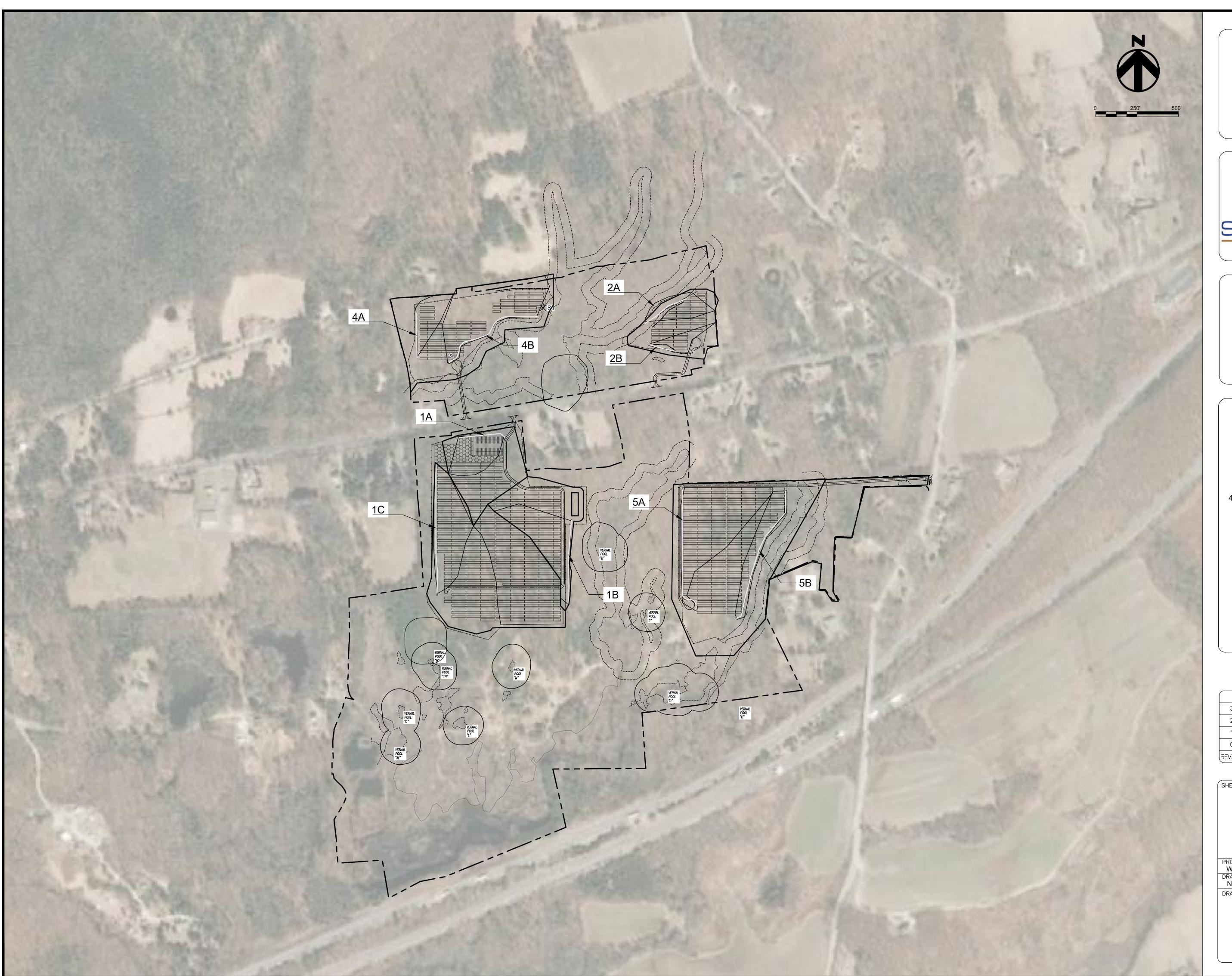
SHEET TITLE:

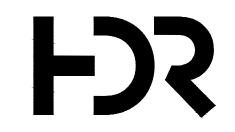
# CULVERT DRAINAGE AREAS

l .			
	PROJ. MGR.	PROJ. ENGR.	DATE:
	WK	MB	5/28/21
	DRAWN BY:	CHECKED BY:	SCALE:
	NC	CP	1:250

DRAWING NO.

**EXHIBIT** 







# NOT FOR CONSTRUCTION

# STONINGTON SOLAR

428, PROVIDENCE-NEW LONDON TURNPIKE NORTH STONINGTON, CT 06359, USA LAT: 41.431830°N LON: 71.821514°W

STONINGTON, CT

_		
3	RE-ISSUED FOR PERMIT	06/25/21
2	RE-ISSUED FOR PERMIT	05/28/21
1	RE-ISSUED FOR PERMIT	02/19/21
0	ISSUED FOR PERMIT	09/30/20
REV. NO	DESCRIPTION	DATE

SHEET TITLE:

# DITCH DRAINAGE AREA EXHIBIT

l			
	PROJ. MGR.	PROJ. ENGR.	DATE:
	WK	MB	5/28/21
	DRAWN BY:	CHECKED BY:	SCALE:
	NC	CP	1:250

DRAWING NO.

**EXHIBIT** 

Stonington Solar Array Facility North Stonington, CT SRC

9/23/2020

**Culvert Calculations** 

Storm Event: 50-yr

Culvert	Туре	Est. Peak Flow Q 25 (cfs)	Est. Peak Flow Q 50-yr (cfs)	Length (ft)	Shape	Span (ft)	Rise (ft)	Area (sf)	Open Area (sf)	OR (Open Area) / Length	Ex Stream Slope (%)	Arch Req'd
C-1	New	126.13	163.36	20	Box	9	3.00	27	18	0.90	0.40	No
C-3	New	69.43	87.23	20	Arch (Bottomless)	9	2.92	26.25	26.25	1.31	5.4	Yes
C-4	Existing	83.36	104.78	20	Arch (Bottomless)	10	3.46	34.58	34.58	1.73	3.5	Yes

# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	126.13	2	748	758,965				CULVERT C-1
2	SCS Runoff	21.52	2	740	112,804				CULVERT C-2
3	SCS Runoff	69.43	2	740	363,040				CULVERT C-3
4	SCS Runoff	83.36	2	742	460,589				CULVERT C-4
ST	ONINGTON-	CULVER	ΓS.gpw		Return F	Period: 25	Year	Wednesda	y, 09 / 23 / 2020

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

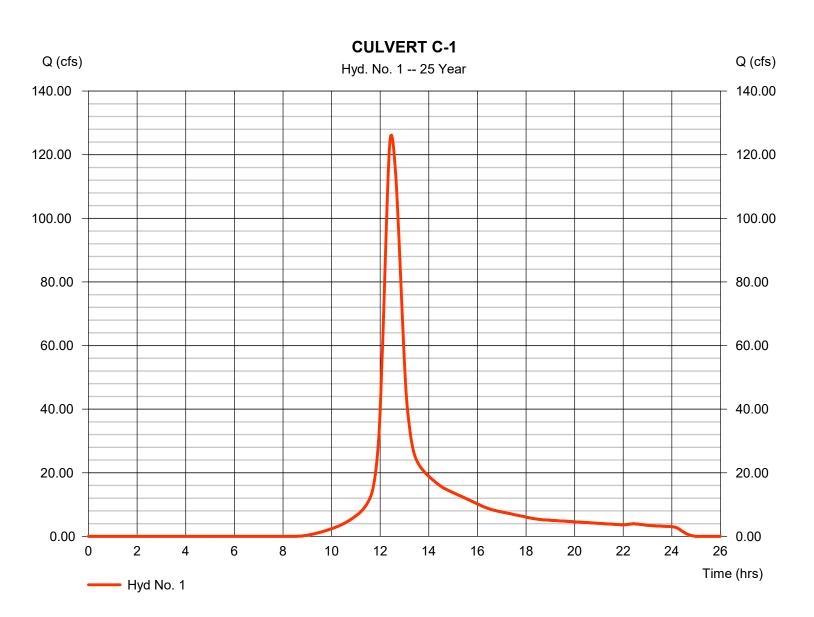
Wednesday, 09 / 23 / 2020

# Hyd. No. 1

**CULVERT C-1** 

Hydrograph type = SCS Runoff Peak discharge = 126.13 cfsStorm frequency = 25 yrs Time to peak  $= 12.47 \, hrs$ Time interval = 2 min Hyd. volume = 758.965 cuft Drainage area Curve number = 74\* = 69.870 acBasin Slope = 4.5 % Hydraulic length = 2679 ftTc method Time of conc. (Tc) = LAG  $= 39.45 \, \text{min}$ Total precip. = 5.77 inDistribution = Type III Storm duration Shape factor = 484 = 24 hrs

<sup>\*</sup> Composite (Area/CN) =  $[(35.000 \times 79) + (34.870 \times 68)] / 69.870$ 



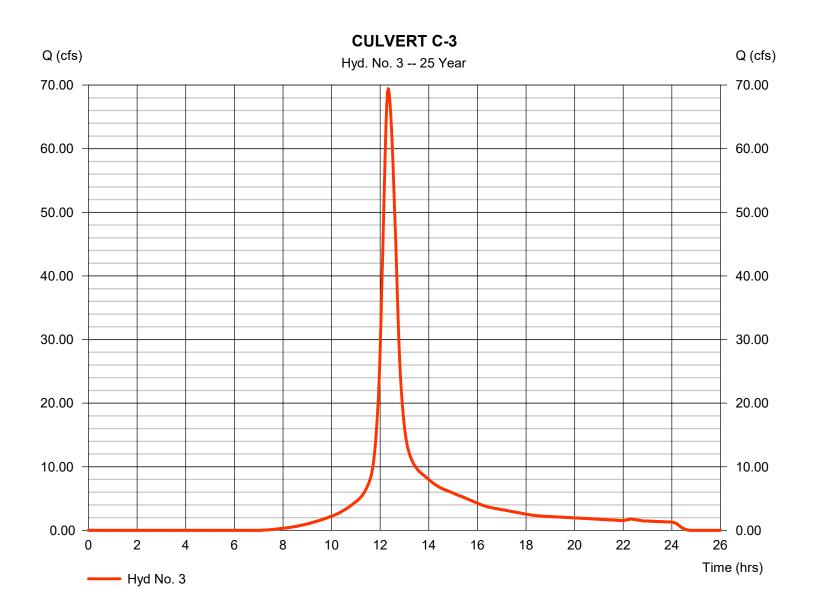
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Wednesday, 09 / 23 / 2020

# Hyd. No. 3

#### **CULVERT C-3**

Hydrograph type = SCS Runoff Peak discharge  $= 69.43 \, \text{cfs}$ Storm frequency Time to peak = 25 yrs $= 12.33 \, hrs$ Time interval = 2 min Hyd. volume = 363.040 cuft Drainage area = 27.980 ac Curve number = 80 = 3.2 % Hydraulic length Basin Slope = 1874 ftTc method = LAG Time of conc. (Tc) = 29.42 min Total precip. = 5.77 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



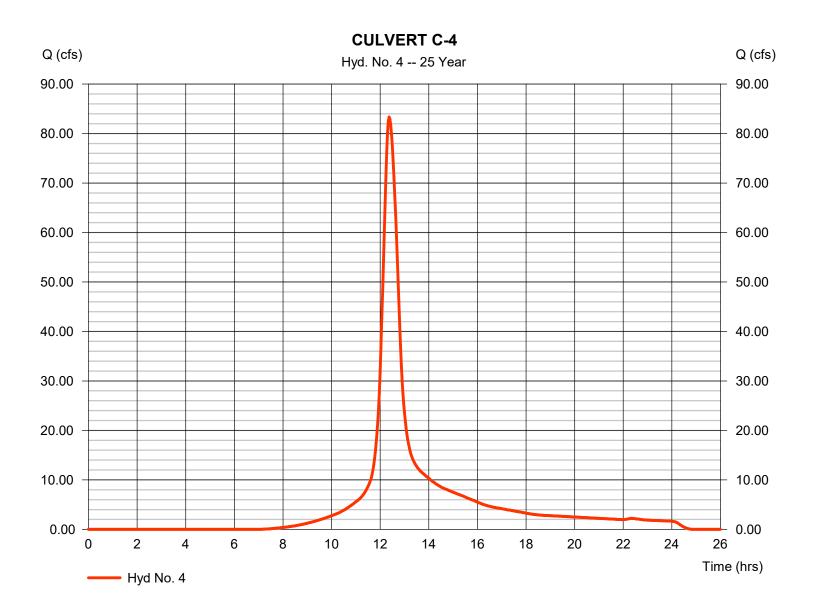
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Wednesday, 09 / 23 / 2020

# Hyd. No. 4

#### **CULVERT C-4**

Hydrograph type = SCS Runoff Peak discharge = 83.36 cfsStorm frequency Time to peak = 25 yrs  $= 12.37 \, hrs$ Time interval = 2 min Hyd. volume = 460,589 cuft Drainage area = 35.060 ac Curve number = 80 Hydraulic length Basin Slope = 3.6 % = 2196 ftTc method = LAG Time of conc. (Tc) = 31.49 min Total precip. = 5.77 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



# Hydrograph Summary Report Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	163.36	2	746	981,098				CULVERT C-1
2	SCS Runoff	28.04	2	740	146,448				CULVERT C-2
3	SCS Runoff	87.23	2	740	458,092				CULVERT C-3
4	SCS Runoff	104.78	2	742	581,182				CULVERT C-4
ST	ONINGTON-0	CULVERT	ΓS.gpw		Return F	Period: 50 Y	⁄ear	Wednesday	y, 09 / 23 / 2020

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

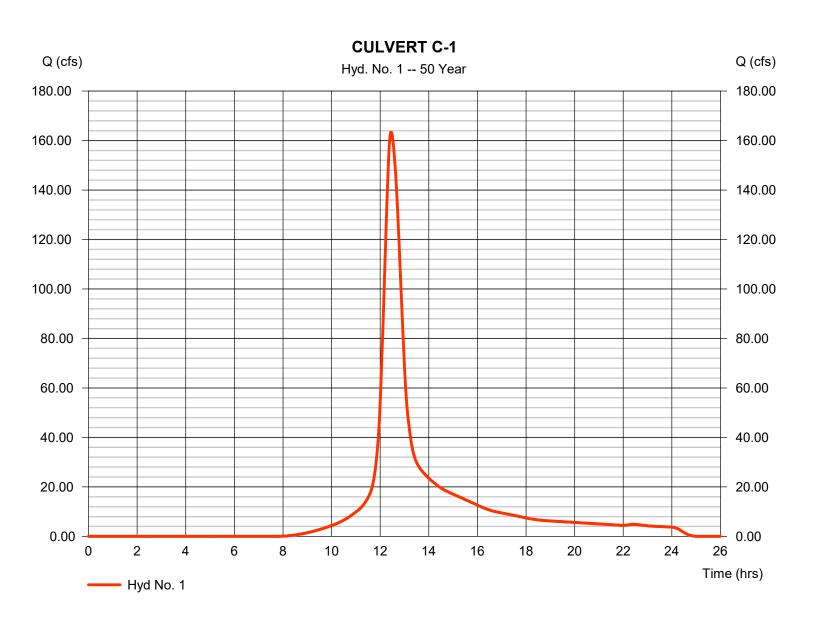
Wednesday, 09 / 23 / 2020

# Hyd. No. 1

**CULVERT C-1** 

Hydrograph type = SCS Runoff Peak discharge = 163.36 cfsStorm frequency = 50 yrsTime to peak  $= 12.43 \, hrs$ Time interval = 2 min Hyd. volume = 981.098 cuft Drainage area Curve number = 74\* = 69.870 acBasin Slope = 4.5 % Hydraulic length = 2679 ftTc method Time of conc. (Tc) = LAG  $= 39.45 \, \text{min}$ Total precip. = 6.80 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) =  $[(35.000 \times 79) + (34.870 \times 68)] / 69.870$ 



Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Wednesday, 09 / 23 / 2020

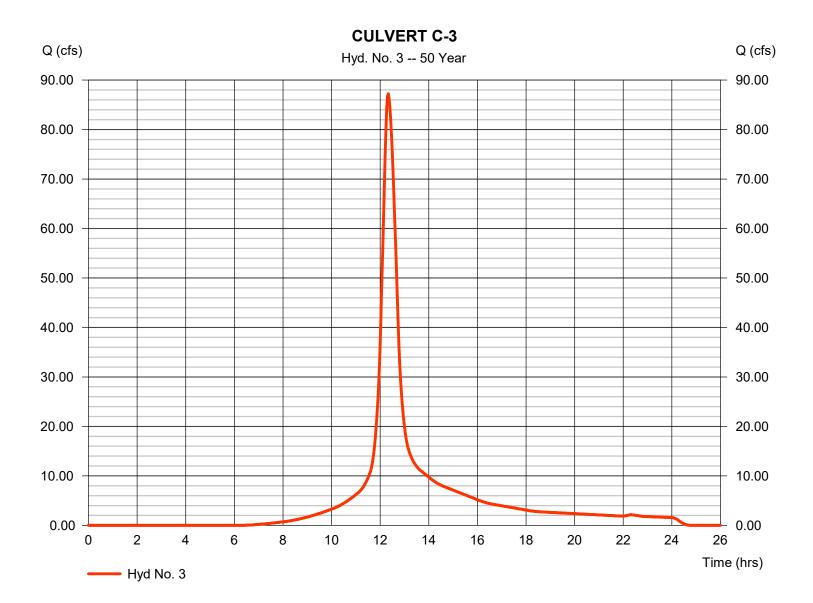
# Hyd. No. 3

#### **CULVERT C-3**

Hydrograph type = SCS Runoff Storm frequency = 50 yrsTime interval = 2 min Drainage area = 27.980 ac = 3.2 % Basin Slope Tc method = LAG Total precip. = 6.80 inStorm duration = 24 hrs

Peak discharge = 87.23 cfs
Time to peak = 12.33 hrs
Hyd. volume = 458,092 cuft
Curve number = 80

Curve number = 80
Hydraulic length = 1874 ft
Time of conc. (Tc) = 29.42 min
Distribution = Type III
Shape factor = 484



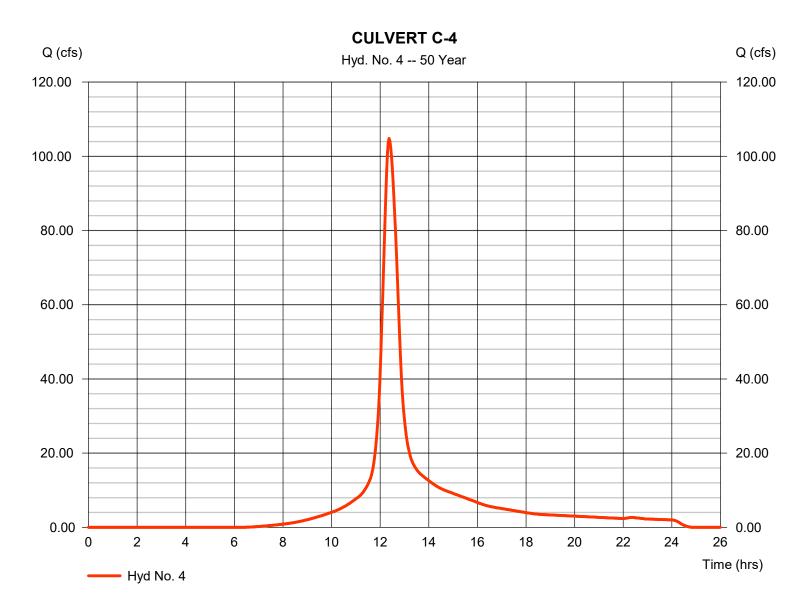
Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2018 by Autodesk, Inc. v2018.3

Wednesday, 09 / 23 / 2020

# Hyd. No. 4

#### **CULVERT C-4**

Hydrograph type = SCS Runoff Peak discharge = 104.78 cfsStorm frequency = 50 yrsTime to peak  $= 12.37 \, hrs$ Time interval = 2 min Hyd. volume = 581,182 cuft Drainage area Curve number = 35.060 ac= 80 Basin Slope = 3.6 % Hydraulic length = 2196 ftTc method = LAG Time of conc. (Tc) = 31.49 min Total precip. = 6.80 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484



# **HY-8 Culvert Analysis Report**

# Water Surface Profile Plot for Culvert: CULV C-1

Crossing - CULVERT C-1, Design Discharge - 163.4 cfs
Culvert - CULV C-1, Culvert Discharge - 163.4 cfs

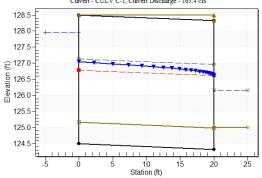


Table 1 - Culvert Summary Table: CULV C-1

Total Discha rge (cfs)	Culvert Discha rge (cfs)	Headw ater Elevati on (ft)	Inlet Contro I Depth (ft)	Outlet Contro I Depth (ft)	Flow Typ e	Norma I Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwat er Depth (ft)	Outlet Velocit y (ft/s)	Tailwat er Velocit y (ft/s)	***************************************
10.00	10.00	125.62	0.418	0.451	3-M 2t	0.360	0.251	0.276	0.272	2.592	2.887	Straight Culvert  Inlet Elevation (invert): 125.17 ft, Outlet Elevation
25.34	25.34	125.99	0.795	0.818	2-M 2c	0.632	0.467	0.467	0.453	3.878	3.848	(invert): 125.00 ft  Culvert Length: 20.00 ft, Culvert Slope: 0.0085
40.67	40.67	126.28	1.090	1.112	2-M 2c	0.843	0.640	0.640	0.582	4.539	4.419	***************************************
56.01	56.01	126.54	1.349	1.371	2-M 2c	1.024	0.792	0.792	0.686	5.050	4.842	Site Data - CULV C-1
71.34	71.34	126.77	1.585	1.606	2-M 2c	1.186	0.931	0.931	0.776	5.474	5.180	Site Data Option: Culvert Invert Data
86.68	86.68	126.99	1.801	1.826	2-M 2c	1.335	1.060	1.060	0.855	5.842	5.466	Inlet Station: 0.00 ft Inlet Elevation: 124.50 ft
102.02	102.02	127.20	2.001	2.033	2-M 2c	1.474	1.181	1.181	0.927	6.168	5.715	Outlet Station: 20.00 ft
117.35	117.35	127.40	2.192	2.231	2-M 2c	1.606	1.297	1.297	0.992	6.462	5.936	Outlet Elevation: 124.33 ft
132.69	132.69	127.59	2.375	2.420	2-M 2c	1.731	1.408	1.408	1.053	6.732	6.135	Number of Barrels: 1
148.02	148.02	127.77	2.551	2.602	2-M 2c	1.851	1.514	1.514	1.110	6.982	6.318	Culvert Data Summary - CULV C-1
163.36	163.36	127.94	2.723	2.778	2-M 2c	1.966	1.617	1.617	1.164	7.216	6.487	Barrel Shape: Concrete Box Barrel Span: 14.00 ft

Barrel Rise: 4.00 ft
Barrel Material: Concrete
Embedment: 8.00 in

Barrel Manning's n: 0.0120 (top and sides)

Manning's n: 0.0350 (bottom)

Culvert Type: Straight

Inlet Configuration: Square Edge (90°) Headwall

Inlet Depression: None

# **Crossing Discharge Data**

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 10 cfs Design Flow: 163.36 cfs Maximum Flow: 163.36 cfs

Table 2 - Summary of Culvert Flows at Crossing: CULVERT C-1

Headwater Elevation (ft)	Total Discharge (cfs)	CULV C-1 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
125.62	10.00	10.00	0.00	1
125.99	25.34	25.34	0.00	1
126.28	40.67	40.67	0.00	1
126.54	56.01	56.01	0.00	1
126.77	71.34	71.34	0.00	1
126.99	86.68	86.68	0.00	1
127.20	102.02	102.02	0.00	1
127.40	117.35	117.35	0.00	1
127.59	132.69	132.69	0.00	1
127.77	148.02	148.02	0.00	1
127.94	163.36	163.36	0.00	1
128.50	214.82	214.82	0.00	Overtopping

Table 3 - Downstream Channel Rating Curve (Crossing: CULVERT C-1)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
10.00	125.27	0.27	2.89	0.58	1.07
25.34	125.45	0.45	3.85	0.96	1.15
40.67	125.58	0.58	4.42	1.23	1.19
56.01	125.69	0.69	4.84	1.46	1.22
71.34	125.78	0.78	5.18	1.65	1.24
86.68	125.85	0.85	5.47	1.81	1.26
102.02	125.93	0.93	5.71	1.97	1.27
117.35	125.99	0.99	5.94	2.11	1.29
132.69	126.05	1.05	6.14	2.23	1.30
148.02	126.11	1.11	6.32	2.36	1.31
163.36	126.16	1.16	6.49	2.47	1.31

#### Tailwater Channel Data - CULVERT C-1

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 10.00 ft

Side Slope (H:V): 10.00 (\_:1)

Channel Slope: 0.0340

Channel Manning's n: 0.0350

Channel Invert Elevation: 125.00 ft

## Roadway Data for Crossing: CULVERT C-1

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 200.00 ft
Crest Elevation: 128.50 ft
Roadway Surface: Gravel
Roadway Top Width: 20.00 ft

# Water Surface Profile Plot for Culvert: CULV C-3

Crossing - CULVERT C-3, Design Discharge - 87.2 cfs
Culvert - CULV C-3, Culvert Discharge - 87.2 cfs

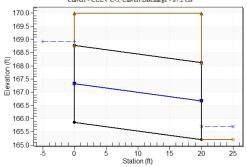


Table 7 - Culvert Summary Table: CULV C-3

Total Discha rge (cfs)	Culvert Discha rge (cfs)	Headw ater Elevati on (ft)	Inlet Contro I Depth (ft)	Outlet Contro I Depth (ft)	Flow Typ e	Norma I Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwat er Depth (ft)	Outlet Velocit y (ft/s)	Tailwat er Velocit y (ft/s)
10.00	10.00	166.47	0.610	0.0*	1-S2 n	0.329	0.339	0.329	0.134	3.441	2.628
17.72	17.72	166.76	0.900	0.0*	1-S2 n	0.476	0.499	0.476	0.189	4.261	3.288
25.45	25.45	167.01	1.153	0.062	1-S2 n	0.603	0.636	0.603	0.234	4.861	3.784
33.17	33.17	167.25	1.386	0.239	1-S2 n	0.721	0.760	0.721	0.274	5.348	4.194
40.89	40.89	167.47	1.614	0.422	1-S2 n	0.832	0.875	0.832	0.311	5.755	4.545
48.62	48.62	167.71	1.846	0.612	1-S2 n	0.940	0.984	0.940	0.345	6.110	4.857
56.34	56.34	167.94	2.077	0.810	1-S2 n	1.044	1.087	1.044	0.376	6.421	5.138
64.06	64.06	168.17	2.308	1.017	1-S2 n	1.148	1.185	1.151	0.406	6.685	5.396
71.78	71.78	168.38	2.519	1.235	1-S2 n	1.252	1.279	1.252	0.435	6.943	5.634
79.51	79.51	168.59	2.729	1.463	1-S2 n	1.356	1.370	1.356	0.462	7.166	5.855
87.23	87.23	168.92	2.939	3.064	7-M 2c	1.461	1.458	1.458	0.488	7.380	6.064

\* Full Flow Headwater elevation is below inlet invert.

\*

Straight Culvert

Inlet Elevation (invert): 165.86 ft, Outlet Elevation (invert): 165.21 ft

Culvert Length: 20.01 ft, Culvert Slope: 0.0325

#### Site Data - CULV C-3

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 165.86 ft Outlet Station: 20.00 ft Outlet Elevation: 165.21 ft

Number of Barrels: 1

#### **Culvert Data Summary - CULV C-3**

Barrel Shape: Arch, Open Bottom

Barrel Span: 9.00 ft Barrel Rise: 2.92 ft

Barrel Material: Corrugated Steel

Embedment: 0.00 in

Barrel Manning's n: 0.0350 (top and sides)

Manning's n: 0.0350 (bottom)

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: None

# **Crossing Discharge Data**

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 10 cfs Design Flow: 87.23 cfs Maximum Flow: 87.23 cfs

Table 8 - Summary of Culvert Flows at Crossing: CULVERT C-3

Headwater Elevation (ft)	Total Discharge (cfs)	CULV C-3 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
166.47	10.00	10.00	0.00	1
166.76	17.72	17.72	0.00	1
167.01	25.45	25.45	0.00	1
167.25	33.17	33.17	0.00	1
167.47	40.89	40.89	0.00	1
167.71	48.62	48.62	0.00	1
167.94	56.34	56.34	0.00	1
168.17	64.06	64.06	0.00	1
168.38	71.78	71.78	0.00	1
168.59	79.51	79.51	0.00	1
168.92	87.23	87.23	0.00	1
170.00	129.81	129.81	0.00	Overtopping

Table 9 - Downstream Channel Rating Curve (Crossing: CULVERT C-3)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
10.00	165.34	0.13	2.63	0.48	1.27
17.72	165.40	0.19	3.29	0.67	1.35
25.45	165.44	0.23	3.78	0.83	1.39
33.17	165.48	0.27	4.19	0.98	1.43
40.89	165.52	0.31	4.55	1.11	1.46
48.62	165.55	0.34	4.86	1.23	1.48
56.34	165.59	0.38	5.14	1.34	1.50
64.06	165.62	0.41	5.40	1.45	1.52
71.78	165.64	0.43	5.63	1.55	1.54
79.51	165.67	0.46	5.86	1.64	1.55
87.23	165.70	0.49	6.06	1.74	1.57

#### Tailwater Channel Data - CULVERT C-3

Tailwater Channel Option: Trapezoidal Channel

Bottom Width: 28.00 ft Side Slope (H:V): 3.00 (\_:1) Channel Slope: 0.0570 Channel Manning's n: 0.0350

Channel Invert Elevation: 165.21 ft

# Roadway Data for Crossing: CULVERT C-3

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft Crest Elevation: 170.00 ft Roadway Surface: Gravel Roadway Top Width: 20.00 ft

# Water Surface Profile Plot for Culvert: CULV C-4

Crossing - CULVERT C-4, Design Discharge - 104.8 cfs
Culvert - CULV C-4, Culvert Discharge - 104.8 cfs

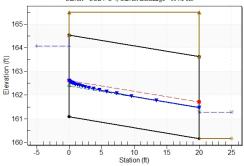


Table 10 - Culvert Summary Table: CULV C-4

Total Discha rge (cfs)	Culvert Discha rge (cfs)	Headw ater Elevati on (ft)	Inlet Contro I Depth (ft)	Outlet Contro I Depth (ft)	Flow Typ e	Norma I Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwat er Depth (ft)	Outlet Velocit y (ft/s)	Tailwat er Velocit y (ft/s)
10.00	10.00	161.64	0.558	0.0*	1-S2 n	0.275	0.316	0.275	0.321	3.678	2.481
19.48	19.48	161.96	0.876	0.0*	1-S2 n	0.419	0.494	0.419	0.464	4.745	3.060
28.96	28.96	162.23	1.147	0.0*	1-S2 n	0.541	0.645	0.541	0.575	5.496	3.449
38.43	38.43	162.47	1.393	0.0*	1-S2 n	0.649	0.780	0.649	0.668	6.105	3.749
47.91	47.91	162.70	1.623	0.139	1-S2 n	0.751	0.904	0.751	0.750	6.611	3.996
57.39	57.39	162.93	1.850	0.319	1-S2 n	0.849	1.021	0.849	0.823	7.050	4.207
66.87	66.87	163.16	2.083	0.504	1-S2 n	0.942	1.132	0.942	0.890	7.438	4.392
76.35	76.35	163.40	2.315	0.696	1-S2 n	1.033	1.239	1.033	0.951	7.788	4.557
85.82	85.82	163.63	2.548	0.893	1-S2 n	1.121	1.340	1.121	1.009	8.106	4.707
95.30	95.30	163.86	2.776	1.099	1-S2 n	1.208	1.437	1.215	1.063	8.358	4.845
104.78	104.78	164.07	2.987	1.312	1-S2 n	1.295	1.531	1.302	1.114	8.620	4.972

\* Full Flow Headwater elevation is below inlet invert.

Straight Culvert

Inlet Elevation (invert): 161.08 ft, Outlet Elevation (invert): 160.17 ft

Culvert Length: 20.02 ft, Culvert Slope: 0.0455

#### Site Data - CULV C-4

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 161.08 ft Outlet Station: 20.00 ft Outlet Elevation: 160.17 ft

Number of Barrels: 1

#### Culvert Data Summary - CULV C-4

Barrel Shape: Arch, Open Bottom

Barrel Span: 10.00 ft Barrel Rise: 3.46 ft

Barrel Material: Corrugated Steel

Embedment: 0.00 in

Barrel Manning's n: 0.0350 (top and sides)

Manning's n: 0.0350 (bottom)

Culvert Type: Straight

Inlet Configuration: Thin Edge Projecting

Inlet Depression: None

## **Crossing Discharge Data**

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 10 cfs
Design Flow: 104.78 cfs
Maximum Flow: 104.78 cfs

Table 11 - Summary of Culvert Flows at Crossing: CULVERT C-4

Headwater Elevation (ft)	Total Discharge (cfs)	CULV C-4 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
161.64	10.00	10.00	0.00	1
161.96	19.48	19.48	0.00	1
162.23	28.96	28.96	0.00	1
162.47	38.43	38.43	0.00	1
162.70	47.91	47.91	0.00	1
162.93	57.39	57.39	0.00	1
163.16	66.87	66.87	0.00	1
163.40	76.35	76.35	0.00	1
163.63	85.82	85.82	0.00	1
163.86	95.30	95.30	0.00	1
164.07	104.78	104.78	0.00	1
165.50	168.02	168.02	0.00	Overtopping

Table 12 - Downstream Channel Rating Curve (Crossing: CULVERT C-4)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)	Velocity (ft/s)	Shear (psf)	Froude Number
10.00	160.49	0.32	2.48	0.40	0.85
19.48	160.63	0.46	3.06	0.58	0.89
28.96	160.74	0.57	3.45	0.72	0.92
38.43	160.84	0.67	3.75	0.83	0.94
47.91	160.92	0.75	4.00	0.94	0.95
57.39	160.99	0.82	4.21	1.03	0.97
66.87	161.06	0.89	4.39	1.11	0.98
76.35	161.12	0.95	4.56	1.19	0.99
85.82	161.18	1.01	4.71	1.26	0.99
95.30	161.23	1.06	4.85	1.33	1.00
104.78	161.28	1.11	4.97	1.39	1.01

#### Tailwater Channel Data - CULVERT C-4

Tailwater Channel Option: Trapezoidal Channel

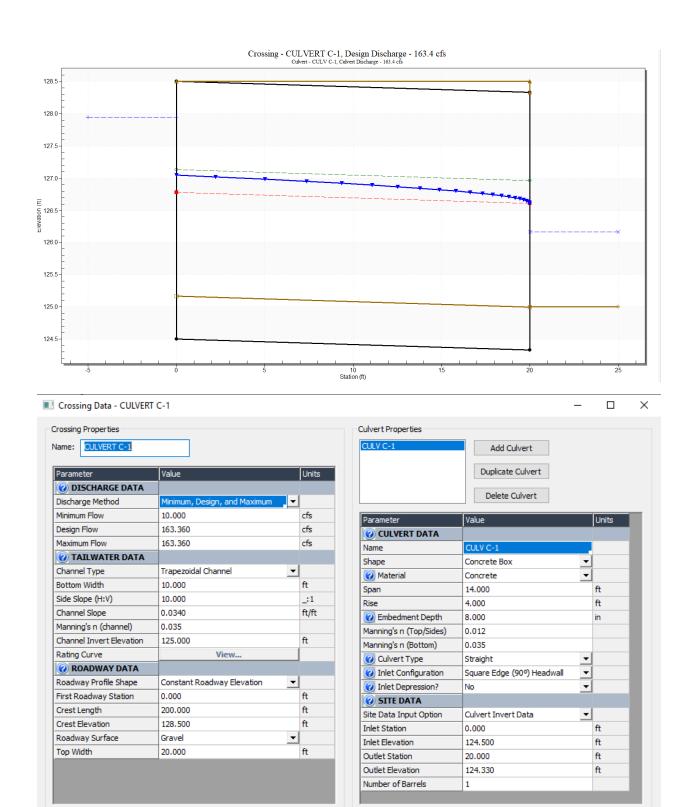
Bottom Width: 10.00 ft Side Slope (H:V): 8.00 (\_:1) Channel Slope: 0.0200 Channel Manning's n: 0.0350

Channel Invert Elevation: 160.17 ft

#### Roadway Data for Crossing: CULVERT C-4

Roadway Profile Shape: Constant Roadway Elevation

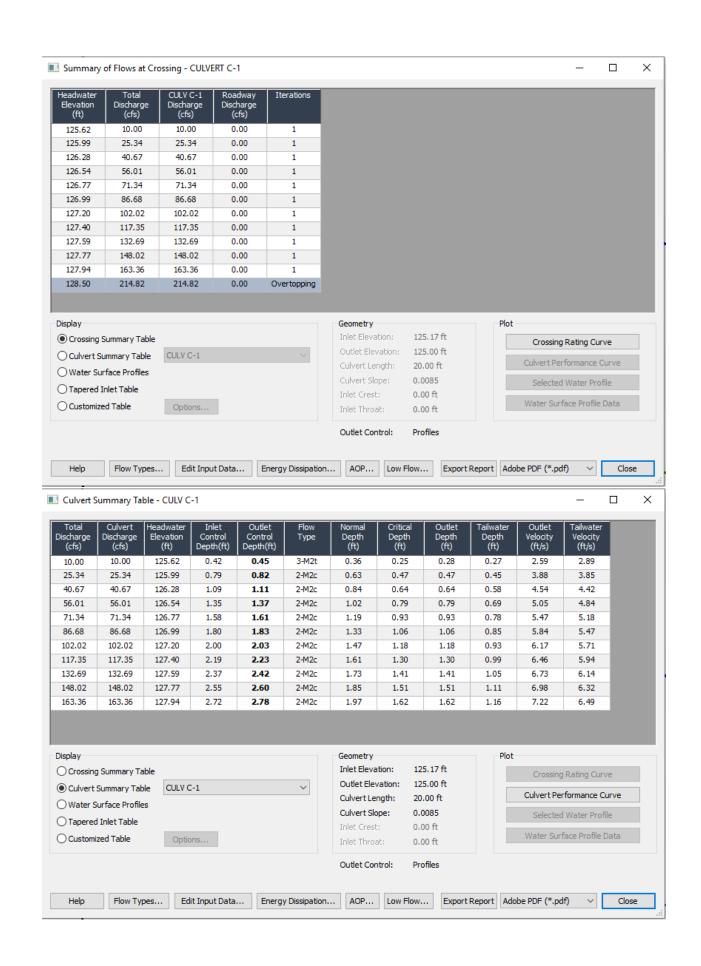
Crest Length: 100.00 ft Crest Elevation: 165.50 ft Roadway Surface: Gravel Roadway Top Width: 20.00 ft

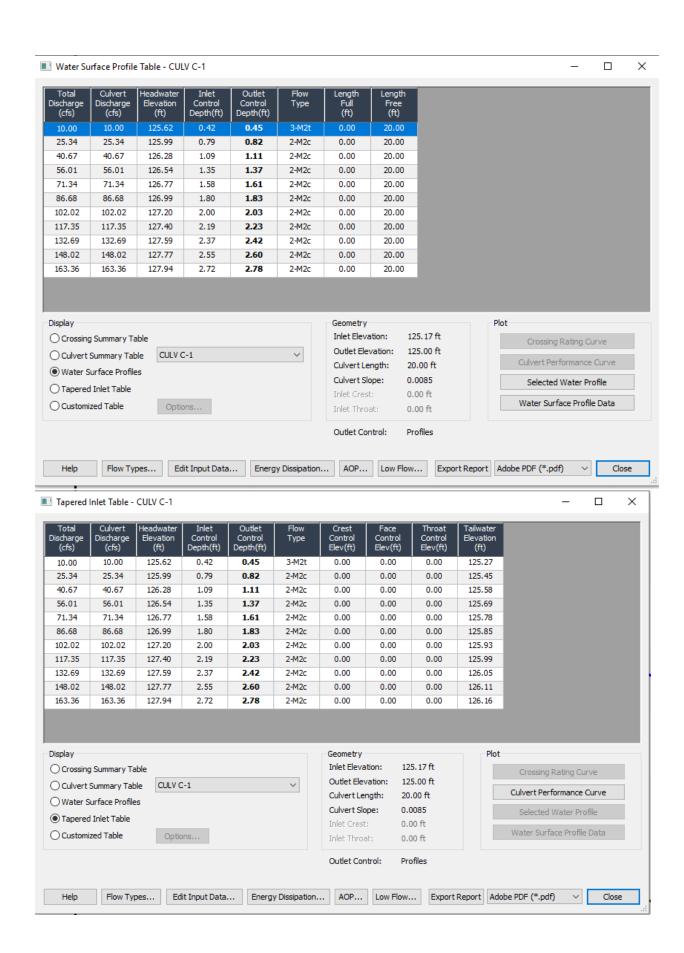


Click on any (i) icon for help on a specific topic Low Flow AOP Energy Dissipation Analyze Crossing

OK

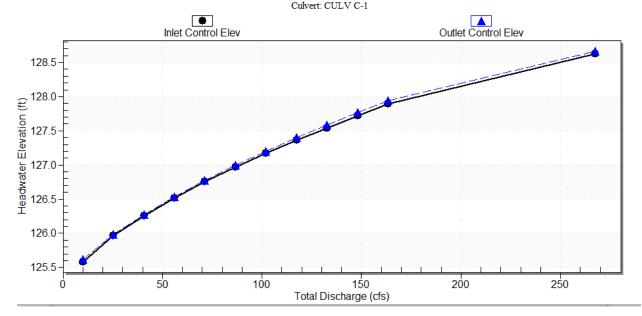
Cancel



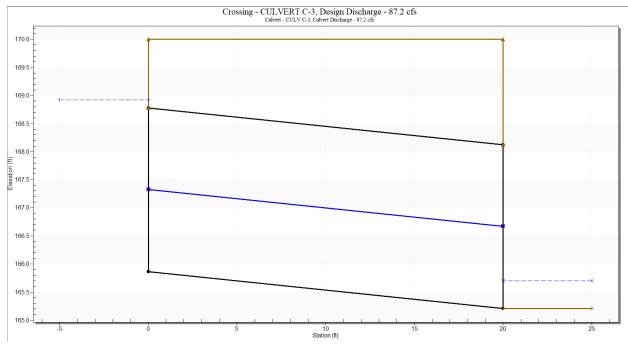


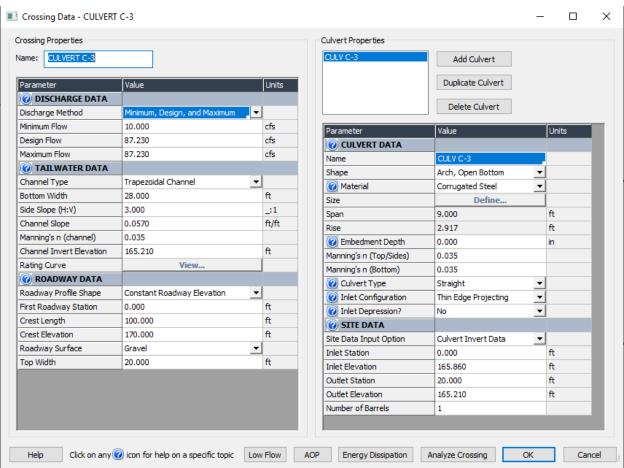
Total ischarge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth(ft)	Outlet Control Depth(ft)	Flow Type	Crest Control Elev(ft)	Face Control Elev(ft)	Throat Control Elev(ft)	Tailwater Elevation (ft)	
10.00	10.00	125.62	0.42	0.45	3-M2t	0.00	0.00	0.00	125.27	
25.34	25.34	125.99	0.79	0.82	2-M2c	0.00	0.00	0.00	125.45	
40.67	40.67	126.28	1.09	1.11	2-M2c	0.00	0.00	0.00	125.58	
56.01	56.01	126.54	1.35	1.37	2-M2c	0.00	0.00	0.00	125.69	
71.34	71.34	126.77	1.58	1.61	2-M2c	0.00	0.00	0.00	125.78	
86.68	86.68	126.99	1.80	1.83	2-M2c	0.00	0.00	0.00	125.85	
102.02	102.02	127.20	2.00	2.03	2-M2c	0.00	0.00	0.00	125.93	
117.35	117.35	127.40	2.19	2.23	2-M2c	0.00	0.00	0.00	125.99	
132.69	132.69	127.59	2.37	2.42	2-M2c	0.00	0.00	0.00	126.05	
148.02	148.02	127.77	2.55	2.60	2-M2c	0.00	0.00	0.00	126.11	
163.36	163.36	127.94	2,72	2.78	2-M2c	0.00	0.00	0.00	126, 16	
100.00						3.55	0.00	0.00	120.10	
						Geometry			Plot	
Display O Crossin	g Summary Ta	able				Geometry Inlet Eleva	ation: 12	5.17 ft		Crossing Rating Curve
Display  Crossini  Culvert	Summary Tab	able CULV (	C-1		V	Geometry	ation: 12			
Display  Crossing  Culvert  Water S	•	able CULV (	0-1		V	Geometry Inlet Eleva Outlet Elev Culvert Le Culvert Slo	ation: 12 vation: 12 ngth: 20 ope: 0.0	5.17 ft 5.00 ft .00 ft		Crossing Rating Curve
Display  Crossing  Culvert  Water S	Summary Tab Surface Profile d Inlet Table	able CULV (	C-1		~	Geometry Inlet Eleva Outlet Elev Culvert Le	vation: 12 vation: 12 ngth: 20 ope: 0.0	5.17 ft 5.00 ft		Crossing Rating Curve  Culvert Performance Curve

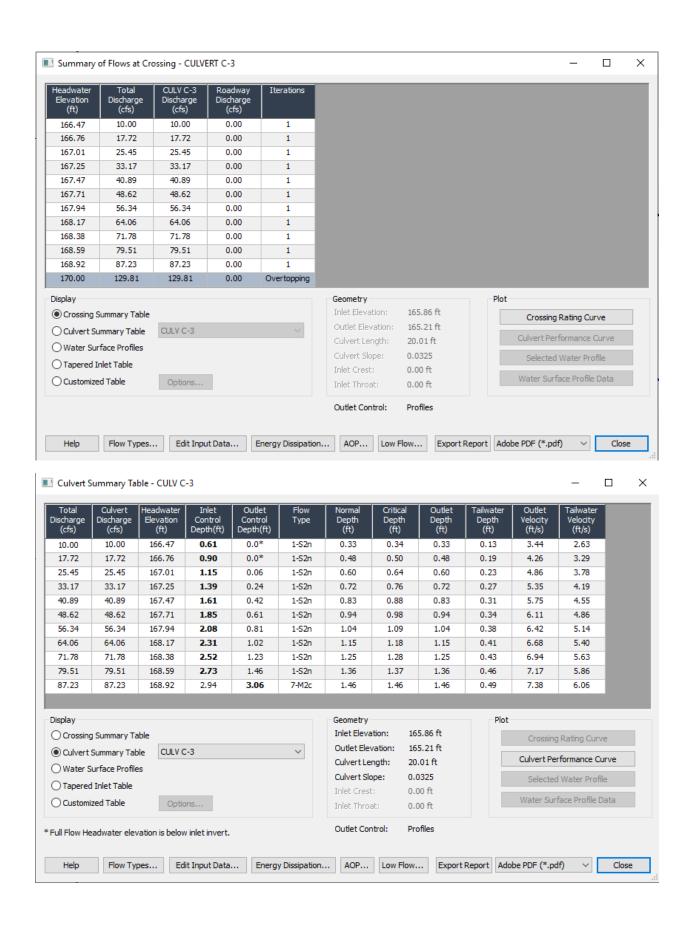
## Performance Curve Culvert: CULV C-1

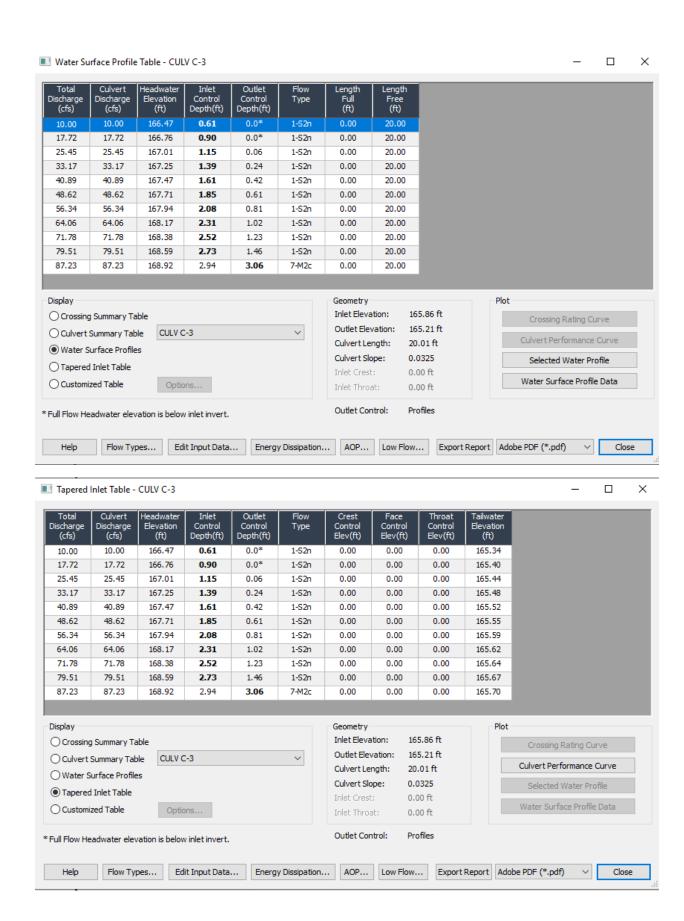


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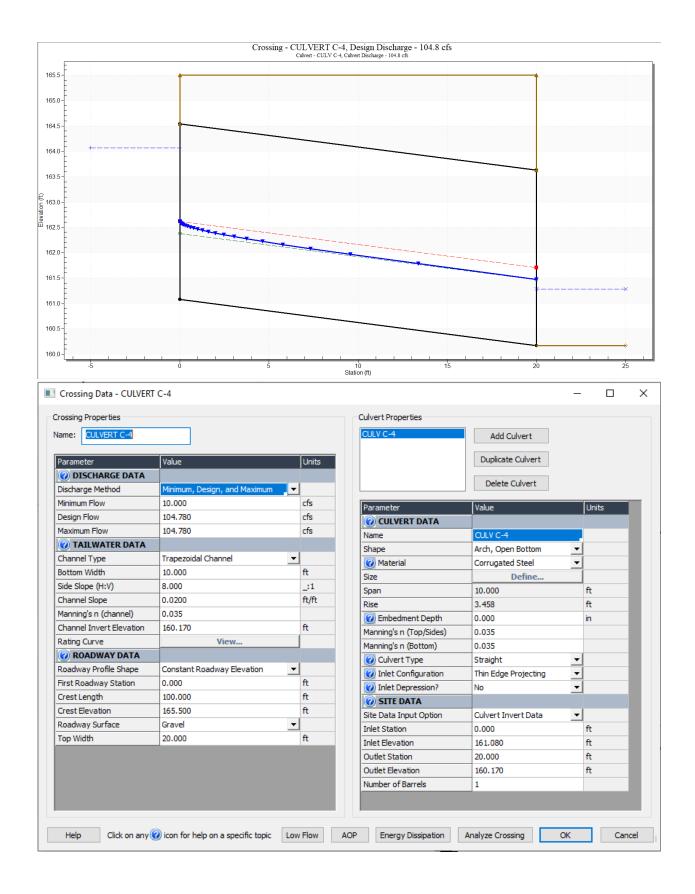


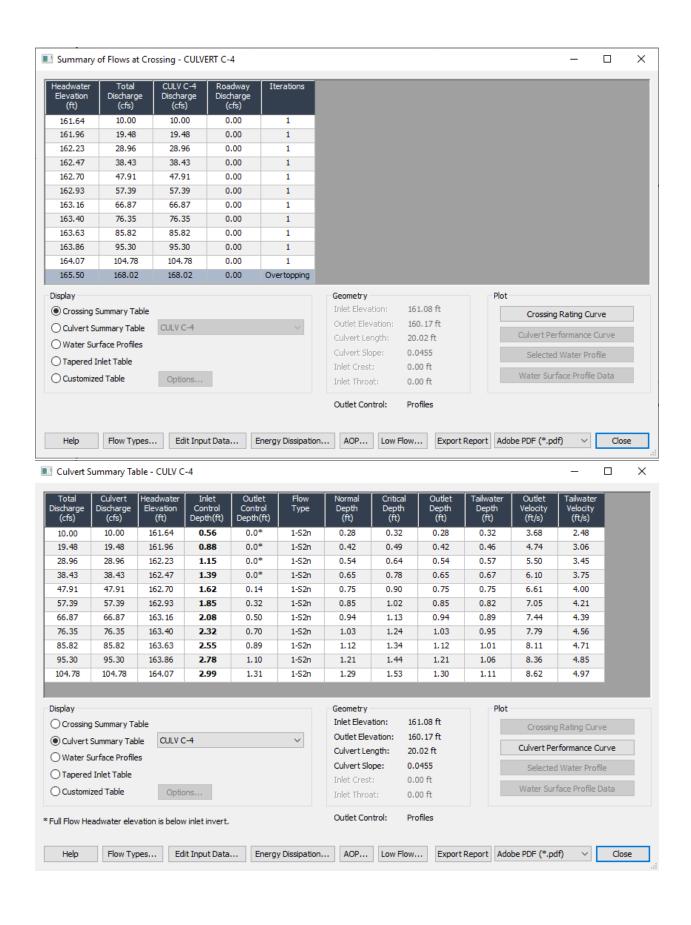


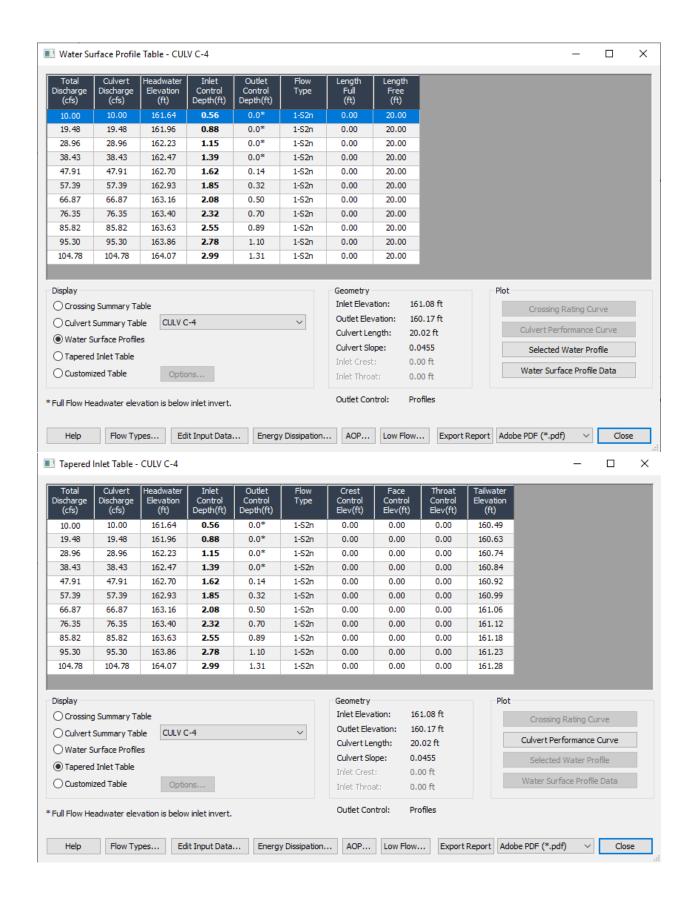


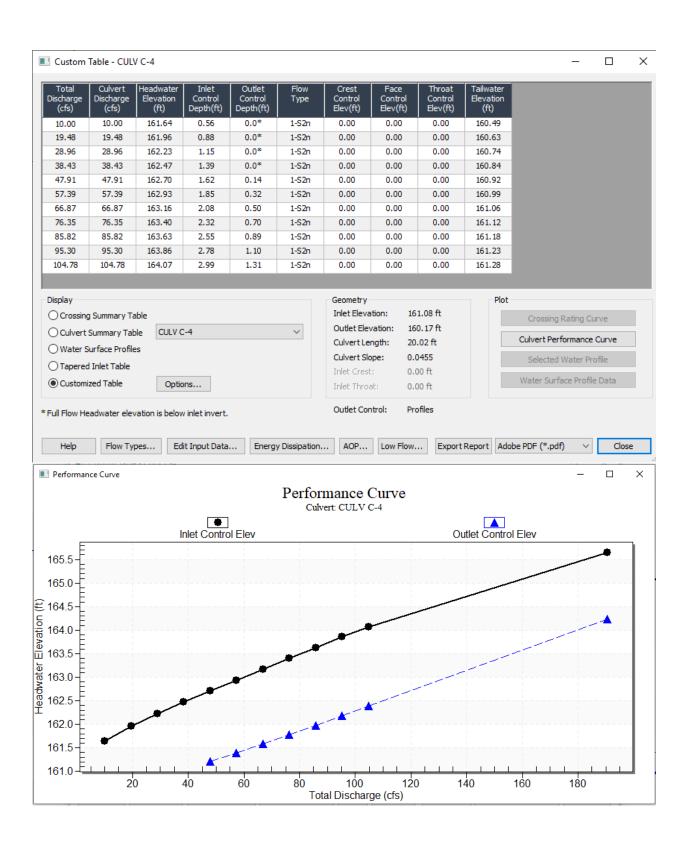


Total	Culvert	Headwater	Inlet	Outlet	Flow	Crest	Face	Throat	Tailwater		
Discharge	Discharge	Elevation	Control	Control	Type	Control	Control	Control	Elevation		
(cfs)	(cfs) 10.00	(ft) 166.47	Depth(ft) 0.61	Depth(ft)	1-S2n	0.00	0.00	0.00	(ft) 165,34		
10.00	17.72	166.76	0.90	0.0*	1-52n	0.00	0.00	0.00	165.40		
25,45	25.45	167.01	1.15	0.06	1-52n	0.00	0.00	0.00	165.44		
33.17	33.17	167.25	1.39	0.24	1-S2n	0.00	0.00	0.00	165.48		
40.89	40.89	167.47	1.61	0.42	1-S2n	0.00	0.00	0.00	165.52		
48.62	48.62	167.71	1.85	0.61	1-S2n	0.00	0.00	0.00	165.55		
56.34	56.34	167.94	2.08	0.81	1-S2n	0.00	0.00	0.00	165.59		
64.06	64.06	168.17	2.31	1.02	1-S2n	0.00	0.00	0.00	165.62		
71.78	71.78	168.38	2.52	1.23	1-S2n	0.00	0.00	0.00	165.64		
79.51	79.51	168.59	2.73	1.46	1-S2n	0.00	0.00	0.00	165.67		
87.23	87.23	168.92	2.94	3.06	7-M2c	0.00	0.00	0.00	165.70		
Dicelay						Coomoto			Plot		
Display	- Cumpress	abla				Geometry Inlet Eleva	ation: 16	5.86 ft	PIOT		
	g Summary Ta					Outlet Elev		5.21 ft		Crossing Rating Curve	
	Summary Tab		C-3		~	Culvert Le		.01 ft		Culvert Performance Curve	
○ Water S	Surface Profile	es				Culvert Slo	-	325		Selected Water Profile	
○ Tapered	d Inlet Table					Inlet Crest	•	00 ft		Selected Water Profile	
<ul><li>Customi</li></ul>	ized Table	Optio	ons			Inlet Thro		00 ft		Water Surface Profile Data	
Help	Flow Ty	pes Ed	lit Input Data	Energ	y Dissipation	. AOP	Low Flow.	Export	Report Ado	be PDF (*,pdf) V Clos	se .
Performar	nce Curve				D C		<b>C</b>				×
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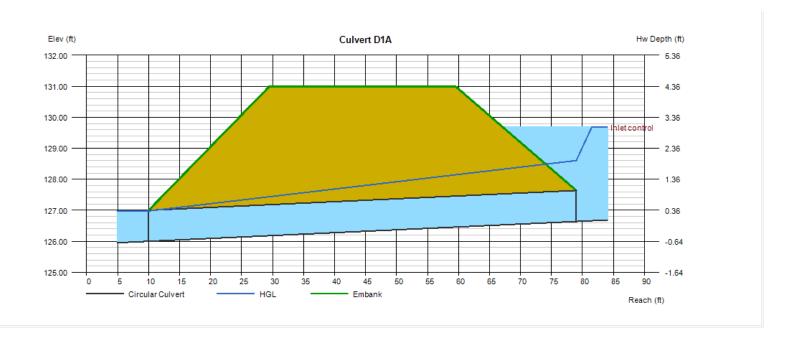
## **Culvert Report**

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Monday, May 24 2021

## **Culvert D1A**

Invert Elev Dn (ft)	= 126.00	Calculations	
Pipe Length (ft)	= 69.00	Qmin (cfs)	= 6.07
Slope (%)	= 0.93	Qmax (cfs)	= 6.07
Invert Elev Up (ft)	= 126.64	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 12.0	, ,	, ,
Shape	= Circular	Highlighted	
Span (in)	= 12.0	Qtotal (cfs)	= 6.07
No. Barrels	= 1	Qpipe (cfs)	= 6.07
n-Value	= 0.012	Qovertop (cfs)	= 0.00
Culvert Type	<ul><li>Circular Concrete</li></ul>	Veloc Dn (ft/s)	= 7.77
Culvert Entrance	= Square edge w/headwall (C)	Veloc Up (ft/s)	= 7.73
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5	HGL Dn (ft)	= 126.98
		HGL Up (ft)	= 128.60
Embankment		Hw Elev (ft)	= 129.68
Top Elevation (ft)	= 131.00	Hw/D (ft)	= 3.04
Top Width (ft)	= 30.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 0.00	-	



Stonington Solar Array Facility North Stonington, CT SRC

6/17/2021

Ditch Calculations

Storm Event: 100-yr 24-hr (Conveyance Protection, per DEEP storm manual 2004 Table 7-1)

Manning's "n": 0.025
Desired Freeboard: 3"

	Draina	age Area and I	Design Fl	OW			Ditch Slope							Ditch	Dims ar	nd Resu	ılts		
Drainage Area	Grading Area	Total Peak Runoff 100- yr Event (cfs)	Ditch	% of Drainage Area	Weighted Peak Runoff 100-yr Event (cfs)	Le	ength	Starting Inv.	Ending Inv.	Fall (ft)	Avg. Slope (%)	Shape	Side Slope z:1	Bott. (ft)	Depth (ft)	Top Width (ft)	Flow Depth (ft)	Free- board (ft)	Free- board (in)
1A	A	19.22	1A	33%	6.37	:	289	129.5	127.5	2	0.69%	Trap.	3	1	1	7	0.73	0.27	3.24
1B	А	19.96	1B	51%	10.15		515	129	127.5	1.5	0.29%	Trap.	3	1.5	1.25	9	1	0.25	3.00
1C	А	52.94	1C1	23%	12.06		790	137.5	123.5	14	1.77%	Trap.	3	1.5	1	7.5	0.73	0.27	3.24
	Α		1C2	43%	22.91		377	124.5	120	4.5	1.19%	Trap.	3	2	1.25	9.5	1	0.25	3
2	D	17.23	2A	29%	4.97		221	200	179	21	9.50%	Tri.	3	0	1	6	0.49	0.51	6.12
			2B	15%	2.65	_	165	198	181	17	10.30%	Tri.	3	0	1	6	0.39	0.61	7.32
4	В	40.93	4A	10%	4.29		275	141	127	14	5.09%	Tri.	3	0	1	6	0.53	0.47	5.64
			4B	43%	17.75		672	141	129	12	1.79%	Trap.	3	3	1	9	0.71	0.29	3.48
5	F	76.83	5A	29%	22.23		793	168	137	31	3.91%	Trap.	3	2	1	8	0.75	0.25	3
			5B	10%	7.52		861	176	133	43	4.99%	Tri.	3	0	1	6	0.65	0.35	4.2

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3.00

Wednesday, Jun 23 2021

#### Ditch 1A

Trapezoidal	
Bottom Width (ft)	= 1.00
Side Slopes (z:1)	= 3.00,
Total Depth (ft)	= 1.00

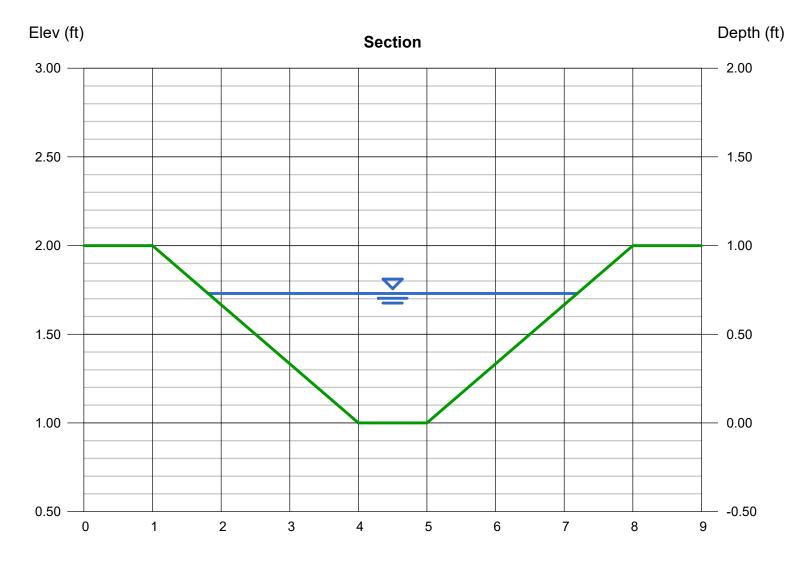
Invert Elev (ft) = 1.00 Slope (%) = 0.69 N-Value = 0.025

**Calculations** 

Compute by: Known Q Known Q (cfs) = 6.37

#### Highlighted

= 0.73Depth (ft) Q (cfs) = 6.370Area (sqft) = 2.33Velocity (ft/s) = 2.74Wetted Perim (ft) = 5.62Crit Depth, Yc (ft) = 0.63Top Width (ft) = 5.38EGL (ft) = 0.85



Reach (ft)

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

= 0.025

Wednesday, Jun 23 2021

#### Ditch 1B

ırapez	oldai
<b>Bottom</b>	Widtl

h (ft) = 1.50Side Slopes (z:1) = 3.00, 3.00Total Depth (ft) = 1.25 Invert Elev (ft) = 1.00 Slope (%) = 0.29

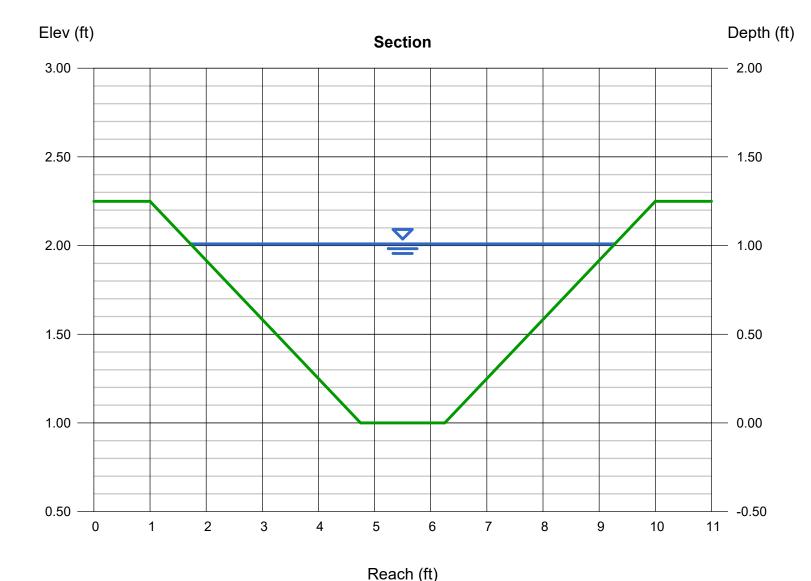
**Calculations** 

N-Value

Compute by: Known Q Known Q (cfs) = 10.15

#### Highlighted

Depth (ft) = 1.01 Q (cfs) = 10.15Area (sqft) = 4.58Velocity (ft/s) = 2.22Wetted Perim (ft) = 7.89Crit Depth, Yc (ft) = 0.73Top Width (ft) = 7.56EGL (ft) = 1.09



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Wednesday, Jun 23 2021

= 1.04

## Ditch 1C1

Trapezoidal	
Bottom Width (ft)	= 1.50
Side Slopes (z:1)	= 3.00, 3.00
Total Depth (ft)	= 1.00
Invert Elev (ft)	= 1.00
Slope (%)	= 1.77
N-Value	= 0.025

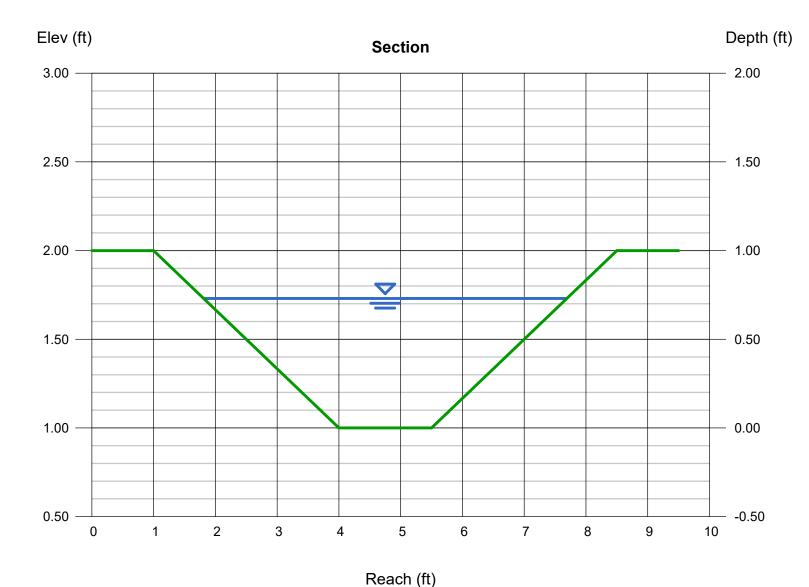
#### **Calculations**

Compute by: Known Q Known Q (cfs) = 12.06

# Highlighted Depth (ft) = 0.73 Q (cfs) = 12.06 Area (sqft) = 2.69

Area (sqft) = 2.69 Velocity (ft/s) = 4.48 Wetted Perim (ft) = 6.12 Crit Depth, Yc (ft) = 0.79 Top Width (ft) = 5.88

EGL (ft)



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## Ditch 1C2

Trapezoidal	
Bottom Width (ft)	= 2.00
Side Slopes (z:1)	= 3.00, 3.00
Total Depth (ft)	= 1.25
Invert Elev (ft)	= 1.00
Slope (%)	= 1.19
N-Value	= 0.025

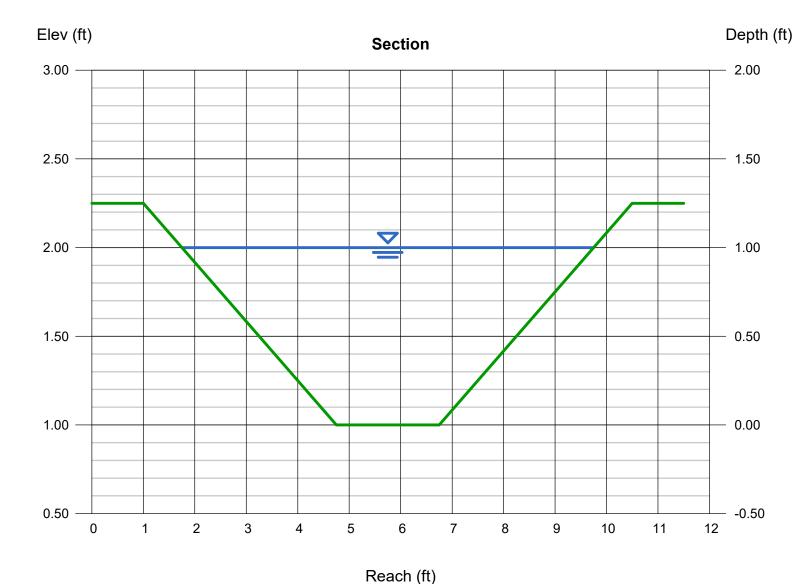
## Calculations

Compute by: Known Q Known Q (cfs) = 22.91

Highlighted	
Depth (ft)	= 1.00
Q (cfs)	= 22.91
Area (sqft)	= 5.00

Velocity (ft/s) = 4.58Wetted Perim (ft) = 8.32Crit Depth, Yc (ft) = 1.02Top Width (ft) = 8.00

EGL (ft) = 1.33



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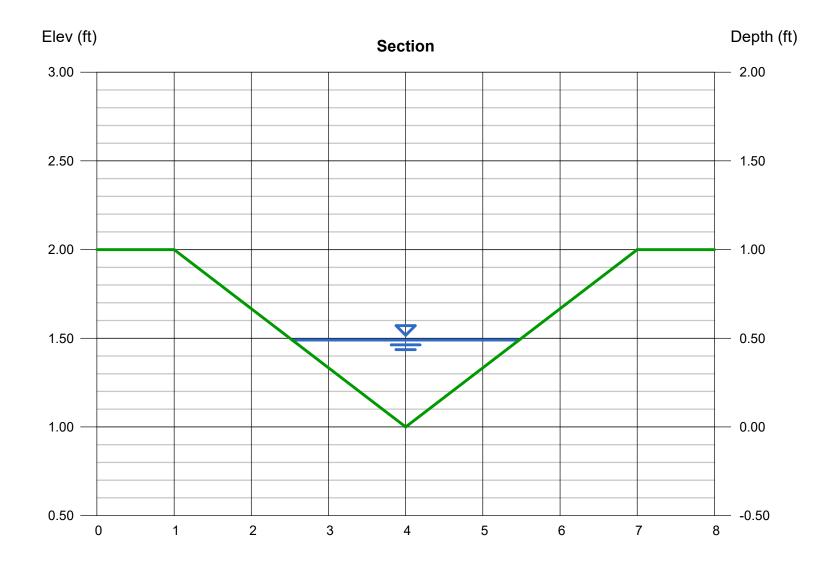
= 4.97

Wednesday, Jun 23 2021

## Ditch 2A

Known Q (cfs)

Triangular		Highlighted	
Side Slopes (z:1)	= 3.00, 3.00	Depth (ft)	= 0.49
Total Depth (ft)	= 1.00	Q (cfs)	= 4.970
		Area (sqft)	= 0.72
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 6.90
Slope (%)	= 9.50	Wetted Perim (ft)	= 3.10
N-Value	= 0.025	Crit Depth, Yc (ft)	= 0.71
		Top Width (ft)	= 2.94
Calculations		EGL (ft)	= 1.23
Compute by:	Known Q		



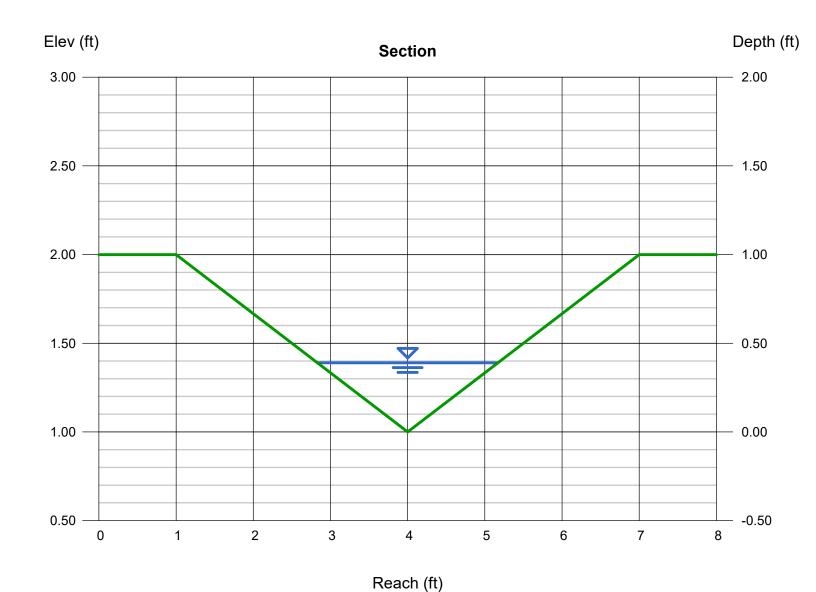
Reach (ft)

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Wednesday, Jun 23 2021

## Ditch 2B

Triangular		Highlighted	
Side Slopes (z:1)	= 3.00, 3.00	Depth (ft)	= 0.39
Total Depth (ft)	= 1.00	Q (cfs)	= 2.650
		Area (sqft)	= 0.46
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 5.81
Slope (%)	= 10.30	Wetted Perim (ft)	= 2.47
N-Value	= 0.025	Crit Depth, Yc (ft)	= 0.55
		Top Width (ft)	= 2.34
Calculations		EGL (ft)	= 0.91
Compute by:	Known Q		
Known Q (cfs)	= 2.65		



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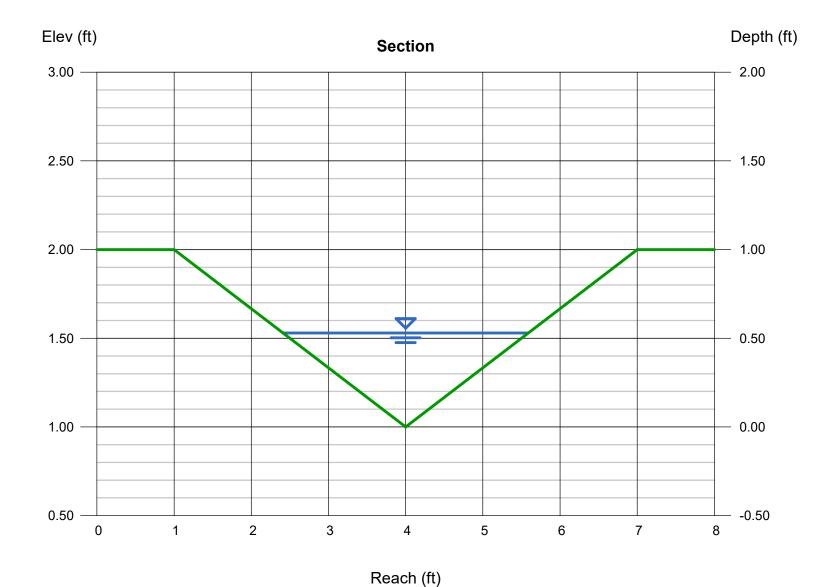
= 4.29

Wednesday, Jun 23 2021

## Ditch 4A

Known Q (cfs)

Triangular		Highlighted	
Side Slopes (z:1)	= 3.00, 3.00	Depth (ft)	= 0.53
Total Depth (ft)	= 1.00	Q (cfs)	= 4.290
		Area (sqft)	= 0.84
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 5.09
Slope (%)	= 5.09	Wetted Perim (ft)	= 3.35
N-Value	= 0.025	Crit Depth, Yc (ft)	= 0.67
		Top Width (ft)	= 3.18
Calculations		EGL (ft)	= 0.93
Compute by:	Known Q		



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## Ditch 4B

Trapezoidal	
Bottom Width (ft)	= 3.00
Side Slopes (z:1)	= 3.00, 3.00
Total Depth (ft)	= 1.00
Invert Elev (ft)	= 1.00
Slope (%)	= 1.79
N-Value	= 0.025

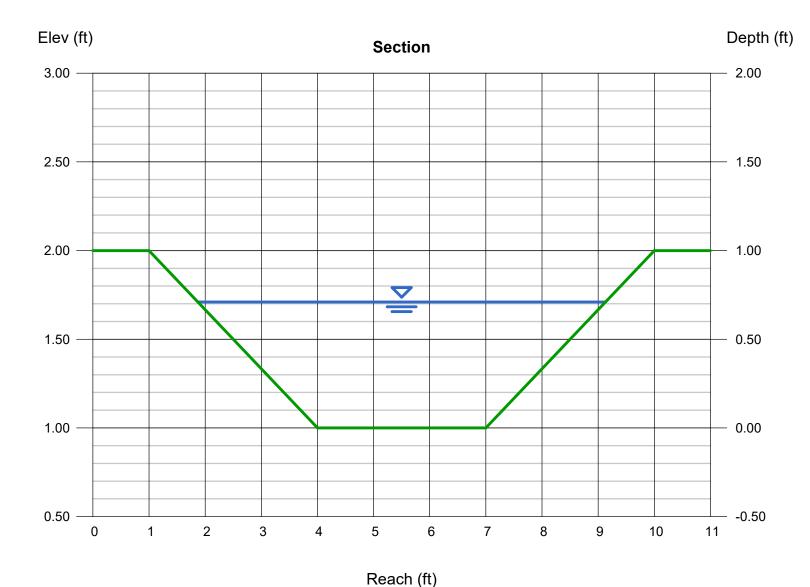
#### **Calculations**

Compute by: Known Q Known Q (cfs) = 17.75

Highlighted	
Depth (ft)	= 0.71
Q (cfs)	= 17.7
Area (sqft)	= 3.64

75 Velocity (ft/s) = 4.87Wetted Perim (ft) = 7.49Crit Depth, Yc (ft) = 0.79Top Width (ft) = 7.26

EGL (ft) = 1.08



Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

= 0.025

Wednesday, Jun 23 2021

## Ditch 5A

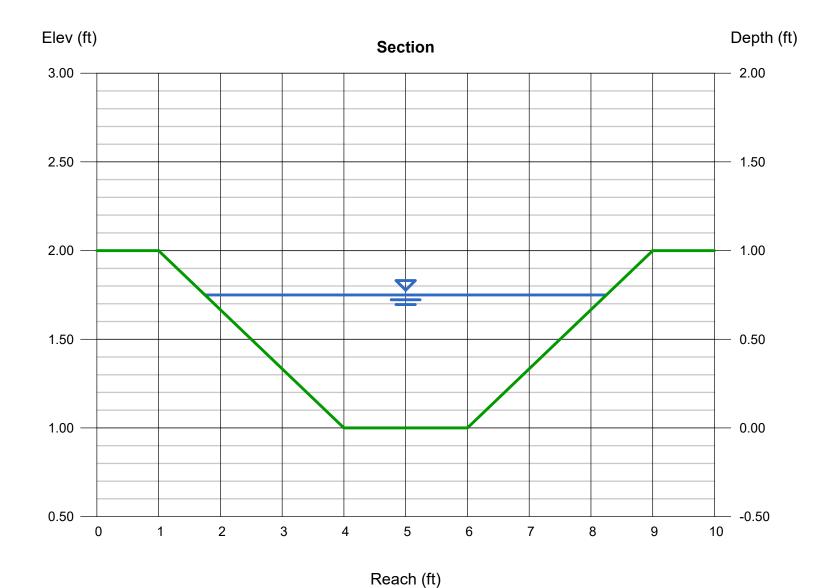
Trapezoidal	
Bottom Width (ft)	= 2.00
Side Slopes (z:1)	= 3.00, 3.00
Total Depth (ft)	= 1.00
Invert Elev (ft)	= 1.00
Slope (%)	= 3.91

**Calculations** 

N-Value

Compute by: Known Q Known Q (cfs) = 22.23

Highlighted	
Depth (ft)	= 0.75
Q (cfs)	= 22.23
Area (sqft)	= 3.19
Velocity (ft/s)	= 6.97
Wetted Perim (ft)	= 6.74
Crit Depth, Yc (ft)	= 1.00
Top Width (ft)	= 6.50
EGL (ft)	= 1.51



Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

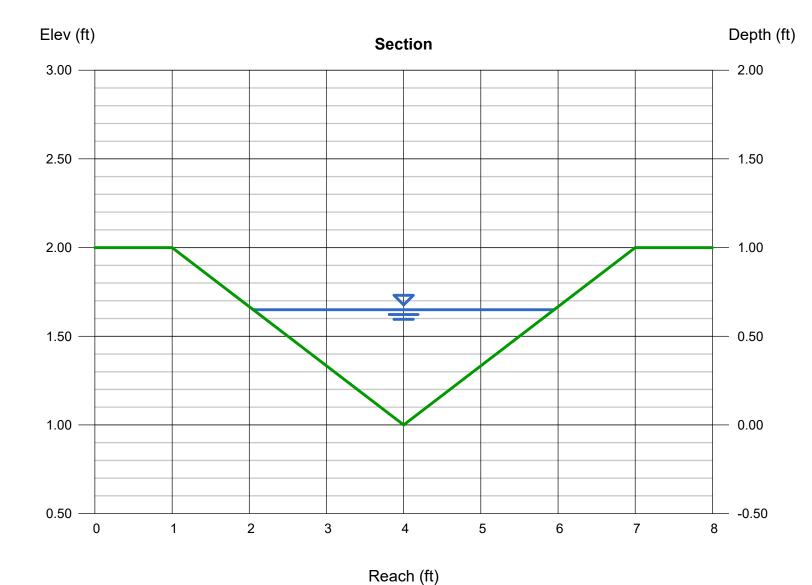
= 7.52

Wednesday, Jun 23 2021

## Ditch 5B

Known Q (cfs)

Triangular		Highlighted	
Side Slopes (z:1)	= 3.00, 3.00	Depth (ft)	= 0.65
Total Depth (ft)	= 1.00	Q (cfs)	= 7.520
		Area (sqft)	= 1.27
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 5.93
Slope (%)	= 4.99	Wetted Perim (ft)	= 4.11
N-Value	= 0.025	Crit Depth, Yc (ft)	= 0.83
		Top Width (ft)	= 3.90
Calculations		EGL (ft)	= 1.20
Compute by:	Known Q		



Stonington Solar Array Facility North Stonington, CT SRC

Water Quality Calculations

WQV = (1")(R)(A)/12

I = % Impervious Cover

R = Volumetric Runoff Coeff. = 0.05 + 0.009 (I)

A = Site Area (Ac)

Drainage Area	Area (A) (Ac)	Imp. Cover (I) (%)	Vol. Runoff Coeff. (R)	Required WQV (Ac-ft)	Required WQV (Cu-ft)	Provided WQV (Cu-ft)	Provided WQV (Ac- ft)	Pond Stage Elev.
1A	4.19	31%	0.327	0.11	4,975	5,226	0.12	125.80
1B	4.57	43%	0.436	0.17	7,233	7,519	0.17	120.20
1C	11.85	50%	0.502	0.50	21,589	21,863	0.50	115.70
2	3.66	29%	0.308	0.09	4,095	4,440	0.10	170.50
4	9.02	18%	0.215	0.16	7,028	7,405	0.17	121.00
5	15.22	35%	0.368	0.47	20,306	21,233	0.49	121.30